



**RDL**® *Radio Design Labs*®

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*SPECIALISTS IN PRACTICAL PRECISION ENGINEERING™*

# ACM-2

M A N U A L

# WARNING

Installation of this equipment requires connection to sample ports on high power coaxial line sections. In some instances, a coaxial line section may need to be installed in order to provide a suitable sample port. The voltages and currents in such line sections are DANGEROUS. The installation, operation, and maintenance of the line sections can involve risks to the safety of personnel and equipment, and should be attempted ONLY by fully qualified engineers who are aware of the risks involved. Primary power to the transmitter should be disconnected during any work involving the transmission lines and related line sections. Personnel must at all times observe safety regulations and precautions provided by the manufacturers of the transmitters and transmission lines. RADIO DESIGN LABS shall not be responsible for injury or damage resulting from improper procedures, or for the employment of unqualified, inexperienced, or improperly trained personnel to perform any task related to this product. It is the sole responsibility of the purchaser to use qualified personnel, to exercise due care, and to enforce appropriate safety precautions in the installation and use of this or any other electronic equipment.

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RDL™ reserves the right to change design parameters and specifications at any time without notice. The performance measurements reflect the products at the time of printing.

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## Introduction

The ACM-2 is a test instrument which monitors the amplitude component present on frequency modulated carriers. The AM component is representative of bandwidth characteristics in the transmission system. The technology of significant synchronous AM noise monitoring was pioneered by Radio Design Labs, the originator of AM noise monitors for FM radio and television aural transmission.

In theory, FM carriers are of a constant amplitude over the range of frequencies they swing above and below carrier frequency. In practice, however, the amplitude is compromised by a variety of factors. These amplitude modulations of the carrier comprise AM noise. Two general varieties of AM noise are considered: 1] Noise induced by power supplies and blower vibrations (noise not synchronized to the applied modulation); 2] AM Noise resulting from frequency modulation of the carrier (noise synchronized to the applied modulation, hence "synchronous" AM noise). This noise is produced by passband amplitude and phase non-linearities in the rf transmission system. Consequently interstage matching is a significant contributor to AM noise as is the phase delay inherent in high gain amplifier stages. These factors combine to produce an operating passband for the transmission system.

As the carrier frequency shifts with modulation, the carrier frequency (or actually resultant sidebands) at a given instant will fall on some point of the skirts of a tuned circuit. If the bandwidth of the tuned circuit is sufficient, the amplitude of the FM carrier will remain constant, or so nearly constant that the amplitude variation is not significant. If there is any roll-off to the passband of the tuned circuit, the carrier amplitude will change with shifting frequency resulting in amplitude modulation.

The FM transmission system considered as a whole will exhibit different passband characteristics above the carrier frequency as it does below that frequency. Therefore the sidebands, both upper and lower, generated by a single cycle of modulation will be unequally attenuated. The resulting disparity produces a difference in carrier amplitude which can be demodulated in an FM receiver. The phase relationship between this demodulated signal and the recovered frequency modulation produces an audible mix which, in stereo systems, is then further demodulated into left and right. It is easily seen how these effects will degrade both stereo and audio receiver performance. The incoming amplitude modulations are often further affected by automatic gain control circuits in the receiver.

## EFFECTS OF AM NOISE

In the FM receiver, signal integrity is dependent on accurate demodulation of several signals, including both amplitude and often frequency modulated subcarriers which are typically at least 20dB below full carrier. Shifts in amplitude can therefore produce marked effects on the subcarrier performance, as intermodulation distortion produces substantial baseband noise in the receiver. This is first usually noticed in degraded stereophonic performance resulting from multipath distortion of the received signal. Observations of the station signal on analog tuners frequently yields an actual narrowing of the occupied width on the dial, even with fairly minor increases in AM noise. AM noise levels in the transmission system can produce noise in the receiver similar to the AM noise actually generated by multipath itself. These effects are detrimental to SCA operation, as crosstalk from the main channel becomes objectionable. These same effects degenerate stereo performance. Even moderate levels of multipath which might otherwise not be objectionable, have been observed to become severe when compounded with transmission system AM noise. Although keeping close monitoring and control over variations in AM noise in the transmitter cannot eliminate multipath distortion which occurs after the signal leaves the antenna, minimizing transmitter AM noise keeps the overall multipath artifacts at the very minimum possible in the receiver. Close control of transmitter AM noise makes possible optimum performance of both SCA and stereophonic transmission.

## **SIGNIFICANT SYNCHRONOUS AM NOISE**

Amplitude modulations which are of both sufficient amplitude and pulse width to produce any receiver artifacts are revealed by the various sampling bandwidth and time constants of analysis circuits in the ACM-2. This significant synchronous noise component is displayed on a fast-rise, damped-decay string display.

## **AM NOISE MONITORING**

As tubes slowly age, and temperatures change, the significant synchronous AM noise level in the transmission system changes. Very low AM noise levels will not materially affect receivers. However, as AM noise increases, it will exceed the threshold above which performance degradation is noticed in SCA or stereo operation. Good engineering of consistent FM transmission requires close control of AM noise, as well as the facility to distinguish between signal inconsistencies produced by AM noise and those resulting from propagation anomalies. To accomplish this, the engineer must have immediate access to AM noise readings. The ACM-2 constantly monitors the AM noise levels and provides an alarm output which can be used to alert the duty operator when the AM noise has exceeded the value set by the engineer. By setting this alarm threshold several dB below the point where AM effects are determined to be objectionable, a transmitter trip can be scheduled and the AM level can be controlled prior to the station signal suffering any adverse effects. The ACM-2 also provides a calibrated remote control output permitting the AM noise level to be read from the studio location at all times.

## **SAMPLING**

Samples of FM carriers are often available at different points in the transmission system. The only appropriate place to obtain an rf sample appropriate for AM noise measurements is AFTER THE LOW-PASS (or other bandwidth-limiting) FILTER. "Monitor" jacks in the PA cavity area of a transmitter are totally useless for AM noise measurements. These jacks provide rf containing harmonic content which yields the AM noise readings totally erroneous. The DCF-100MB supplied with the ACM-2 is to be connected to a DIRECTIONAL sampler situated in a metering line section at the point nearest the antenna feed-line. Samplers are available in two general types: Capacitive samplers and Directional samplers. It is a sampler of the directional type which must be used for AM noise readings. Capacitive samplers typically have a screw adjustment on them to set rf pickup, and they sample both forward and reflected waves. For AM noise measurements, only the forward wave must be used. It is imperative that the DCF-100MB be connected physically RIGHT AT THE SAMPLER JACK. Do not connect a length of cable between the sampler and the DCF-100MB input, as even the slightest VSWR in this cable can substantially impair the accuracy of your readings. Often a station will have a line section already installed just prior to the antenna feed line for power monitoring purposes. One of these sample ports is suitable for installing a directional sampler to feed the DCF-100MB. Often, however, one or both of these ports is being used to feed either remote control readings or to detect transmitter power for automatic switchover or alerts. If the sampler for the DCF-100MB is displacing metering slug normally used to supply a forward power indication, note that the ACM-2 has a DC power metering output. This output can be used for remote power metering, or can be resistively divided down to a usable sample level for other switching purposes. This ACM-2 output is independent of the front-panel calibrate control, and is buffered against external load effects.

