Engineering Thermodynamics Solutions Manual

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Foreword

Title - Engineering Thermodynamics - Solutions Manual

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Thermodynamics is an essential subject in the study of the behaviour of gases and vapours in real engineering applications.

This book is a complimentary follow up for the book "Engineering Thermodynamics" also published on BOOKBOON, presenting the solutions to tutorial problems, to help students to check if their solutions are correct; and if not, to show how they went wrong, and change it to get the correct answers.

This solutions manual is a small book containing the full solution to all tutorial problems given in the original book which were grouped in chapter four, hence the sections of this addendum book follows the format of the textbook, and it is laid out in three sections as follows:

4.1 First Law of Thermodynamics N.F.E.E Applications

In this section there are 6 tutorial problems

4.2 First Law of Thermodynamics S.F.E.E Applications

In this section there are 5 tutorial problems

4.3 General Thermodynamics Systems

In this section there are 15 tutorial problems

First Law of Thermodynamics 4.1 **N.F.E.E** Applications

1. In a non-flow process there is heat transfer loss of 1055 kJ and an internal energy increase of 210 kJ. Determine the work transfer and state whether the process is an expansion or compression.

[Ans: -1265 kJ, compression]

Solution:

Closed system for which the first law of Thermodynamics applies,

Q - W = ΔU

1055 - W = 210

Hence the work done can be found as:

W = -1265 kJ

Since negative, it must be work input, ie compression.

2. In a non-flow process carried out on 5.4 kg of a substance, there was a specific internal energy decrease of 50 kJ/kg and a work transfer from the substance of 85 kJ/kg. Determine the heat transfer and state whether it is gain or loss.

[Ans: 189 kJ, gain]

Solution:

Closed system for which the first law of Thermodynamics applies,

Q - W =
$$\Delta U$$

Q =
$$\Delta U + W$$

= 5.4x (-50) +5.4 x 85
= + 189 kJ,

Since Q is positive, it implies heat is entering the control volume, ie Gain.

3. During the working stroke of an engine the heat transferred out of the system was 150 kJ/kg of the working substance. If the work done by the engine is 250 kJ/kg, determine the change in internal energy and state whether it is decrease or increase.

[Ans: -400 kJ/kg, decrease]

Solution:

Closed system for which the first law of Thermodynamics applies,

Q - W = ΔU

Hence

 $\Delta U = Q - W$ = (-150) - 250 = -400 kJ/kg

Since the sign is negative, there is a decrease in internal energy.

4. Steam enters a cylinder fitted with a piston at a pressure of 20 MN/m² and a temperature of 500 deg C. The steam expands to a pressure of 200 kN/m² and a temperature of 200 deg C. During the expansion there is a net heat loss from the steam through the walls of the cylinder and piston of 120 kJ/kg. Determine the displacement work done by one kg of steam during this expansion.

[Ans: 168.6 kJ/kg]

Solution:

State 1 at 20 MPa, 500 C: u = 2942.9 kJ/kg

State 2 at 200 kPa, 200C: u = 2654.4 kJ/kg

Closed system for which the first law of Thermodynamics applies,

Q - W = ΔU

Rearranging to determine the work done:

 $W = Q - \Delta U = (-120) - (2654.4 - 2942.9) = 168.5 \text{ kJ/kg}$

5. A closed rigid system has a volume of 85 litres contains steam at 2 bar and dryness fraction of 0.9. Calculate the quantity of heat which must be removed from the system in order to reduce the pressure to 1.0 bar. Also determine the change in enthalpy and entropy per unit mass of the system.

[Ans: -38 kJ]

Solution:

Closed system for which the first law of Thermodynamics applies,

-	p = 0.2 MPa (120.23 C)				
'	v	u	h	s	
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K	
Sat. liquid	0.00106	504.5	504.7	1.5300	
Sat. vapour	0.8857	2529.5	2706.7	7.1272	

Q - W = ΔU

For a rigid system W=0,

hence $Q = \Delta U$

At 2bar, x=0.9, the properties are:

