## I NSTRUCTI ON MANUAL

# INNOVATOR LX SERIES UHF Analog Driver/Transmitter 

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## Chapter 1 I ntroduction

This manual explains the installation, setup, alignment, and maintenance procedures for the Innovator LX Series UHF analog modular driver/transmitter. It is important that you read all of the instructions, especially the safety information in this chapter, before you begin to install or operate the unit.

### 1.1 Manual Overview

This instruction manual is divided into five chapters and supporting appendices. Chapter 1, Introduction, contains information on the assembly numbering system used in the manual, safety, maintenance, return procedures, and warranties. The second chapter describes the driver/transmitter and includes discussions on system control and status indicators and remote control connections. Chapter 3 explains how to unpack, install, setup, and operate the driver/transmitter. Chapter 4 contains circuit-level descriptions for boards and board-level components in the driver/transmitter. Chapter 5, Detailed Alignment Procedures, provides information on adjusting the system assemblies for optimal operation. The appendices contain assembly and subassembly drawings and parts lists, and system specifications.

### 1.2 Assembly Designators

Axcera has assigned assembly numbers, such as $A x$ ( $x=1,2,3 .$. ), to all assemblies, modules, and boards that are referenced in the text of this manual and shown on the block diagrams and interconnect drawings provided in the appendices. These supporting documents are arranged in increasing numerical order in the appendices. Section titles in the text for assembly or module descriptions or alignment procedures contain the associated part number(s) and the
relevant appendix that contains the drawings for that item.

### 1.3 Safety

The UHF drivers and transmitters manufactured by Axcera are designed to be easy to use and repair while providing protection from electrical and mechanical hazards. Listed throughout the manual are notes, cautions, and warnings concerning possible safety hazards that may be encountered while operating or servicing the driver/transmitter. Please review these warnings and familiarize yourself with the operation and servicing procedures before working on the driver/transmitter.

Read All Instructions - All of the operating and safety instructions should be read and understood before operating this equipment.

Retain Manuals - The manuals for the driver/transmitter should be retained at the transmitter site for future reference. We provide two sets of manuals for this purpose; one set can be left at the office while one set can be kept at the site.

## Heed all Notes, Warnings, and

 Cautions - All of the notes, warnings, and cautions listed in this safety section and throughout the manual must be followed.Follow Instructions - All of the operating and use instructions for the driver/transmitter should be followed.

Cleaning - Unplug or otherwise disconnect all power from the equipment before cleaning. Do not use liquid or aerosol cleaners. Use a damp cloth for cleaning.

Ventilation - Openings in the cabinets and module front panels are provided for
ventilation. To ensure the reliable operation of the driver/transmitter, and to protect the unit from overheating, these openings must not be blocked.

Servicing - Do not attempt to service this product yourself until becoming familiar with the equipment. If in doubt, refer all servicing questions to qualified Axcera service personnel.

## Replacement Parts - When

 replacement parts are used, be sure that the parts have the same functional and performance characteristics as the original part. Unauthorized substitutions may result in fire, electric shock, or other hazards. Please contact the Axcera Technical Service Department if you have any questions regarding service or replacement parts.
### 1.4 Maintenance

The Innovator LX Series Driver/Transmitter is designed with components that require little or no periodic maintenance except for the routine cleaning of the fans and the front panels of the modules.

The amount of time between cleanings depends on the conditions within the transmitter room. While the electronics have been designed to function even if covered with dust, a heavy buildup of dust, dirt, or insects will affect the cooling of the components. This could lead to a thermal shutdown or the premature failure of the affected module.

When the front panels of the modules become dust covered, the top covers should be taken off and any accumulated foreign material should be removed. A vacuum cleaner, utilizing a small, wandtype attachment, is an excellent way to suction out the dirt. Alcohol and other cleaning agents should not be used unless you are certain that the solvents will not damage components or the silkscreened markings on the modules and boards. Water-based cleaners can be
used, but do not saturate the components. The fans and heatsinks should be cleaned of all dust or dirt to permit the free flow of air for cooling purposes.

It is recommended that the operating parameters of the driver/transmitter be recorded from the LEDs on the modules and the LCD system metering on the control/monitoring module at least once a month. It is suggested that this data be retained in a rugged folder or envelope.