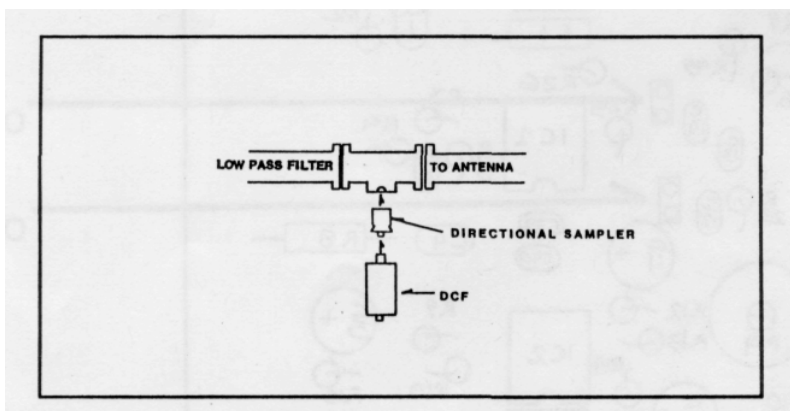
## INSTALLATION:

### READ AND UNDERSTAND THIS BEFORE INSTALLING!!!

Many hookups within a broadcast facility can be done merely to "make it work", even though they may not be exactly done right. THIS IS NOT THE CASE WITH AM NOISE SAMPLES. If you do not begin with an accurate sample, your ACM-2 may still register readings, however, those readings can be grossly inaccurate, leading you to make corresponding adjustments to your transmitter which have an adverse effect on your signal or efficiency. Obtaining a correct sample is not difficult, but the importance of "doing it right" cannot be emphasized enough. Once a correct sample is established, you can have years of optimum service from your transmitter without giving the sample port a "second thought". If you have not yet read the preceding section, "SAMPLING", read it now, as it details all the pertinent considerations in establishing an accurate sample point.

Plugging the DCF-100MB into just any BNC rf sample may not be appropriate. If the sample contains harmonic energy (as in PA rf loop samples, or any pre-harmonic-filter samples), or if it contains reflected power, this additional material can add or subtract from your fundamental carrier rf voltage, thereby generating AM noise IN YOUR SAMPLE. This problem is avoided by the use of a DIRECTIONAL (forward) sample.

Many, if not most, FM stations have a line section with slug ports for power metering. An excellent method of obtaining a forward sample suitable for AM noise metering is to replace a slug with a directional rf sampler, as shown in the following drawing:



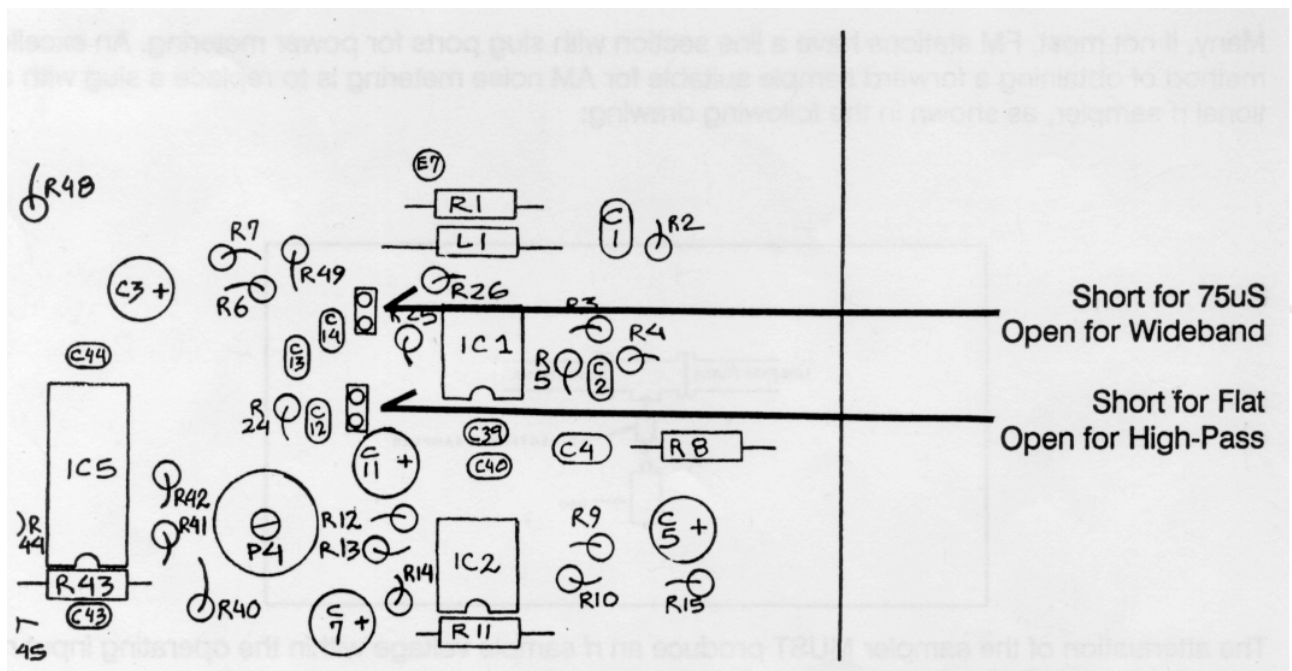
The attenuation of the sampler MUST produce an rf sample voltage within the operating input range of the DCF-100MB. The following table lists the appropriate attenuation levels for common power ranges. Part numbers are shown for samplers produced by Coaxial Dynamics (Cleveland, Ohio). These samplers are specifically designed for use with the ACM-2.

<u>Transmitter Power</u>	<u>Line Section</u>	<u>Attenuation</u>	<u>Sampler</u>
440W-5KW	1-5/8"	40 dB	87024H
4.4Kw-35Kw	3-1/8"	50 dB	87035H

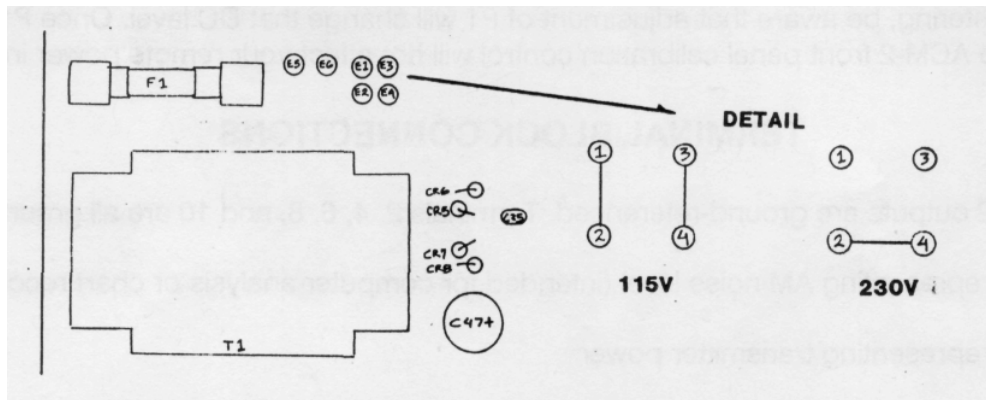
Coaxial Dynamics      800-262-9425  
                                 216-267-2233