Hence:

h = hf + x.(hg-hf) = 504.7 + 0.9 (2706.7 - 504.7) = 2486.5 kJ/kg

u = uf + x.(ug - uf) = 504.5 + 0.9 (2529.5-504.5) = 2327.0 kJ/kg

v = vf + x.(vg - vf) = 0.00106 + 0.9 (0.8857 - 0.00106) = 0.797 kJ/kg

mass = volume/specific volume = 85 litres x $10^{-3} / 0.797 = 0.1066$ kg

-	p = 0.10 MPa (99.63 C)				
	v	u	h	S	
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K	
Sat. liquid	0.00104	417.3	417.4	1.3030	
Sat. vapour	1.694	2506.1	2675.5	7.3594	

at 1 bar

v = vf + x.(vg - vf)x = (v-vf)/(vg-vf) = (0.797-0.00104)/(1.694-0.00104) = 0.470h = 417.4 + 0.470 (2675.5 - 417.4) = 1479.06 kJ/kgu = 417.3 + 0.470 (2506.1 - 417.3) = 1399.36 kJ/kg

Q = m (u2-u1) = 0.1066 x (2327.0 - 1399.36) = 98.9 kJ not the answer given in the text, please

2 kg of air is heated at constant pressure of 2 bar to 500 °C. Determine the initial temperature and 6. the change in its entropy if the initial volume is 0.8 m³.

[Ans: 2.04 kJ/kgK]

Solution:

$$T_{1} = \frac{P_{1}xV_{1}}{mxR}$$
$$= \frac{2x10^{5}x0.8}{2x287}$$
$$= 278.746 K$$
$$\Delta S = m.Cp.\ln\frac{T_{2}}{T_{1}}$$
$$= 2x1005x\ln\frac{500 + 273}{278.7}$$

= 2.05 kJ / kgK

278.7

accept this as the correct answer.

First Law of Thermodynamics 4.2 S.F.E.E Applications

1. A boiler is designed to work at 14 bar and evaporate 8 kg/s of water. The inlet water to the boiler has a temperature of 40 deg C and at exit the steam is 0.95 dry. The flow velocity at inlet is 10 m/s and at exit 5 m/s and the exit is 5 m above the elevation at entrance. Determine the quantity of heat required. What is the significance of changes in kinetic and potential energy on the result?

[Ans: 20.186 MW]

Solution:

1. SFEE:
$$Q - W = m[(h_2 - h_1) + \frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1)]$$

W =0 (since constant pressure process),

ignoring Δke and ΔPe : the SFEE reduces to

 $Qs = m_s (h_2 - h_1)$

State 1- h₁ is hf at T=40C, closest to this is Ts=45, h1=191.83 kJ/kg

State 2, $h=h_f+0.95h_{fg}$ at 14 bar.

 $h_2 = 830.30 + 0.95 \times 1959.7 = 2692 \text{ kJ/kg}$

hence

 $Qs = m_s (h_2 - h_1) = 8 x(2692 - 191.83) = 2000136 kW = 20 MW$

2. Taking into account changes in KE and PE

The KE and PE contribution is calculated

$$X = m[\frac{V_2^2 - V_1^2}{2}] + g(Z_2 - Z_1)]$$

= $8x[\frac{5^2 - 10^2}{2000} + 9.81x(\frac{5}{1000})]$
= $-0.3 + 0.049$
= $-0.251 \, kW$

This is tiny (0.001%) in comparison to 20 MW.

2. Steam flows along a horizontal duct. At one point in the duct the pressure of the steam is 1 bar and the temperature is 400°C. At a second point, some distance from the first, the pressure is 1.5 bar and the temperature is 500°C. Assuming the flow to be frictionless and adiabatic, determine whether the flow is accelerating or decelerating.

[Ans: Decelerating]

Solution:

Q - W = m[(h₂ - h₁) + $\frac{V_2^2 - V_1^2}{2}$ + g (z₂ - z₁)] 1. SFEE :

W =0 (since constant pressure process),

Q = 0 adiabatic

PE = 0 horizontal layout

Hence

$$(\mathbf{h}_2 - \mathbf{h}_1) = -\frac{V_2^2 - V_1^2}{2}$$



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Find enthalpy values at 1 and 2:

State 1- 1.0 bar and the temperature is 400°C, hence $h_1 = 3263.9 \text{ kJ/kg}$

State 2- 1.5 bar and the temperature is 500°C, $h_2 = 3473 \text{ kJ/kg}$

 $(h_2 - h_1) = 3473 - 3263.9 = 209.1 \text{ kJ/kg}$ Hence

Since this is positive, then $V_1 > V_2$ ie decelerating

Steam is expanded isentropically in a turbine from 30 bar and 400°C to 4 bar. Calculate the work 3. done per unit mass flow of steam. Neglect changes in Kinetic and Potential energies.