### 1.5 Material Return Procedure

To insure the efficient handling of equipment or components that have been returned for repair, Axcera requests that each returned item be accompanied by a Material Return Authorization Number (MRA\#).

An MRA\# can be obtained from any Axcera Field Service Engineer by contacting the Axcera Field Service Department at (724) 873-8100 or by fax at (724) 873-8105. This procedure applies to all items sent to the Field Service Department regardless of whether the item was originally manufactured by Axcera.

When equipment is sent to the field on loan, an MRA\# is included with the unit. The MRA\# is intended to be used when the unit is returned to Axcera. In addition, all shipping material should be retained for the return of the unit to Axcera.

Replacement assemblies are also sent with an MRA\# to allow for the proper routing of the exchanged hardware. Failure to close out this type of MRA\# will normally result in the customer being invoiced for the value of the loaner item or the exchange assembly.

When shipping an item to Axcera, please include the MRA\# on the packing list and on the shipping container. The packing slip should also include contact
information and a brief description of why the unit is being returned.

Please forward all MRA items to:
AXCERA, LLC
103 Freedom Drive
P.O. Box 525

Lawrence, PA 15055-0525 USA
For more information concerning this procedure, call the Axcera Field Service Department.

Axcera can also be contacted through email at info@axcera.com and on the Web at www.axcera.com.

### 1.6 Limited One-Year Warranty for Axcera Products

Axcera warrants each new product that it has manufactured and sold against defects in material and workmanship under normal use and service for a period of one (1) year from the date of shipment from Axcera's plant, when operated in accordance with Axcera's operating instructions. This warranty shall not apply to tubes, fuses, batteries, or bulbs.

Warranties are valid only when and if (a) Axcera receives prompt written notice of breach within the period of warranty, (b) the defective product is properly packed and returned by the
buyer (transportation and insurance prepaid), and (c) Axcera determines, in its sole judgment, that the product is defective and not subject to any misuse, neglect, improper installation, negligence, accident, or (unless authorized in writing by Axcera) repair or alteration. Axcera's exclusive liability for any personal and/or property damage (including direct, consequential, or incidental) caused by the breach of any or all warranties, shall be limited to the following: (a) repairing or replacing (in Axcera's sole discretion) any defective parts free of charge (F.O.B. Axcera's plant) and/or (b) crediting (in Axcera's sole discretion) all or a portion of the purchase price to the buyer.

Equipment furnished by Axcera, but not bearing its trade name, shall bear no warranties other than the special hours-of-use or other warranties extended by or enforceable against the manufacturer at the time of delivery to the buyer.

NO WARRANTIES, WHETHER STATUTORY, EXPRESSED, OR I MPLIED, AND NO WARRANTIES OF MERCHANTABI LITY, FITNESS FOR ANY PARTICULAR PURPOSE, OR FREEDOM FROM I NFRI NGEMENT, OR THE LIKE, OTHER THAN AS SPECIFIED IN PATENT LIABI LITY ARTI CLES, AND IN THI S ARTI CLE, SHALL APPLY TO THE EQUI PMENT FURNISHED HEREUNDER.

## T WARNI NG!!!

< HIGH VOLTAGE >
DO NOT ATTEMPT TO REPAIR OR TROUBLESHOOT THIS EQUI PMENT UNLESS YOU ARE FAMILIAR WITH ITS OPERATION AND EXPERIENCED IN SERVICING HIGH VOLTAGE EQUIPMENT. LETHAL VOLTAGES ARE PRESENT WHEN POWER IS APPLIED TO THIS SYSTEM. IF POSSIBLE, TURN OFF POWER BEFORE MAKI NG ADJ USTMENTS TO THE SYSTEM.
^ RADIO FREQUENCY RADI ATI ON HAZARD $\star$
MICROWAVE, RF AMPLIFIERS AND TUBES GENERATE HAZARDOUS RF RADIATION THAT CAN CAUSE SEVERE INJURY INCLUDING CATARACTS, WHICH CAN RESULT IN BLINDNESS. SOME CARDI AC PACEMAKERS MAY BE AFFECTED BY THE RF ENERGY EMITTED BY RF AND MICROWAVE AMPLIFIERS. NEVER OPERATE THE TRANSMITTER SYSTEM WITHOUT A PROPERLY MATCHED RF ENERGY ABSORBING LOAD ATTACHED. KEEP PERSONNEL AWAY FROM OPEN WAVEGUIDES AND ANTENNAS. NEVER LOOK I NTO AN OPEN WAVEGUI DE OR ANTENNA. MONITOR ALL PARTS OF THE RF SYSTEM FOR RADI ATI ON LEAKAGE AT REGULAR I NTERVALS.