The ACM-2 package consists of two units. The DCF-100MB is plugged directly into a directional sampler, as described above. You must connect a coaxial cable with a BNC plug on each end between the DCF-100MB and the ACM-2. The ACM-2 is designed to mount in a standard 19" equipment rack. Slots are provided in the ACM-2 chassis for ventilation. Do not mount the ACM-2 such that these slots are obstructed. As supplied from the factory, the ACM-2 is set up for "ACM Standard Wideband" signal analysis, with no high-pass filtering. This is the correct setting for nearly every installation. Two options are available, however, and should be considered prior to installation. Removal of the cover will reveal two jumpers on the pc board. One selects 75 $\mu$ S de-emphasis for all AM noise readings. This may be selected if the ACM-2 is being used to analyze asynchronous noise, or is used in a country or for measurements where de-emphasis is required. The second jumper selects the high-pass filter. This is used in the rare circumstance where the asynchronous AM noise (power supply and/or blower vibrations) are a few dB greater than the synchronous AM noise. This filter rolls off the low frequencies to permit accurate synchronous AM noise nulling on such transmitters. In most instances where asynchronous noise is greater than synchronous noise, this indicates a need for power supply repair rather than a need to select this filter! It is recommended that the ACM-2 be first installed using the factory settings. These are later easily changed, if desired.

The following drawing details the jumper locations:



The ACM-2 is capable of operation from either a 115 or 230v power source. If it is desired to change operating input voltage, this is done by means of soldered jumpers on terminal posts. The following drawing details the connections required for each operating input voltage. DISCONNECT PRIMARY POWER BEFORE ATTEMPTING TO CHANGE THESE JUMPERS! These terminals are located between the ACM-2 rear panel and the power transformer. It is necessary to remove the top cover to change these settings.



### CAUTION

DO NOT CONNECT THE RF SAMPLE FROM YOUR TRANSMISSION LINE SAMPLER DIRECTLY TO THE INPUT ON THE RACK-MOUNT ACM-2. THE DCF-100MB MUST BE CONNECTED BETWEEN THE SAMPLER AND THE ACM-2!

INSURE THAT THE RF SAMPLE DOES NOT PRODUCE A VOLTAGE WHICH EXCEEDS THE INPUT RATING OF THE DCF-100MB. A MAXIMUM SIGNAL INPUT OF 20V P-P INTO 50 OHMS IS PERMITTED. NOMINAL CORRECT INPUT IS 8V P-P INTO 50 OHMS.

Before connecting the DCF-100MB to the sample port, first connect it to the input of the ACM-2, with power applied to the ACM-2. Connect a DC voltmeter between terminals 3(+) and 4(Gnd) on the rear terminal board. Set the voltmeter to a scale appropriate to read from 0v to 20vdc. The coarse input level trimmer, P1, is located adjacent to the terminal board on the rear of the ACM-2. Set P1 for approximately 1/8 turn from the off (counter-clockwise) stop. With the transmitter on, connect the DCF-100MB to the sample port and observe the voltage on your DC voltmeter. If the voltage exceeds 10 vdc, then your sample is likely to exceed the input limits of the DCF-100MB. Check the 50 Ohm loaded sample voltage at the DCF-100MB input. This is most easily accomplished by inserting a BNC "T" prior to the DCF-100MB and observing the p-p rf voltage with a high-frequency oscilloscope.

Once it is known that the sample voltage does not exceed the DCF-100MB input limit, advance P1 (with DCF connected, and transmitter operating) until you obtain a reading of 12.5vdc. If you are unable to obtain this reading, then your sample voltage is insufficient, and a sampler yielding less attenuation must be installed to feed the DCF-100MB. Once you have adjusted P1 and obtained a reading of 12.5vdc, the ACM-2 is ready to make readings.

If the ACM-2 is to be connected to a remote control, check your remote control manual for the maximum permitted DC input voltage on a metering channel. If the metering input cannot withstand a DC input voltage of at least 12.5 volts, it is recommended that metering outputs from the ACM-2 be attenuated through a resistive voltage-divider, or through a variable attenuator. RDL's STP-1 operated in the high-impedance mode, is a suitable variable attenuator for this purpose. The STP-1 is a two channel device. One channel can be used to attenuate power metering. The other channel can be used to attenuate the remote AM noise reading.



If you plan to use the remote power metering output from the ACM- 2 for your remote control transmitter power metering, be aware that adjustment of P1 will change that DC level. Once P1 is set, operation of the ACM-2 front panel calibration control will not affect your remote power indication.

## TERMINAL BLOCK CONNECTIONS

Note: All ACM-2 outputs are ground-referenced. Terminals 2, 4, 6, 8, and 10 are all ground terminals.

- 1] DC output representing AM noise level (intended for computer analysis or chart recorder)
- 3] DC output representing transmitter power
- 5] Remote metering AM noise output (continuously averaged DC voltage representing AM noise level for remote readings. Ratio of 1v to 10v corresponds to the 20dB on ACM-2 display)
- 7] Audio output (used to feed an audio amplifier if audio indication is desired to assist in transmitter tuning. RDL's™ STA-3 together with a small loudspeaker make a convenient monitoring system.)
- 9] Alarm output (Used for status indication of excessive AM noise. "0" volts present when alarm threshold not exceeded; approx. +15vdc present when alarm threshold is exceeded. If a contact closure is required, use RDL's ST-LCR1 Logic Interface module.)

## OPERATION

*CALIBRATING THE ACM-2* First set the "DISPLAY<sup>1</sup>" selector to the "OP" position, and set the "MODE" selector to the "CAL" position. The display now shows the ACM-2's internal carrier level reference. Adjust the "CAL" control adjacent to the "MODE" selector until the uppermost LED on the display JUST LIGHTS. This sets the internal point to which all AM noise readings are referred. The ACM-2 is now calibrated and ready to read AM noise. Return the "MODE" selector to the "OP" position.