[Ans: 476 kJ/kg]

Solution:

1. SFEE:
$$Q - W = m[(h_2 - h_1) + \frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1)]$$

Q = 0 isentropic expansion

KE=PE = 0

Hence $W = m[(h_2 - h_1)]$

State 1- 30 bar and the temperature is 400°C,

-	<i>p</i> = 3.00 MPa (233.90 C)				
,	v	u	h	S	
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K	
Sat. liquid	0.001216	1004.8	1008.4	2.6457	
Sat. vapour	0.06668	2604.1	2804.2	6.1869	
400	0.09936	2932.8	3230.9	6.9212	

Hence

 $h_1 = 3230.9 \text{ kJ/kg},$

 $s_1 = 6.9212 \text{ kJ/kgK}$

Expanding at constant entropy, to 4 bar,

Slightly superheated,

h₂= 2750 kJ/kg (approximately)

-	<i>p</i> = 0.40 MPa (143.63 C)					
'	v	u	h	s		
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K		
Sat. liquid	0.00108	604.3	604.7	1.7766		
Sat.Vapour	0.4625	2553.6	2738.6	6.8959		
150	0.4708	2564.5	2752.8	6.9299		
200	0.5342	2646.8	2860.5	7.1706		

Hence

$$W = m (h_2 - h_1)$$

= 1x(3230.9 - 2750)
= 480.9 kJ/kg

4. A compressor takes in air at 1 bar and 20°C and discharges into a line. The average air velocity in the line at a point close to the discharge is 7 m/s and the discharge pressure is 3.5 bar. Assuming that the compression occurs isentropically, calculate the work input to the compressor. Assume that the air inlet velocity is very small.

[Ans: -126.6 kW/kg]

Solution:

Q - W = m[(h₂ - h₁) +
$$\frac{V_2^2 - V_1^2}{2}$$
 + g (z₂ - z₁)]

Assume adiabatic condition, Q=0, and horizontally mounted, (PE=0), SFEE reduces to

$$-W = m[Cp(T_2 - T_1) + \frac{V_2^2 - V_1^2}{2}]$$
$$T_2 = T_1 \left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}} = 293 \left(\frac{3.5}{1}\right)^{\frac{0.4}{1.4}} = 419.1K$$

$$\frac{W}{m} = -[1005(419.1 - 293) + \frac{7^2 - 0}{2}]$$

$$= -[126728 + 24.5]$$

$$= -126.7 \ kW / kg$$

5. Air is expanded isentropically in a nozzle from 13.8 bar and 150°C to a pressure of 6.9 bar. The inlet velocity to the nozzle is very small and the process occurs under steady-flow, steady-state conditions. Calculate the exit velocity from the nozzle knowing that the nozzle is laid in a horizontal plane and that the inlet velocity is 10 m/s.

[Ans: 390.9 m/s]



Solution:

The situation is an open system for which the SFEE applies:

$$Q - W = m \left[C_p (T_2 - T_1) + \frac{V_2^2 - V_1^2}{2} + g(Z_2 - Z_1) \right]$$

Q = 0 adiabatic

$$g(Z_2 - Z_1) = 0 \text{ (Assumed)}$$

And W=0 no moving parts

Hence SFEE reduces to $0 = m \left[C_p (T_2 - T_1) + \frac{V_2^2 - V_1^2}{2000} \right]$

$$T_2 = T_1 \left(\frac{P_2}{P_1}\right)^{\frac{n-1}{n}} = (273 + 150)x \left(\frac{6.9}{13.8}\right)^{\frac{0.4}{1.4}} = 347K$$

The SFEE can now be used to determine the mass flow rate

$$0 = m \left[1.005(347 - 423) + \frac{V_2^2 - 10^2}{2000} \right]$$

m = 1
hence
 $V_2 = \sqrt{100 + 2000x1.005x76} = 390 \text{ m/s}$

4.3 General Thermodynamics Systems

1. A rotary air compressor takes in air (which may be treated as a perfect gas) at a pressure of 1 bar and a temperature of 20°C and compresses it adiabatically to a pressure of 6 bar. The isentropic efficiency of the processes is 0.85 and changes in kinetic and potential energy may be neglected. Calculate the specific entropy change of the air. Take R = 0.287 kJ/kg K and $C_p = 1.006 \text{ kJ/kg K}$.