## EMERGENCY FI RST AID I NSTRUCTI ONS

Personnel engaged in the installation, operation, or maintenance of this equipment are urged to become familiar with the following rules both in theory and practice. It is the duty of all operating personnel to be prepared to give adequate Emergency First Aid and thereby prevent avoidable loss of life.


1. Find out if the person is breathing.

You must find out if the person has stopped breathing. If you think he is not breathing, place him flat on his back. Put your ear close to his mouth and look at his chest. If he is breathing you can feel the air on your cheek. You can see his chest move up and down. If you do not feel the air or see the chest move, he is not breathing.

## RESCUE BREATHI NG


2. If he is not breathing, open the airway by tilting his head backwards.

Lift up his neck with one hand and push down on his forehead with the other. This opens the airway. Sometimes doing this will let the person breathe again by himself.
3. If he is still not breathing, begin rescue breathing.
-Keep his head tilted backward. Pinch nose shut.
-Put your mouth tightly over his mouth.
-Blow into his mouth once every five seconds
-DO NOT STOP rescue breathing until help arrives.
LOOSEN CLOTHING - KEEP
WARM
Do this when the victim is
breathing by himself or help is
available. Keep him as quiet as
possible and from becoming
chilled. Otherwise treat him for
shock.

## BURNS

SKIN REDDENED: Apply ice cold water to burned area to prevent burn from going deeper into skin tissue. Cover area with clean sheet or cloth to keep away air. Consult a physician.

SKIN BLISTERED OR FLESH CHARRED: Apply ice cold water to burned area to prevent burn from going deeper into skin tissue.

Cover area with clean sheet or cloth to keep away air. Treat victim for shock and take to hospital.

EXTENSIVE BURN - SKIN BROKEN: Cover area with clean sheet or cloth to keep away air. Treat victim for shock and take to hospital.