*READING AM NOISE* The purpose of AM noise monitoring is to evaluate transmission system performance under actual operating conditions. The ACM-2 is to be used under full modulation, using normal programming together with any subcarriers. Do not unmodulate the transmitter or inject particular test tones for the reading of AM noise, unless doing so for some specific purpose. For normal AM noise readings, begin with both "RANGE" selectors out, which is the "0" dB position for each switch. With this setting, the ACM-2 is amplifying the AM component 20dB and the display is registering the AM component between 20 and 39 dB below the carrier. The range is indicated by the illuminated range pointer. If there is no display on the monitor, then your AM noise is below -39dB, and you will need to switch in either 10dB, 20dB, or 30dB (both the 10dB and 20dB switches) additional gain. As you do so, the range pointer will change to indicate the proper range to read. Transmitters which have not previously been tuned and adjusted for maximum bandwidth, or minimum AM noise, typically can read around -25dB. Correctly adjusted transmitters typically read -50 to -60dB. Once final tuning has been accomplished, it is recommended that a range be selected which has only a few LEDs flashing. AM noise tends to increase with time, and this range selection will permit these increases, while still maintaining an on-scale reading. It also permits the alarm threshold to be set to a comfortable mid-scale point.

*NOTE:* During tuning, the AM noise levels frequently jump to greater than full-scale indications. This in no way damages the ACM-2. It is normal for this to occur.

*SETTING THE ALARM THRESHOLD* Prior to initially setting the alarm threshold, it may be desirable to detune the transmitter slightly, noting the ACM-2 reading as it relates to main channel degradation, subcarrier crosstalk, and increased multipath artifacts. Once a threshold has been established above which performance is substantively degenerated, a reasonable alarm threshold can be determined. This threshold is typically 5 to 8 dB below the objectionable AM level in order to allow sufficient time for a transmitter visit to be planned. Some engineers may already have target alarm figures in mind. Many engineers find that the absolute worst-case AM level tolerable is about -45dB, with -55dB to -60dB being acceptable tuning targets. Other engineers operating transmitters in variable terrain find -50dB to be the worst tolerable AM noise level.

Set the "DISPLAY<sup>1</sup>" selector to the "SET<sup>1</sup>" position and adjust the "ALARM" knob until the uppermost LED illuminated indicates the threshold desired. Then return the selector to the "OP" position. Now, when the threshold is exceeded, the "ALARM" LED will light, and a "HI" will appear at the remote alarm terminal on the rear of the ACM-2.

*OBSERVING AM NOISE* The amplitude component may be observed visually by connecting an oscilloscope to the front panel "SCOPE" Monitor Jack. This may be particularly helpful in isolating the nature and source of asynchronous AM noise during maintenance periods. It is an interesting tuning aid, particularly the first time or two the ACM-2 is used on a given transmitter. Under modulation, it becomes visibly apparent whether slope detection is equal in both sidebands, or if a circuit is off-tuned to one side or the other. After some use of the ACM-2, the engineer will acquire a "feel" for properly centered tuning, as the ballistics of the LED string are substantially slower, indicating less peak activity, when neither sideband is excessively slope detected.

*REMOTE CONTROL READINGS* The reading fed to the remote AM noise terminals on the barrier block, is a continuously "averaged" derivation of the front panel display. The "averaging" circuit is actually a modified "peak-hold" circuit which indicates the highest AM excursion "instantly", and then decays very slowly. It is only "averaging" in the sense that very rapid spikes which would tend to destabilize digital remote controls are ignored by the circuit. Under normal, correctly tuned transmitter operation, the remote AM output is therefore a slow-release version of exactly what appears as the highest consecutive peak excursions on the front panel display.

The remote reading circuitry uses the logarithmic 1 : 10 relationship to correspond to the 20dB display range. A reading of full-scale on the display would be "10" (or a voltage scaled down from 10). A reading 20dB below this figure would output "1" (or a voltage scaled down USING THE SAME RATIO as that used to scale down the "10"). If the actual full-scale output read 10 volts, then a displayed -20dB would output 1 volt, and a -10dB display would output 3.16 volts. This permits the calibration and reading even on a digital remote control, without logarithmic display, to be simple and straightforward. If you calibrate the remote control channel to read 10, 100, or 1000, then all that is required to read the actual AM noise is a chart converting the remote reading into decibels. These charts are already prepared and are found in the back of this manual. They are for your use, to photocopy and place at the control point in your system.

To calibrate your remote control, select the ACM-2 input on your remote control. Set the "MODE" selector on the ACM-2 to the "CAL" position, and adjust the remote control channel input so you have an appropriate reading on the remote control. It is suggested to use 10, 100, or 1000, as this makes the charts provided in this manual direct-reading. Once this level is set, return the ACM-2 "MODE" switch to the "OP" position.

*PRACTICAL GUIDELINES FOR TRANSMITTER TUNING* Transmitter tuning is typically the most critical element in maintaining acceptable AM noise levels. These levels can often be brought to within practical operating limits through tuning only. It is critical that each stage be matched correctly, including the input from the exciters well as the output to the antenna. Best performance is attained

when the collective system passband has no excessive roll-off of either or both sidebands, and when each stage is centertuned. Bear in mind that the total passband performance of the transmitter is an accumulation of attenuation and group delay. Therefore, a shift on one parameter in one stage may be compensated by a shift elsewhere. This means that best overall performance doesn't necessarily result when a given interstage match has a VSWR of exactly 1.0:1.0, although it should be close. Symmetrical sideband performance is not always practical, and certain limited compromise may be required.

If your transmitter is running subcarriers (in addition to the 38KHz), the AM noise should be nulled with tuning while the subcarriers are on. Then the null should be checked with the subcarriers off. Main channel modulation should be present at all times. If there is a shift in tuning with the subcarrier on or off, this indicates one or more stages with uneven attenuation in sidebands. This is likely indicative of a serious passband problem and should be investigated. This problem, as with generally excessive AM noise levels, is often improved through increased final amplifier loading. In tetrode amplifiers, the screen voltage is generally a highly volatile parameter in achieving minimum AM noise. Development of new tuning procedures for minimum AM noise is frequently aided by trying first tuning the power amplifier and then moving to the driver stages. Certain trial and error is required, bearing in mind good stage matches and wideband operation yields the best results.

## **CIRCUIT DESCRIPTION**

Signal input is applied through J1. This signal supplied by the DCF-100MB, contains a DC reference voltage together with an ac voltage. The DC represents the carrier level. The ac voltage is the preconditioned AM component. The signal input is applied to the coarse input level control P1 through rf filter L1, C1. IC1A brings the signal up to the appropriate operating level for the ACM-2. The DC signal is extracted by low-pass filter R6, C3 and is buffered by IC5B which feeds the remote power output terminals.

The output of the input attenuator P1 is filtered by R12, C4 as it enters the splitter circuitry. IC2A buffers the signal to low-pass filter R11, C7. IC2B amplifies the DC carrier level. P4 is the calibration control for the DC reference. The DC signal is blocked by C5, feeding the ac component into amplifiers IC4A, IC4B, and IC1B. Each side of IC4 adds gain to the ac component, as selected by S1 and/or

S2. IC1B provides programmable filtering. When the input jumper is removed, C12 together with R24 provide low frequency roll-off. When the feedback jumper is closed, C13 together with R25 provide 75uS de-emphasis of the ac component.

IC6A buffers the amplified ac component for distribution to the audio and scope outputs.

