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ETABS

ACI 318-14 Example 001

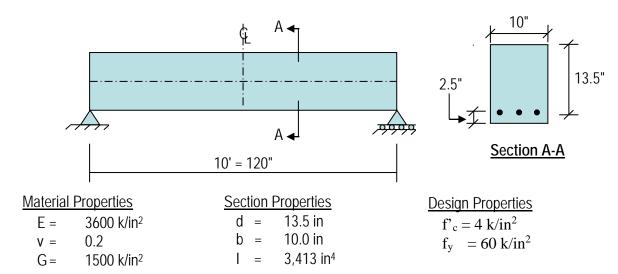
SHEAR AND FLEXURAL REINFORCEMENT DESIGN OF A SINGLY REINFORCED RECTANGLE

EXAMPLE DESCRIPTION

The flexural and shear design of a rectangular concrete beam is calculated in this example.

A simply supported beam is subjected to an ultimate uniform load of 9.736 k/ft. This example is tested using the ACI 318-14 concrete design code. The flexural and shear reinforcing computed is compared with independent hand calculated results.

GEOMETRY, PROPERTIES AND LOADING



TECHNICAL FEATURES TESTED

- ➤ Calculation of Flexural reinforcement, A_s
- Enforcement of Minimum tension reinforcement, A_{s,min}
- > Calculation of Shear reinforcement, A_v
- Enforcement of Minimum shear reinforcing, A_{v.min}



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RESULTS COMPARISON

Independent results are hand calculated based on the equivalent rectangular stress distribution described in Example 6.1 in Notes on ACI 318-14 Building Code.

Output Parameter	ETABS	Independent	Percent Difference
Design Moment, Mu (k-in)	1460.4	1460.4	0.00%
Tension Reinf, A _s (in ²)	2.37	2.37	0.00%
Design Shear Force, V _u	37.73	37.73	0.00%
Shear Reinf, A _v /s (in ² /in)	0.041	0.041	0.00%

COMPUTER FILE: ACI 318-14 Ex001

CONCLUSION

The computed results show an exact match for the flexural and the shear reinforcing.

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HAND CALCULATION

Flexural Design

The following quantities are computed for all the load combinations:

$$\varphi = 0.9, \ A_g = 160 \text{ sq-in}$$

$$A_{s,min} = \frac{200}{f_y} b_w d = 0.450 \text{ sq-in (Govern)}$$

$$= \frac{3\sqrt{f_c'}}{f_y} b_w d = 0.427 \text{ sq-in}$$

$$\beta_1 = 0.85 - 0.05 \left(\frac{f_c' - 4000}{1000}\right) = 0.85$$

$$c_{max} = \frac{0.003}{0.003 + 0.005} d = 5.0625 \text{ in}$$

$$a_{max} = \beta_1 c_{max} = 4.303 \text{ in}$$

Combo1

$$w_u = (1.2w_d + 1.6w_l) = 9.736 \text{ k/ft}$$

 $M_u = \frac{w_u l^2}{8} = 9.736 \cdot 10^2 / 8 = 121.7 \text{ k-ft} = 1460.4 \text{ k-in}$

The depth of the compression block is given by:

$$a = d - \sqrt{d^2 - \frac{2|M_u|}{0.85 f_c' \varphi b}} = 4.183 \text{ in } (a < a_{max})$$

The area of tensile steel reinforcement is given by:

$$A_s = \frac{M_u}{\varphi f_y \left(d - \frac{a}{2}\right)} = \frac{1460.4}{0.9 \cdot 60 \cdot \left(13.5 - 4.183/2\right)}$$

$$A_s = 2.37 \text{ sq-in}$$

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Shear Design

The following quantities are computed for all of the load combinations:

$$\varphi = 0.75$$

Check the limit of $\sqrt{f_c'}$:

$$\sqrt{f_c'} = 63.246 \text{ psi} < 100 \text{ psi}$$

The concrete shear capacity is given by:

$$\varphi V_c = \varphi 2 \sqrt{f_c'} bd = 12.807 k$$

The maximum shear that can be carried by reinforcement is given by:

$$\varphi V_s = \varphi 8 \sqrt{f_c'} bd = 51.229 k$$

The following limits are required in the determination of the reinforcement:

$$(\varphi V_c/2)$$
 = 6.4035 k
 $(\varphi V_c + \varphi 50 bd)$ = 11.466 k
 $\varphi V_{\text{max}} = \varphi V_c + \varphi V_s$ = 64.036 k

Given V_u , V_c and V_{max} , the required shear reinforcement in area/unit length for any load combination is calculated as follows:

If
$$V_u \leq \varphi(V_c/2)$$
,

$$\frac{A_{v}}{s}=0,$$

else if $\varphi(V_{\mathcal{O}}/2) < V_{\mathcal{U}} \leq \varphi V_{\text{max}}$

$$\frac{A_{v}}{s} = \frac{(V_{u} - \phi V_{c})}{\phi f_{ys} d} \ge \left(\frac{A_{v}}{s}\right)_{\min}$$

where:

$$\left(\frac{A_{v}}{s}\right)_{\min} = \max\left\{50\left(\frac{b_{w}}{f_{yt}}\right), \left(\frac{b_{w}}{f_{yt}}\right) \cdot \frac{3}{4}\sqrt{f_{c}'}\right\}$$

else if $V_u > \varphi V_{\text{max}}$,

a failure condition is declared.



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Combo1

$$V_{u} = 9.736^{\bullet}(5-13.5/12) = 37.727 \text{ k}$$

$$\phi(V_{c}/2) = 6.4035 k \le V_{u} = 37.727 k \le \phi V_{\text{max}} = 64.036 k$$

$$\left(\frac{A_{v}}{s}\right)_{\text{min}} = \max\left\{50\left(\frac{10}{60,000}\right), \left(\frac{10}{60,000}\right)^{\bullet} \frac{3}{4}\sqrt{4,000}\right\}$$

$$\left(\frac{A_{v}}{s}\right)_{\text{min}} = \max\left\{0.0083, 0.0079\right\} = 0.0083 \frac{in^{2}}{in}$$

$$\frac{A_{v}}{s} = \frac{(V_{u} - \phi V_{c})}{\phi f_{vs} d} = 0.041 \frac{in^{2}}{in} = 0.492 \frac{in^{2}}{ft}$$