## Note: Because of possible FCC assigned offset, check for the assigned Carrier Frequency as written on License.

## UHF Channels NTSC Standard IF, 45.75 MHz

| Visual Carrier Frequency ( MHz ) |  |  |  | $\begin{gathered} \begin{array}{c} \text { L.O. } \\ (\mathbf{M H z}) \end{array} \\ \hline \text { Nominal } \end{gathered}$ | Crystal Frequency ( MHz ) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Channel | Nominal | Minus | Plus |  | Nominal | Minus | Plus |
| 14 | 471.25 | 471.24 | 471.26 | 517.00 | 64.625 | 64.62375 | 64.62625 |
| 15 | 477.25 | 477.24 | 477.26 | 523.00 | 65.375 | 65.37375 | 65.37625 |
| 16 | 483.25 | 483.24 | 483.26 | 529.00 | 66.125 | 66.12375 | 66.12625 |
| 17 | 489.25 | 489.24 | 489.26 | 535.00 | 66.875 | 66.87375 | 66.87625 |
| 18 | 495.25 | 495.24 | 495.26 | 541.00 | 67.625 | 67.62375 | 67.62625 |
| 19 | 501.25 | 501.24 | 501.26 | 547.00 | 68.375 | 68.37375 | 68.37625 |
| 20 | 507.25 | 507.24 | 507.26 | 553.00 | 69.125 | 69.12375 | 69.12625 |
| 21 | 513.25 | 513.24 | 513.26 | 559.00 | 69.875 | 69.87375 | 69.87625 |
| 22 | 519.25 | 519.24 | 519.26 | 565.00 | 70.625 | 70.62375 | 70.62625 |
| 23 | 525.25 | 525.24 | 525.26 | 571.00 | 71.375 | 71.37375 | 71.37625 |
| 24 | 531.25 | 531.24 | 531.26 | 577.00 | 72.125 | 72.12375 | 72.12625 |
| 25 | 537.25 | 537.24 | 537.26 | 583.00 | 72.875 | 72.87375 | 72.87625 |
| 26 | 543.25 | 543.24 | 543.26 | 589.00 | 73.625 | 73.62375 | 73.62625 |
| 27 | 549.25 | 549.24 | 549.26 | 595.00 | 74.375 | 74.37375 | 74.37625 |
| 28 | 555.25 | 555.24 | 555.26 | 601.00 | 75.125 | 75.12375 | 75.12625 |
| 29 | 561.25 | 561.24 | 561.26 | 607.00 | 75.875 | 75.87375 | 75.87625 |
| 30 | 567.25 | 567.24 | 567.26 | 613.00 | 76.625 | 76.62375 | 76.62625 |
| 31 | 573.25 | 573.24 | 573.26 | 619.00 | 77.375 | 77.37375 | 77.37625 |
| 32 | 579.25 | 579.24 | 579.26 | 625.00 | 78.125 | 78.12375 | 78.12625 |
| 33 | 585.25 | 585.24 | 585.26 | 631.00 | 78.875 | 78.87375 | 78.87625 |
| 34 | 591.25 | 591.24 | 591.26 | 637.00 | 79.625 | 79.62375 | 79.62625 |
| 35 | 597.25 | 597.24 | 597.26 | 643.00 | 80.375 | 80.37375 | 80.37625 |
| 36 | 603.25 | 603.24 | 603.26 | 649.00 | 81.125 | 81.12375 | 81.12625 |
| 37 | 609.25 | 609.24 | 609.26 | 655.00 | 81.875 | 81.87375 | 81.87625 |
| 38 | 615.25 | 615.24 | 615.26 | 661.00 | 82.625 | 82.62375 | 82.62625 |
| 39 | 621.25 | 621.24 | 621.26 | 667.00 | 83.375 | 83.37375 | 83.37625 |
| 40 | 627.25 | 627.24 | 627.26 | 673.00 | 84.125 | 84.12375 | 84.12625 |
| 41 | 633.25 | 633.24 | 633.26 | 679.00 | 84.875 | 84.87375 | 84.87625 |
| 42 | 639.25 | 639.24 | 639.26 | 685.00 | 85.625 | 85.62375 | 85.62625 |
| 43 | 645.25 | 645.24 | 645.26 | 691.00 | 86.375 | 86.37375 | 86.37625 |