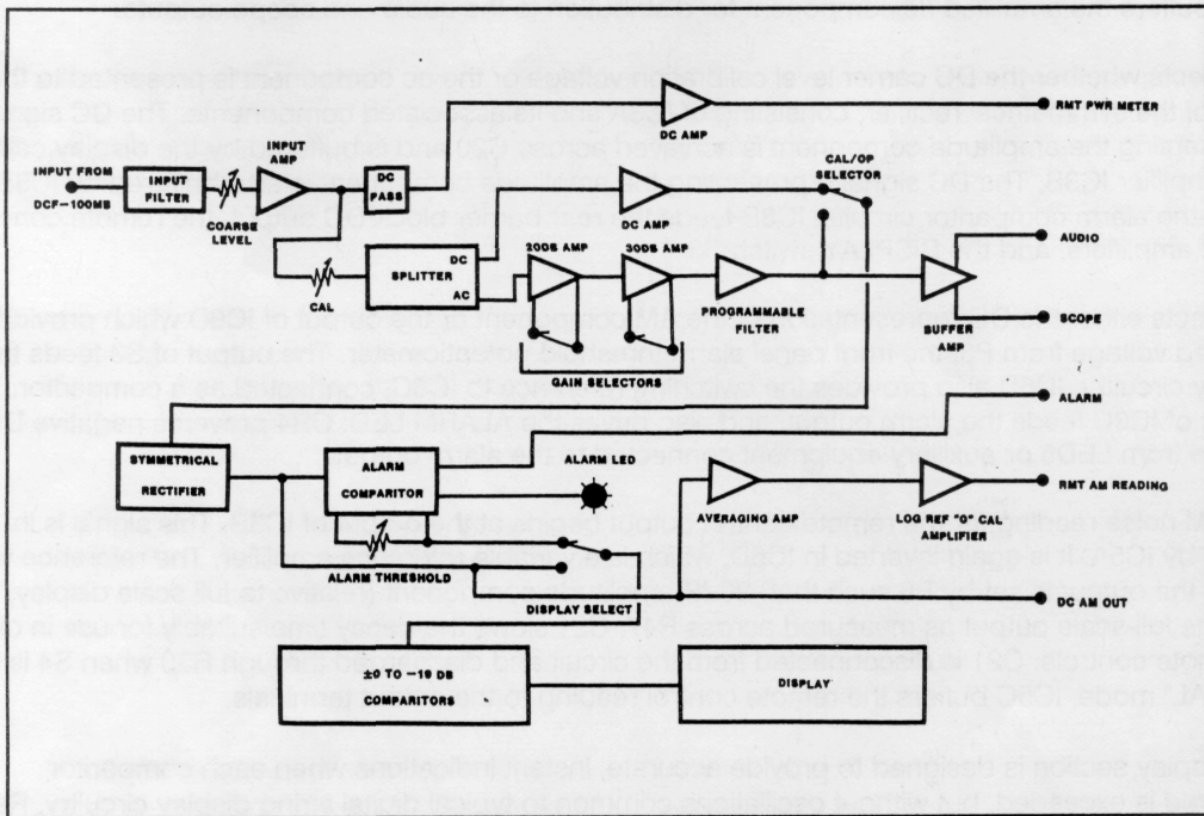
S4 selects whether the DC carrier level calibration voltage or the ac component is presented to the input of the symmetrical rectifier, consisting of IC3A and its associated components. The DC signal representing the amplitude component is achieved across C20 and is buffered by the display calibration amplifier IC3B. The DC signal representing the amplitude component is also buffered by IC6B for use in the alarm comparator circuits. IC3B feeds the rear barrier block DC output, the remote control output amplifiers, and the DISPLAY switch S3.

S3 selects either the DC representation of the AM component or the output of IC6D which provides a buffered voltage from P3, the front panel alarm threshold potentiometer. The output of S3 feeds the display circuitry. IC6D also provides the switching reference to IC6C, connected as a comparator. The output of IC6C feeds the alarm output, and also drives the ALARM LED. CR4 prevents negative DC voltage from LED5 or auxiliary equipment connected to the alarm output.

The AM noise reading for the remote control output begins at the output of IC3B. This signal is inverted by IC5A. It is again inverted in IC5D, which is a variable reference amplifier. The reference voltage at the output is set by P6 such that -20dB amplitude component (relative to full scale display) = 1/10 the full-scale output as measured across R47. C21 slows the decay time suitably for use in digital remote controls. C21 is disconnected from the circuit and discharged through R30 when S4 is in the "CAL" mode. IC5C buffers the remote control reading to the output terminals.

The display section is designed to provide accurate, instant indications when each comparator threshold is exceeded, but without oscillations common to typical digital string display circuitry. Reference voltages are determined by R98 through R122 voltage dividers. These voltages are buffered by IC7 through IC11. IC12 through IC16 function as comparators to drive the front panel LEDs. CR9 through CR28 protect the LED string from negative voltages. Power is stepped down from either 115v or 230V source through T1. CR5,6,7,8 rectify the AC in a full-wave bridge configuration. Voltage regulation is provided by VR1 and VR2, which are 18vdc regulators, positive and negative respectively.

# SPECIFICATIONS and BLOCK DIAGRAM



## Typical Performance:

Input/Output Connector Type:	BNC
Maximum Input Signal:	30v (combined filtered carrier + AM)
Measurement Range:	-20dB to -69 dB Front Panel Display -10 dB to -90 dB Front Panel Scope Jack Output
Residual Noise:	<95 dB below 100% AM
Oscilloscope Jack:	BNC 5v p-p for full scale display
Audio Output:	+4 dBv, 100 Ohm source impedance
THD of Recovered AM component:	<0.03%
Remote Metering Outputs:	
DC Output:	DC level representing significant synchronous AM
Power Metering:	DC level representing transmitter power; 12 vdc=100%
Remote Reading AM noise:	Continuously averaged damped DC output for remote control reading (analog or digital) of AM component calibrated to cover the 20dB display range selected
Alarm Output:	Normally low. Provides a +15 vdc signal when user determined alarm threshold has been exceeded (Note: If contact closure is desired, use RDL's ST-LCR1 logic interface)
Dimensions:	1 3/4" x 6" x 19"
Power Requirements:	115/230v 50/60 Hz, 30 Watts International power cords available
<b>Response Bandwidth:</b>	
ACM Standard:	+/- 1.5 dB 10 Hz - 70 KHz
High Pass Rolloff:	-1dB @ 2 KHz -2.8 dB @ 1 KHz -4.5 dB @ 720 Hz -9.5 dB @ 360 KHz
De-emphasized:	75 μS
Display Ranges:	-20 dB to -39 dB -30 dB to -49 dB -40 dB to -59 dB -50 dB to -69 dB

## DCF-100MB

Input Impedance:	50 Ohms		
Input Sample Signal Requirement:	<u>Attenuation of Sample</u>	<u>Min TPO</u>	<u>Max TPO</u>
	60 dB	44 Kw	1000 Kw
	55 dB	14 Kw	315 Kw
	50 dB	4.4 Kw	100 Kw
	45 dB	1.4 Kw	31Kw
	40 dB	440W	10Kw