[Ans: 0.07 kJ/kg K]

Solution:

Closed system for which the first law of Thermodynamics applies,

 $dQ - dW = \Delta U$ dQ = T.dS;dW = -pdV; Cv = du/dT,Hence Tds - pdV = Cv.dTdS = (P/T)dV + Cv(dT/T)integrating $(S_2-S_1)=R \ln(V_2/V_1) + Cv \ln(T_2/T_1)$ For isentropic process $V_{2}/V_{1} = (P_{1}/P_{2})^{1/n}$ $T_{2}/T_{1} = (P_{2}/P_{1})^{(n-1)/n}$ Hence $S_2 - S_1 = R \ln(P_1/P_2) \wedge 1/n + Cv \ln(T_2/T_1)$ $T2s = T2 (P2/P1)^{(1-n)}/n = 488.5 K$ T2 = T1 + (T2s-T1)/effc = 293 + (488.5-293)/0.85 = 523 K $S_2 - S_1 = R \ln(P_1/P_2) \wedge 1/n + Cv \ln(T_2/T_1)$ $S_2-S_1=0.287 \text{xln}(1/6)^{(1/1.4)} + (1.006-0.287) \ln(523/293)$ = -0.3673 + 0.4166= 0.05 kJ/kgK

Very small quantity, note that if the process is 100% isentropic, the change in entropy would be zero.

- 2. An air receiver has a capacity of 0.86m³ and contains air at a temperature of 15°C and a pressure of 275 kN/m². An additional mass of 1.7 kg is pumped into the receiver. It is then left until the temperature becomes 15°C once again. Determine,
 - a) the new pressure of the air in the receiver, and
 - b) the specific enthalpy of the air at 15°C if it is assumed that the specific enthalpy of the air is zero at 0°C.

Take $C_p = 1.005 \text{ kJ/kg}$, $C_v = 0.715 \text{ kJ/kg}$ K

[Ans: 442 kN/m², 15.075 kJ/kg]

Solution:

$$m_{1} = \frac{PV}{RT}$$

$$= \frac{275 \times 10^{3} \times 0.86}{(2005 - 715) \times 288}$$

$$= 2.8316 \ kg$$
added
$$dm = 1.7 \ kg$$
hence
$$m_{2} = m_{1} + dm = 2.8316 + 1.7 = 4.5316 \ kg$$

$$P_2 = \frac{mRT_2}{V}$$
$$= \frac{4.5316x (2005 - 715)x 288}{0.86}$$

= 440 kPa

b) h = Cp.dT = 1005 x(288-273) = 15.075 kJ/kg.

- 3. Oxygen has a molecular weight of 32 and a specific heat at constant pressure = 0.91 kJ/kg K.
 - a) Determine the ratio of the specific heats.
 - b) Calculate the change in internal energy and enthalpy if the gas is heated from 300 to 400 K.

[Ans: 1.4, 65 kJ/kg, 91 kJ/kg]

Solution:

- a) $R = \frac{\text{Ro}}{\text{M}} = \frac{8314.3}{32} = 0.2598 \, kJ/kgK$
 - Cv = Cp R = 0.91 0.2598 = 0.65 kJ/kgK

n = Cp/Cv = 0.91 / 0.65 = 1.3996

b) du = Cv (T2-T1) = 0.65 (400 - 300) = 65 kJ/kg



- **4.** A steam turbine inlet state is given by 6 MPa and 500°C. The outlet pressure is 10 kPa. Determine the work output per unit mass if the process:
 - a) is reversible and adiabatic (ie 100% isentropic),
 - b) such that the outlet condition is just dry saturated,
 - c) such that the outlet condition is 90% dry.

[Ans: 1242.7 kJ/kg, 837.5 kJ/kg, 1076.8 kJ/kg]

Solution:

a) when 100% isentropic $h_1 = 3422.2 \text{ kJ/kg}$, $S_1=6.8803 \text{ kJ/kgK}$ $S_{2'} = s_1 \text{ and } x_2$ is found using