## Note: Because of possible FCC assigned offset, check for the assigned Carrier Frequency as written on License.

UHF Channels NTSC Standard IF, 45.75 MHz

| Visual Carrier Frequency ( MHz ) |  |  |  | $\begin{gathered} \begin{array}{l} \text { L.O. } \\ \text { ( MHz) } \end{array} \\ \text { Nominal } \end{gathered}$ | Crystal Frequency ( MHz ) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Channel | Nominal | Minus | Plus |  | Nominal | Minus | Plus |
| 44 | 651.25 | 651.24 | 651.26 | 697.00 | 87.125 | 87.12375 | 87.12625 |
| 45 | 657.25 | 657.24 | 657.26 | 703.00 | 87.875 | 87.87375 | 87.87625 |
| 46 | 663.25 | 663.24 | 663.26 | 709.00 | 88.625 | 88.62375 | 88.62625 |
| 47 | 669.25 | 669.24 | 669.26 | 715.00 | 89.375 | 89.37375 | 89.37625 |
| 48 | 675.25 | 675.24 | 675.26 | 721.00 | 90.125 | 90.12375 | 90.12625 |
| 49 | 681.25 | 681.24 | 681.26 | 727.00 | 90.875 | 90.87375 | 90.87625 |
| 50 | 687.25 | 687.24 | 687.26 | 733.00 | 91.625 | 91.62375 | 91.62625 |
| 51 | 693.25 | 693.24 | 693.26 | 739.00 | 92.375 | 92.37375 | 92.37625 |
| 52 | 699.25 | 699.24 | 699.26 | 745.00 | 93.125 | 93.12375 | 93.12625 |
| 53 | 705.25 | 705.24 | 705.26 | 751.00 | 93.875 | 93.87375 | 93.87625 |
| 54 | 711.25 | 711.24 | 711.26 | 757.00 | 94.625 | 94.62375 | 94.62625 |
| 55 | 717.25 | 717.24 | 717.26 | 763.00 | 95.375 | 95.37375 | 95.37625 |
| 56 | 723.25 | 723.24 | 723.26 | 769.00 | 96.125 | 96.12375 | 96.12625 |
| 57 | 729.25 | 729.24 | 729.26 | 775.00 | 96.875 | 96.87375 | 96.87625 |
| 58 | 735.25 | 735.24 | 735.26 | 781.00 | 97.625 | 97.62375 | 97.62625 |
| 59 | 741.25 | 741.24 | 741.26 | 787.00 | 98.375 | 98.37375 | 98.37625 |
| 60 | 747.25 | 747.24 | 747.26 | 793.00 | 99.125 | 99.12375 | 99.12625 |
| 61 | 753.25 | 753.24 | 753.26 | 799.00 | 99.875 | 99.87375 | 99.87625 |
| 62 | 759.25 | 759.24 | 759.26 | 805.00 | 100.625 | 100.62375 | 100.62625 |
| 63 | 765.25 | 765.24 | 765.26 | 811.00 | 101.375 | 101.37375 | 101.37625 |
| 64 | 771.25 | 771.24 | 771.26 | 817.00 | 102.125 | 102.12375 | 102.12625 |
| 65 | 777.25 | 777.24 | 777.26 | 823.00 | 102.875 | 102.87375 | 102.87625 |
| 66 | 783.25 | 783.24 | 783.26 | 829.00 | 103.625 | 103.62375 | 103.62625 |
| 67 | 789.25 | 789.24 | 789.26 | 835.00 | 104.375 | 104.37375 | 104.37625 |
| 68 | 795.25 | 795.24 | 795.26 | 841.00 | 105.125 | 105.12375 | 105.12625 |
| 69 | 801.25 | 801.24 | 801.26 | 847.00 | 105.875 | 105.87375 | 105.87625 |
| 70 | 807.25 | 807.24 | 807.26 | 853.00 | 106.625 | 106.62375 | 106.62625 |

Note: Because of possible FCC assigned offset, check for the assigned Carrier Frequency as written on License.

| UHF Frequency Assignments |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Channel Number | Bandwidth ( MHz ) | Video <br> (MHz) | Color <br> (MHz) | Audio (MHz) |
| 14 | 470-476 | 471.25 | 474.83 | 475.75 |
| 15 | 476-482 | 477.25 | 480.83 | 481.75 |
| 16 | 482-488 | 483.25 | 486.83 | 487.75 |
| 17 | 488-494 | 489.25 | 492.83 | 493.75 |
| 18 | 494-500 | 495.25 | 498.83 | 499.75 |
| 19 | 500-506 | 501.25 | 504.83 | 505.75 |
| 20 | 506-512 | 507.25 | 510.83 | 511.75 |
| 21 | 512-518 | 513.25 | 516.83 | 517.75 |
| 22 | 518-524 | 519.25 | 522.83 | 523.75 |
| 23 | 524-530 | 525.25 | 528.83 | 529.75 |
| 24 | 530-536 | 531.25 | 534.83 | 535.75 |
| 25 | 536-542 | 537.25 | 540.83 | 541.75 |
| 26 | 542-548 | 543.25 | 546.83 | 547.75 |
| 27 | 548-554 | 549.25 | 552.83 | 553.75 |
| 28 | 554-560 | 555.25 | 558.83 | 559.75 |
| 29 | 560-566 | 561.25 | 564.83 | 565.75 |
| 30 | 566-572 | 567.25 | 570.83 | 571.75 |
| 31 | 572-578 | 573.25 | 576.83 | 577.75 |
| 32 | 578-584 | 579.25 | 582.83 | 583.75 |
| 33 | 584-590 | 585.25 | 588.83 | 589.75 |
| 34 | 590-596 | 591.25 | 594.83 | 595.75 |
| 35 | 596-602 | 597.25 | 600.83 | 601.75 |
| 36 | 602-608 | 603.25 | 606.83 | 607.75 |
| 37 | 608-614 | 609.25 | 612.83 | 613.75 |
| 38 | 614-620 | 615.25 | 618.83 | 619.75 |
| 39 | 620-626 | 621.25 | 624.83 | 625.75 |
| 40 | 626-632 | 627.25 | 630.83 | 631.75 |
| 41 | 632-638 | 633.25 | 636.83 | 637.75 |
| 42 | 638-644 | 639.25 | 642.83 | 643.75 |
| 43 | 644-650 | 645.25 | 648.83 | 649.75 |