## ACM-2 MAINTENANCE REPLACEABLE PARTS LIST

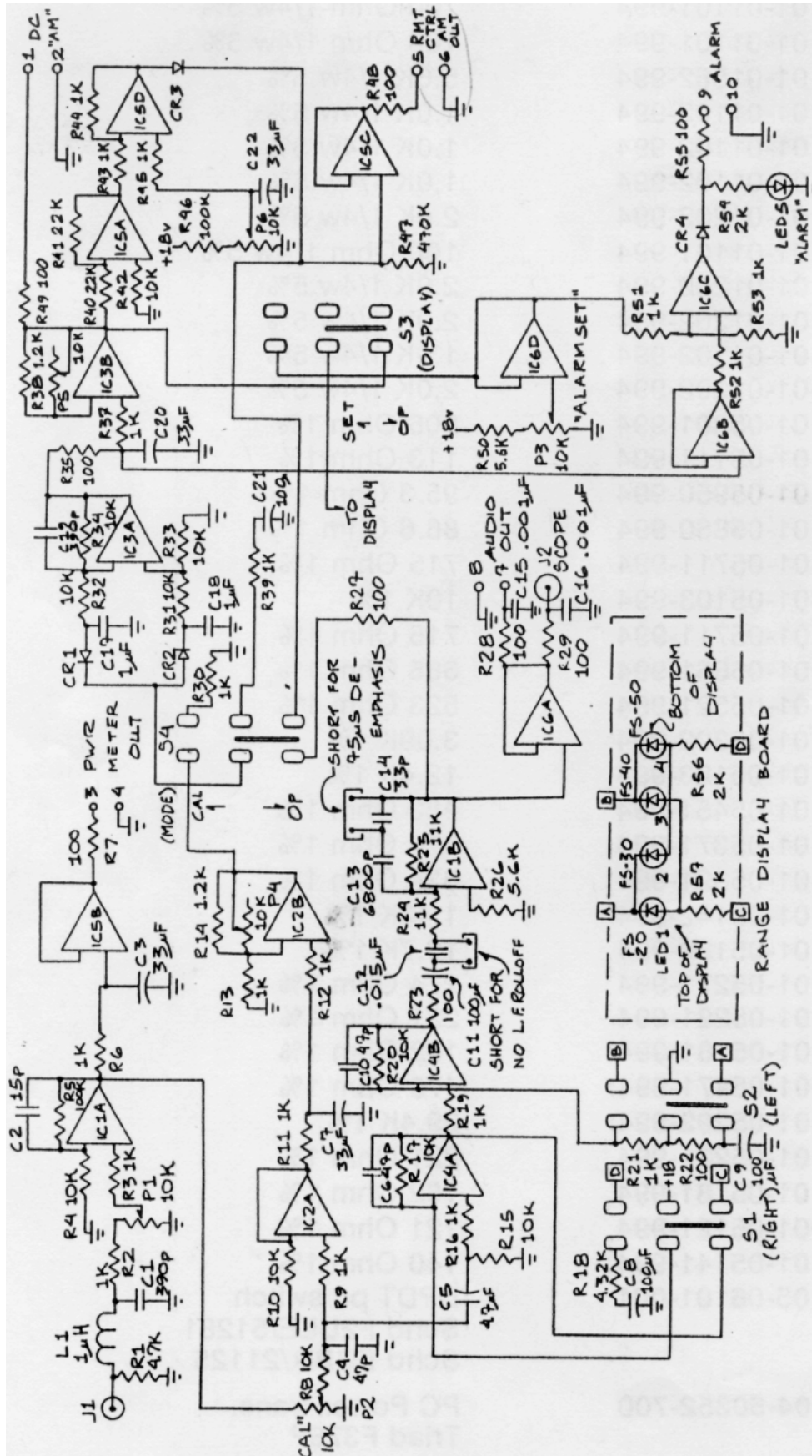
_	<u>Designation</u>	<u>RDL Part No.</u>	<u>Description</u>
C	1	02-07391-102	390pf 1kv Cer Disc
C	2	02-08150-050	15pf50vNPO
C	3	02-01330-050	33µF 50v Alumelec
C	4	02-07470-102	47pf 1kv Cer Disc
C	5	02-01050-035	4.7µF 35v Alumelec
C	6	02-07470-102	47pf 1kv Cer Disc
C	7	02-01330-050	33µF 50v Alumelec
C	8	02-01101-050	100µF 50v Alumelec
C	9	02-01101-050	100µF 50v Alumelec
C	10	02-07470-102	47pf 1kv Cer Disc
C	11	02-01101-050	100µF 50v Alumelec
C	12	02-08153-050	.015µF50vNPO
C	13	02-10682-050	.0068µF 50v NPO
C	14	02-08330-050	33pf 50v NPO
C	15	02-07102-050	.001 µF 50V Cer Disc
C	16	02-07102-050	.001 µF 50V Cer Disc
C	17	02-08105-050	1.0 µF 50V Monocap
C	18	02-08105-050	1.0 µF 50V Monocap
C	19	02-07391-102	390pf 1kv Cer Disc
C	20	02-01330-050	33µF 50v Alumelec
C	21	02-01101-050	100µF 50v Alumelec
C	22	02-01330-050	33µF 50v Alumelec
C	23	02-01222-035	2200µF 35v Alumelec
C	24	02-01222-035	2200µF 35v Alumelec
C	25-46	02-12104-050	0.1µF 50v Mono Z5U
CR	1-28	07-50001-100	1N4001
F	1	15-01938-101	Fuse .375A 250V SloBlo
FC	1-2	15-02001-001	Fuseclip LF102069
1C	1-4	06-01001-001	NE5532P
1C	5-16	06-01003-001	LM348N
J	1-2	03-07005-000	BNC PanelJack
KN	1-2	10-04005-004	Round knob-ACM2 Selco3/02TPN 110-006
LED	1-25	07-80101-901	Red Led w/Holder LumexSSF-LXH103ID
P	1	01-10103-994	IOK trimpot Piher PT-10V-10K
P	2-3	01-09103-001	10K Piher panel pot PT15WB10K