Then $6.8803 = 0.6493 + x_{y}$ (7.5009), from which $x_{y} = 0.8307$

Thus $h_2 = h_f + x h_{fg} = 191.83 + 0.8307 x 2392.87 = 2179.6 kJ/kg$

Hence W = h₁ - h₂ = 3422.2 - 2179.6 = 1242.6 kJ/kg

b) if x=1, $h_2 = 2584.7 \text{ kJ/kg}$ $W = h_1 - h_2 = 3422.2 - 2584.7 = 837.5 \text{ kJ/kg}$

c) if x=0.9 $h_2 = h_f + x h_{fg} = 191.83 + 0.9 x 2392.87 = 2345.4 kJ/kg$

Hence W = h₁ - h₂ = 3422.2 - 2345.4 = 1076.8 kJ/kg

5. Determine the volume for carbon dioxide contained inside a cylinder at 0.2 MPa, 27°C:-

- a) assuming it behaves as an ideal gas
- b) taking into account the pressure and volume associated with its molecules

[Ans: 0.2833m³/kg]

Substance	Chemical	Molar Mass M	Gas constant R	Critical Temp TC	Critical Pressure PC (MPa)		r Waals tants
Substance	Formula	(kg/kmol)	(J/kgK)	(K)		а	b
Carbon Dioxide	CO ₂	44.01	188.918	304.20	7.386	188.643	0.00097

Solution:

a) Assuming perfect gas behaviour:

$$R = \frac{Ro}{M} = \frac{8314.3}{44} = 188.96$$
$$V = \frac{mRT}{P}$$
$$= \frac{1x188.96x300}{0.2x10^6}$$
$$= 0.2834 \ m^3 \ / \ kg$$

b) using Van Der Vaal's equation

$$P = \frac{RT}{v - b} - \frac{a}{v^2}$$
$$0.2x10^6 = \frac{1889.96x300}{v - 0.00097} - \frac{188.643}{v^2}$$

solve

$$V = 0.2833 \, m^3 \, / \, kg$$

6. A cylindrical storage tank having an internal volume of 0.465 m³ contains methane at 20°C with a pressure of 137 bar. If the tank outlet valve is opened until the pressure in the cylinder is halved, determine the mass of gas which escapes from the tank assuming the tank temperature remains constant.

[Ans: 20.972 kg]

Solution:

$$R = \frac{Ro}{M} = \frac{8314.3}{16} = 519.644 \text{ J/kgK}$$
$$m_1 = \frac{PV}{RT}$$
$$= \frac{137 \times 10^5 \times 0.465}{519.644 \times 293}$$
$$= 41.841 \text{ kg}$$
$$P_2 = 0.5P_1$$
hence
$$m_2 = 0.5m_1 = 20.920 \text{ kg}$$
so

 $dm = 20.920 \ kg$

- 7. Find the specific volume for H_20 at 1000 kN/m² and 300°C by using:
 - a) the ideal gas equation assuming R = 461.5 J/kg K
 - b) steam tables

[Ans: 0.264m³/kg, 0.258 m³/kg]

a) for a perfect gas

Solution:

$$v = \frac{RT}{P}$$
$$= \frac{461.5x573}{1x10^6}$$

$$= 0.2644 \, m^3 \, / \, kg$$

b) using the steam Tables

V=0.2579 m³/kg

The difference = 2.4% under-estimation if assumed ideal gas.



- 8. Determine the specific volume of steam at 6 MPa using the steam tables for the following conditions:
 - a) dryness fraction x = 0
 - b) dryness fraction x = 0.5
 - c) dryness fraction x = 1
 - d) its temperature is 600°C

Sat. liq Sat. vap

т	p = 6.0 Mpa (257.64 deg-C)						
'	v	u	h	s			
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K			
Sat. liquid	0.00132	1205.4	1213.3	3.0267			
Sat. vapour	0.03244	2589.7	2784.3	5.8892			
300	0.03616	2667.2	2884.2	6.0674			
350	0.04223	2789.6	3043.0	6.3335			
400	0.04739	2892.9	3177.2	6.5408			
450	0.05214	2988.9	3301.8	6.7193			
500	0.05665	3082.2	3422.2	6.8803			
550	0.06101	3174.6	3540.6	7.0288			
600	0.06525	3266.9	3658.4	7.1677			
700	0.07352	3453.1	3894.2	7.4234			

4132.7

4375.3

4622.7

4875.4

5133.3

5396.0

7.6566

7.8727

8.0751

8.2661

8.4474

8.6199

[Ans: 0.001319, 0.01688, 0.03244, 0.06525 m³/kg]

Solution:

- a) v=vf=0.001319 m³/kg
- b) v=vf+X(vg-vf) =0.00132+0.5(0.03244-0.00132) $= 0.01688 \text{ m}^3/\text{kg}$