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P	4-6	01-10103-994	IOK trimpot Piherr PT-10V-10K
R	1	01-01472-994	4.7K ¼w 5%
R	2	01-01102-994	1.0K ¼w 5%
R	3	01-01102-994	1.0K ¼w 5%
R	4	01-01103-994	10K¼w 5%
R	5	01-01104-994	100K ¼w 5%
R	6	01-01102-994	1.0K ¼w 5%
R	7	01-01101-994	100 Ohm ¼w 5%
R	8	01-01103-994	10K ¼w 5%
R	9	01-01102-994	1.0K ¼w 5%
R	10	01-01103-994	10K ¼w 5%
R	11	01-01102-994	1.0K ¼w 5%
R	12	01-01102-994	1.0K ¼w 5%
R	13	01-01102-994	1.0K ¼w 5%
R	14	01-01122-994	1.2K ¼w 5%
R	15	01-01103-994	10K ¼w 5%
R	16	01-01102-994	1.0K ¼w 5%
R	17	01-05103-994	10K 1%
R	18	01-05440-994	4.32KOhm1%
R	19	01-01102-994	1.0K¼w5%
R	20	01-05103-994	10K 1%
R	21	01-05102-994	1.0K1%
R	22	01-05902-994	90.9 Ohm 1%
R	23	01-01101-994	100 Ohm ¼w 5%
R	24	01-05113-994	11.0K1%
R	25	01-05113-994	11.0K1%
R	26	01-01562-994	5.6K ¼w 5%
R	27	01-01101-994	100Ohm¼w5%
R	28	01-01101-994	100 Ohm ¼w 5%
R	29	01-01101-994	100Ohm¼w5%
R	30	01-01102-994	1.0K¼w5%
R	31	01-05103-994	10K1%
R	32	01-05103-994	10K1%
R	33	01-05103-994	10K 1%
R	34	01-05103-994	10K1%
R	35	01-01101-994	100 Ohm ¼w 5%
R	36	01-01102-994	1.0K¼w5%
R	37	01-01102-994	1.0K¼w5%
R	38	01-01122-994	1.2K¼w5%
R	39	01-01102-994	1.0K¼w5%
R	40	01-01223-994	22K ¼w 5%
R	41	01-01223-994	22K ¼w 5%
R	42	01-01103-994	10K¼w5%
R	43	01-01102-994	1.0K¼w5%
R	44	01-01102-994	1.0K¼w5%

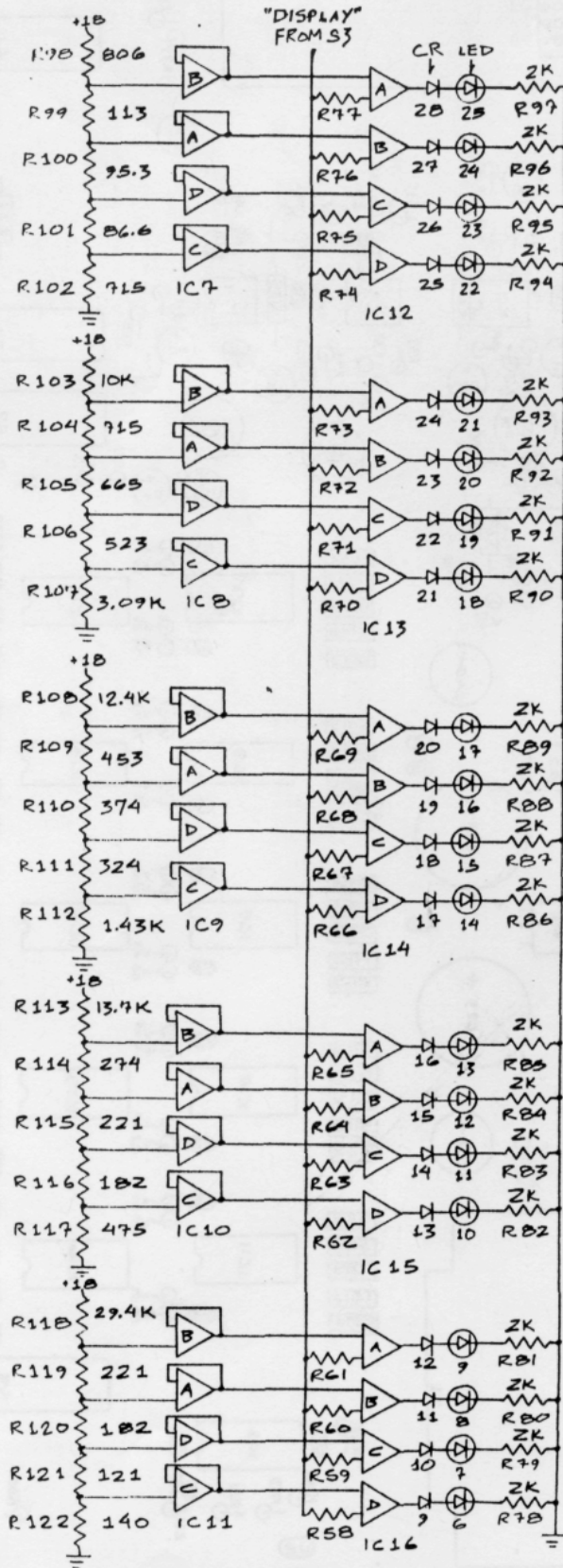
R	45	01-01102-994	1.0K $\frac{1}{4}$ w5%
R	46	01-01104-994	100K $\frac{1}{4}$ W5%
R	47	01-01474-994	470K $\frac{1}{4}$ w 5%
R	48	01-01101-994	100 Ohm $\frac{1}{4}$ w 5%
R	49	01-01101-994	100 Ohm $\frac{1}{4}$ w 5%
R	50	01-01562-994	5.6K $\frac{1}{4}$ w 5%
R	51	01-01102-994	1.0K $\frac{1}{4}$ w5%
R	52	01-01102-994	1.0K $\frac{1}{4}$ w5%
R	53	01-01102-994	1.0K $\frac{1}{4}$ w5%
R	54	01-01202-994	2.0K $\frac{1}{4}$ w 5%
R	55	01-01101-994	100 Ohm $\frac{1}{4}$ w 5%
R	56	01-01202-994	2.0K $\frac{1}{4}$ w 5%
R	57	01-01202-994	2.0K $\frac{1}{4}$ w 5%
R	58-77	01-01102-994	1.0K $\frac{1}{4}$ w5%
R	78-97	01-01202-994	2.0K $\frac{1}{4}$ w 5%
R	98	01-05801-994	806 Ohm 1%
R	99	01-05111-994	1130hm1%
R	100	01-05950-994	95.3 Ohm 1%
R	101	01-05860-994	86.6 Ohm 1%
R	102	01-05711-994	715 Ohm 1%
R	103	01-05103-994	10K 1%
R	104	01-05711-994	715 Ohm 1%
R	105	01-05661-994	665 Ohm 1%
R	106	01-05521-994	523 Ohm 1%
R	107	01-05302-994	3.09K 1%
R	108	01-05123-994	12.4K 1%
R	109	01-05451-994	453 Ohm 1%
R	110	01-05371-994	374 Ohm 1%
R	111	01-05321-994	324 Ohm 1%
R	112	01-05142-994	1.43K1%
R	113	01-05132-994	13.7K1%
R	114	01-05271-994	274 Ohm 1%
R	115	01-05221-994	221 Ohm 1%
R	116	01-05181-994	182Ohm1%
R	117	01-05471-994	475 Ohm 1%
R	118	01-05292-994	29.4K 1%
R	119	01-05221-994	221 Ohm 1%
R	120	01-05181-994	182Ohm1%
R	121	01-05121-994	121 Ohm 1%
R	122	01-05141-994	140 Ohm 1%
S	1-4	05-06101-001	DPDT pc switch Schd F2UEE/51281 Schd FGBIk/21125
T	1	04-50352-700	PC Power trans. Triad F376P