800

900

1000

1100

1200

1300

0.0816

0.08958

0.09749

0.10536

0.11321

0.12106

3643.1

3837.8

4037.8

4243.3

4454.0

4669.6

- c) $v=vg = 0.03244 \text{ m}^3/\text{kg}$
- d) v = 0.06525 m³/kg

9. Steam at 4 MPa, 400°C expands at constant entropy till its pressure is 0.1 MPa. Determine:

- a) the energy liberated per kg of steam
- b) repeat if the process is 80% isentropic

[Ans: 758 kJ/kg, 606 kJ/kg]

-	p = 4.0 MPa (250.4 deg C)					
T	v	u	h	S		
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K		
Sat. liquid	0.00125	1082.3	1087.3	2.7964		
Sat. vapour	0.04978	2602.3	2801.4	6.0701		
275	0.05457	2667.9	2886.2	6.2285		
300	0.05884	2725.3	2960.7	6.3615		
350	0.06645	2826.7	3092.5	6.5821		
400	0.07341	2919.9	3213.6	6.7690		

т	<i>p</i> = 0.10 MPa (99.63 C)					
1	v	u	h	S		
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K		
Sat. liquid	0.00104	417.3	417.4	1.3030		
Sat. vapour	1.694	2506.1	2675.5	7.3594		

Solution:

a) h₁ = 3213.6 kJ/kg, S1=6.769 kJ/kgK

$$X_{2} = \frac{S_{1} - S_{f}}{S_{g} - S_{f}} = \frac{6.7690 - 1.303}{7.3594 - 1.303} = 0.9024$$

 $h_2 = h_f + X_2(h_g - h_f) = 417.4 + 0.9024(2675.5 - 417.4) = 2455.4 \, kJ/kg$

 $W = h_1 - h_2 = 3213.6 - 2455.4 = 758.2 \text{ kJ/kg}$

b) if efficiency = 80%

W =
$$0.8(h_1 - h_2)$$

= $0.8(3213.6 - 2455.39)$
= 606.6 kJ/kg

- **10.** a) Steam (1 kg) at 1.4 MPa is contained in a rigid vessel of volume 0.16350 m³. Determine its temperature.
 - b) If the vessel is cooled, at what temperature will the steam be just dry saturated?
 - c) If cooling is continued until the pressure in the vessel is 0.8 MPa; calculate the final dryness fraction of the steam, and the heat rejected between the initial and the final states.

[Ans: 250°C, 188°C, 0.678; 8181 kJ]

Solution:

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a) at 1.4 MPa and v =0.16350 m³/kg, from steam tables, it can be verified that the condition of the fluid is superheated, at 250 C.

 $h_1 = 2927.2 \text{ kJ/kg}$

-	<i>p</i> = 1.40 MPa (195.07*C)					
· ·	v	u	h	S		
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K		
Sat. liquid	0.00115	828.7	830.3	2.2842		
Sat. Vapour	0.14084	2592.8	2790.0	6.4693		
200	0.14302	2603.1	2803.3	6.4975		
250	0.16350	2698.3	2927.2	6.7467		
300	0.18228	2785.2	3040.4	6.9534		

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b) now if the vessel is cooled, at constant volume, till x=1, then the temperature is equal to the saturation value at a new pressure of 1.2 MPa, T=Ts=187.99C

-	<i>p</i> = 1.20 МРа (187.99 С)				
'	v	u	h	s	
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K	
Sat. liquid	0.00114	797.3	798.6	2.2166	
Sat. vapour	0.16333	2588.8	2784.4	6.5233	

c) further cooling, to a reduced pressure of 0.8MPa, the fluid is in the wet region, as v lies between vf and vg at this pressure.

T	<i>p</i> = 0.80 MPa (170.43 C)				
'	v	u	h	S	
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K	
Sat. liquid	0.00111	720.2	721.1	2.0462	
Sat. vapour	0.2404	2576.8	2769.1	6.6628	

Then $0.16333 = 0.00111 + x_{2'}(0.2404 - 0.00111)$,

from which $x_{2'} = 0.678$

$$\begin{split} h_2 &= h_f + x \ h_{fg} \\ &= 721.1 + 0.678 x (2769.1 - 721.1) \\ &= 2109.5 \ kJ/kg \end{split}$$

h₁=2927.2 kJ/kg

Q = m (h1-h2) = 1x(2927.2-2109.5) = 818 kJ

11. Steam (0.05 kg) initially saturated liquid, is heated at constant pressure of 0.2 MPa until its volume becomes 0.0658 m³. Calculate the heat supplied during the process.

[Ans: 128.355 kJ]

Solution:

т	<i>p</i> = 0.2 MPa (120.23 C)			
	v	u	h	S
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K
Sat. liquid	0.00106	504.5	504.7	1.5300
Sat. vapour	0.8857	2529.5	2706.7	7.1272
150	0.9596	2576.9	2768.8	7.2795
200	1.0803	2654.4	2870.5	7.5066
250	1.1988	2731.2	2971.0	7.7086
300	1.3162	2808.6	3071.8	7.8926
400	1.5493	2966.7	3276.6	8.2218

at 0.2 MPa and x=0,

 $h_1 = 504.70 \text{ kJ/kg}$

 $v_2 = 0.0658 / 0.05 = 1.316 \text{ m}^3/\text{kg}$,

 $P_2 = 0.2 \text{ MPa},$ $h_2 = 3071.48 \text{ kJ/kg}$

hence the heat supplied during the process 1-2 is calculated as follows:

 $Q = m (h_1 - h_2)$ = 0.05x(3071.80 - 504.70) = 128.355 kJ **12.** Steam at 0.6 MPa and dryness fraction of 0.9 expands in a cylinder behind a piston isentropically to a pressure of 0.1 MPa. Calculate the changes in volume, enthalpy and temperature during the process.

[Ans: 1.1075 m³, -276 kJ/kg, -59°C]

Solution:

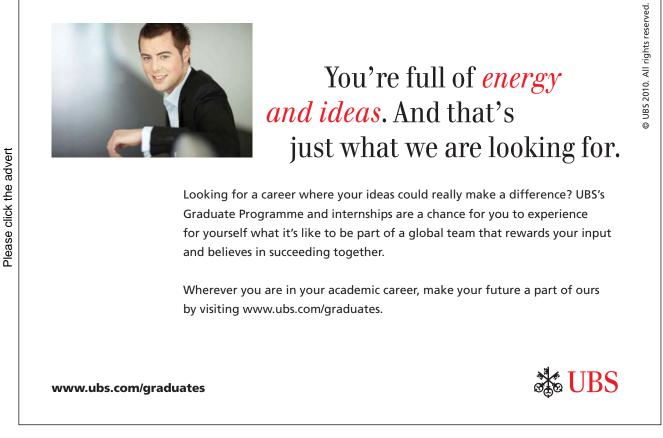
-	p = 0.60 MPa (158.85 C)			
	v	u	h	s
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K
Sat. liquid	0.00110	669.4	670.6	1.9312
Sat. vapour	0.3175	2567.4	2756.8	6.7600

at 0.6 MPa and x=0.9,

T=158.85 C

- $h_1 = h_f + x h_{f_{a}}$
 - = 670.6 + 0.9 x (2756.8 670.6)

=2548.18 kJ/kg



$$V_1 = V_f + x V_{fg}$$

= 0.0011 + 0.9x(0.3715 - 0.0011)

 $= 0.28424 \text{ m}^3/\text{kg}$

 $S_1 = S_f + x S_{fg}$

= 1.9312 + 0.9x(6.7600 - 1.9312)

= 6.2771 kJ/kgK

T	<i>p</i> = 0.10 MPa (99.63 C)			
	v	u	h	S
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K
Sat. liquid	0.00104	417.3	417.4	1.3030
Sat. vapour	1.694	2506.1	2675.5	7.3594

at 0.1 MPa, constant entropy, S₂=S₁=6.2771 kJ/kgK T=99.63 C

$$X_{2} = \frac{S_{1} - S_{f}}{S_{g} - S_{f}} = \frac{6.2771 - 1.303}{7.3594 - 1.303} = 0.821$$

$$h_{2} = h_{f} + X_{2}(h_{g} - h_{f}) = 417.4 + 0.821(2675.5 - 417.4) = 2272.2 \text{ kJ/kg}$$

$$v_{2} = v_{f} + X_{2}(v_{g} - v_{f}) = 0.00104 + 0.821(1.694 - 0.00104) = 1.3909 \text{ m}^{3}/\text{kg}$$

hence

dT = 158.85 - 99.63 = 59.22 C

 $dv = 1.3909- 0.28424 = 1.107 \text{ m}^3/\text{kg}$

dh = 2548.18 - 2272.2 = 276.0 kJkg

13. The pressure in a steam main pipe is 1.2 MPa; a sample is drawn off and throttled where its pressure and temperature become 0.1 MPa, 140°C respectively. Determine the dryness fraction of the steam in the main stating reasonable assumptions made!