# ACM-2 SCHEMATIC Sheet 1

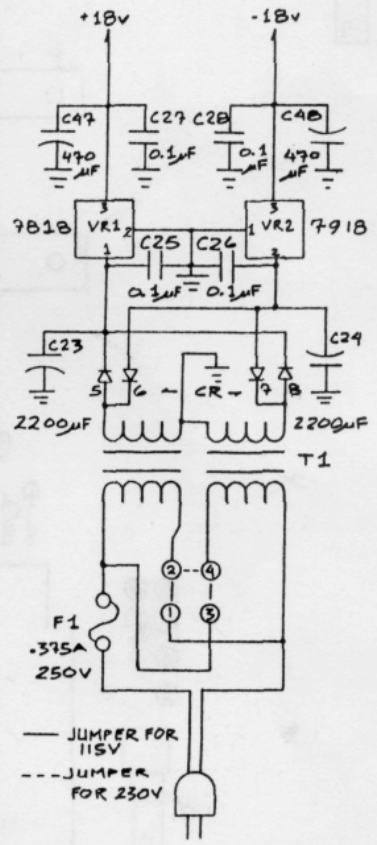


# ACM-2 SCHEMATIC Sheet 2

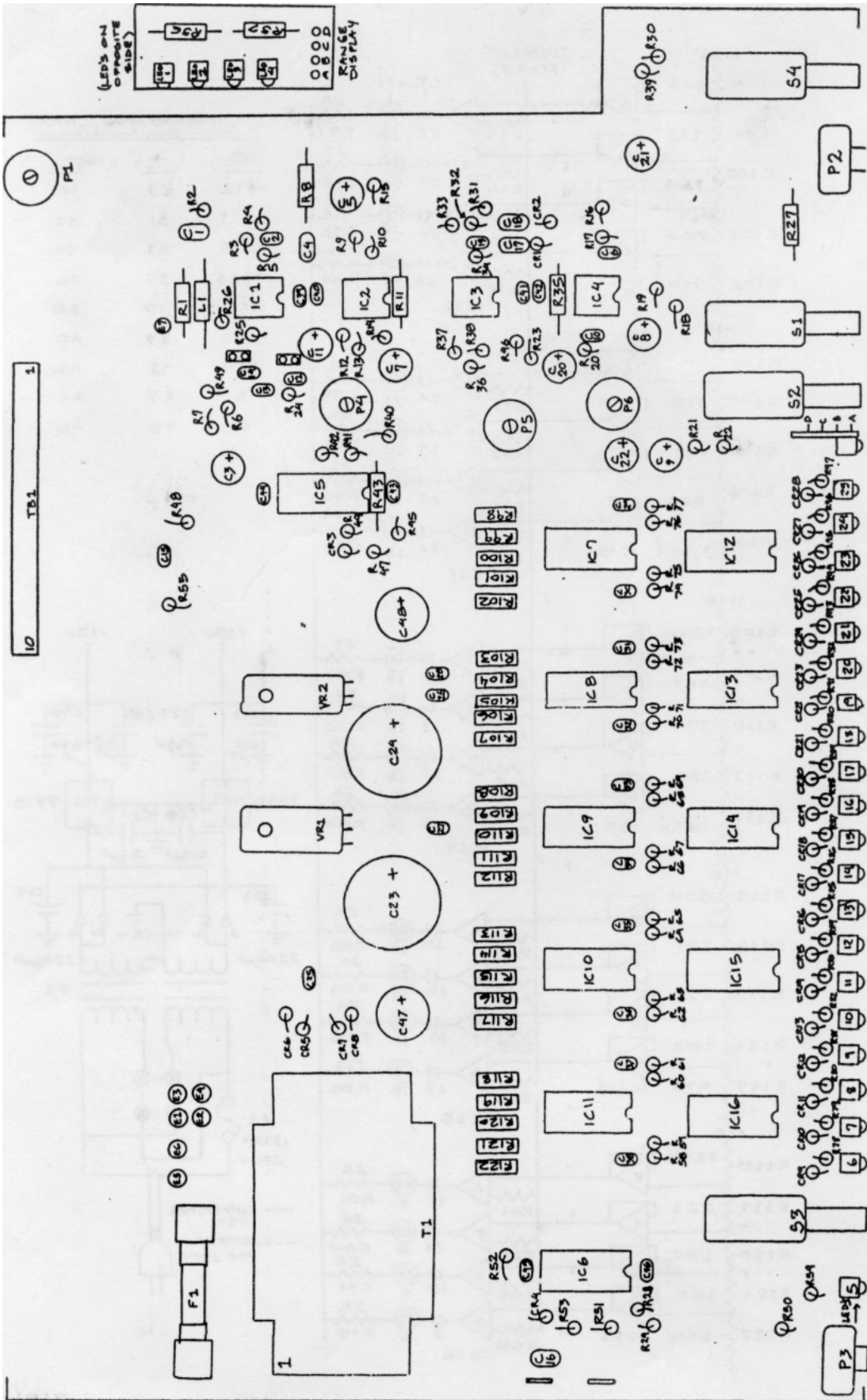


## IC DECOUPLING CAPS

IC	+	-
7#12	29	30
8#13	31	32
9#14	33	34
10#15	35	36
11#16	37	38
1#2	39	40
3#4	41	42
5	43	44
6	45	46



# ACM-2 ASSEMBLY DIAGRAM



## AM NOISE, Remote Control Readings

Decibel Conversion Chart Scale: 0 to 100		Decibel Conversion Chart Scale: 0 to 1000		Decibel Conversion Chart Scale: 0 to 10	
<u>Reading</u> For a Remote Control Reading of:	<u>AM Noise</u> Add- _____ to the number in this column	<u>Reading</u> For a Remote Control Reading of:	<u>AM Noise</u> Add- _____ to the number in this column	<u>Reading</u> For a Remote Control Reading of:	<u>AM Noise</u> Add- _____ to the number in this column
100.0	0	1000	0	10.00	0
89.1	-1	891	-1	8.91	-1
79.4	-2	794	-2	7.94	-2
70.8	-3	708	-3	7.08	-3
63.1	-4	631	-4	6.31	-4
56.2	-5	562	-5	5.62	-5
50.1	-6	501	-6	5.01	-6
44.7	-7	447	-7	4.47	-7
39.8	-8	398	-8	3.98	-8
35.5	-9	355	-9	3.55	-9
31.6	-10	316	-10	3.16	-10
28.2	-11	282	-11	2.82	-11
25.1	-12	251	-12	2.51	-12
22.4	-13	224	-13	2.24	-13
20.0	-14	200	-14	2.00	-14
17.8	-15	178	-15	1.78	-15
15.8	-16	158	-16	1.58	-16
14.1	-17	141	-17	1.41	-17
12.6	-18	126	-18	1.26	-18
11.2	-19	112	-19	1.12	-19
10.0	-20	100	-20	1.00	-20