[Ans: 0.986, assuming constant enthalpy]

Solution:

state 2, at 0.1 MPa and T=140C

h₂= 2756.36 kJ/kg S₂=7.5630 kJ/kgK

T	p = 0.10 MPa (99.63 C)			
	V	u	h	s
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K
Sat. liquid	0.00104	417.3	417.4	1.3030
Sat. vapour	1.694	2506.1	2675.5	7.3594
100	1.6958	2506.7	2676.2	7.3614
150	1.9364	2582.8	2776.4	7.6143

at 1.2 MPa, constant enthalpy, $h_1=h_2=2756.36 \text{ kJ/kg}$

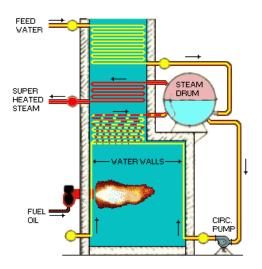
-	p = 1.20 MPa (187.99 C)			
	v	u	h	S
deg-C	m^3/kg	kJ/kg	kJ/kg	kJ/kg K
Sat. liquid	0.00114	797.3	798.6	2.2166
Sat. vapour	0.16333	2588.8	2784.4	6.5233

$$X_1 = \frac{h_1 - h_f}{h_q - h_f} = \frac{2756.36 - 798.6}{2784.4 - 798.6} = 0.9858$$

14. A boiler receives feed water at 20 kPa as saturated liquid and delivers steam at 2 MPa and 500°C. If the furnace of this boiler is oil fired, the calorific value of oil being 42000 kJ/kg; determine the efficiency of the combustion when 4.2 tonnes of oil was required to process 42000 kg of steam.

[Ans: 76%]

Solution:



a) Constant pressure process.

 $h_1 = h_{f_{a20}} kPa = 251.40 kJ/kg$

$$h_2 = 3467.6 \text{ kJ/kg}$$

SFEE ignoring W, Δke and ΔPe :

Qs = $m_s (h_2 - h_1)$ = 42000 (3467.6 - 251.4) = 135 x 10⁶ kJ

b) The heat generated by burning oil in the furnace is

= mass of oil burned x calorific value

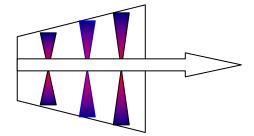
 $= 4200 \ge 42000 = 176 \ge 10^6 \text{ kJ}$

$$\therefore Efficiency = \frac{\text{Energy Output}}{\text{Energy Input}} = \frac{135}{176} = 76.7\%$$

15. 10 kg/s steam at 6 MPa and 500°C expands isentropically in a turbine to a pressure of 100 kPa. If the heat transfer from the casing to surroundings represents 1 per cent of the overall change of enthalpy of the steam, calculate the power output of the turbine. Assume exit is 5 m above entry and that initial velocity of steam is 100 m/s whereas exit velocity is 10 m/s.

[Ans: 9 MW]

Solution:



At 6 MPa, 500 °C

 $h_1 = 3422.2 \text{ kJ/kg}$

 $s_1 = 6.8803 \text{ kJ/kgK}$

at 100 kPa,

$$s_f = 1.303, s_{fg} = 6.056 \text{ kJ/kgK}$$

 $h_f = 417, h_{fg} = 2258 \text{ kJ/kg}$
 $x_2 = x_2 = \frac{6.8803 - 1.303}{6.056} = 0.921$
 $h_2 = 417 + 0.921 \text{ x } 2258 = 2496.5 \text{ kJ/kg}$

The Steady Flow Energy Equation applies to this situation:

Q - W = m[(h₂ - h₁) +
$$\frac{V_2^2 - V_1^2}{2}$$
 + g (z₂ - z₁)]
but Q = - $\frac{m}{100}$ (h₂ - h₁) Heat loss (negative sign)
W = -m[1.01 (h₂ - h₁) + $\frac{V_2^2 - V_1^2}{2}$ + g (z₂ - z₁)]
 $W = 10x \left[1.01(3422.2 - 2496.5) + \frac{10^2 - 100^2}{2 \times 1000} + \frac{9.8 \times 5}{1000} \right] = 9 MW$