## Note: Because of possible FCC assigned offset, check for the assigned Carrier Frequency as written on License.

| UHF Frequency Assignments |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Channel Number | Bandwidth ( MHz) | Video <br> (MHz) | Color <br> (MHz) | Audio (MHz) |
| 44 | 650-656 | 651.25 | 654.83 | 655.75 |
| 45 | 656-662 | 657.25 | 660.83 | 661.75 |
| 46 | 662-668 | 663.25 | 666.83 | 667.75 |
| 47 | 668-674 | 669.25 | 672.83 | 673.75 |
| 48 | 674-680 | 675.25 | 678.83 | 679.75 |
| 49 | 680-686 | 681.25 | 684.83 | 685.75 |
| 50 | 686-692 | 687.25 | 690.83 | 691.75 |
| 51 | 692-698 | 693.25 | 696.83 | 697.75 |
| 52 | 698-704 | 699.25 | 702.83 | 703.75 |
| 53 | 704-710 | 705.25 | 708.83 | 709.75 |
| 54 | 710-716 | 711.25 | 714.83 | 715.75 |
| 55 | 716-722 | 717.25 | 720.83 | 721.75 |
| 56 | 722-728 | 723.25 | 726.83 | 727.75 |
| 57 | 728-734 | 729.25 | 732.83 | 733.75 |
| 58 | 734-740 | 735.25 | 738.83 | 739.75 |
| 59 | 740-746 | 741.25 | 744.83 | 745.75 |
| 60 | 746-752 | 747.25 | 750.83 | 751.75 |
| 61 | 752-758 | 753.25 | 756.83 | 757.75 |
| 62 | 758-764 | 759.25 | 762.83 | 763.75 |
| 63 | 764-770 | 765.25 | 768.83 | 769.75 |
| 64 | 770-776 | 771.25 | 774.83 | 775.75 |
| 65 | 776-782 | 777.25 | 780.83 | 781.75 |
| 66 | 782-788 | 783.25 | 786.83 | 787.75 |
| 67 | 788-794 | 789.25 | 792.83 | 793.75 |
| 68 | 794-800 | 795.25 | 798.83 | 799.75 |
| 69 | 800-806 | 801.25 | 804.83 | 805.75 |
| 70 | 806-812 | 807.25 | 810.83 | 811.75 |

## dBm, dBw, dBmV, dB $\mu \mathrm{V}, \&$ VOLTAGE <br> EXPRESSED IN WATTS

50 Ohm System

| WATTS | PREFIX | dBm | dBw | dBm <br> V | $\mathrm{dB} \mu \mathrm{V}$ | VOLTAGE |
| ---: | :--- | :---: | :---: | :---: | :---: | :---: |
| $1,000,000,000,000$ | 1 TERAWATT | +150 | +120 |  |  |  |
| $100,000,000,000$ | 100 GIGAWATTS | +140 | +110 |  |  |  |
| $10,000,000,000$ | 10 GIGAWATTS | +130 | +100 |  |  |  |
| $1,000,000,000$ | 1 GI GAWATT | +120 | +99 |  |  |  |
| $100,000,000$ | 100 MEGAWATTS | +110 | +80 |  |  |  |
| $10,000,000$ | 10 MEGAWATTS | +100 | +70 |  |  |  |
| $1,000,000$ | 1 MEGAWATT | +90 | +60 |  |  |  |
| 100,000 | 100 KILOWATTS | +80 | +50 |  |  |  |
| 10,000 | 10 KILOWATTS | +70 | +40 |  |  |  |
| 1,000 | 1 KILOWATT | +60 | +30 |  |  |  |
| 100 | 1 HECTROWATT | +50 | +20 |  |  |  |
| 50 |  | +47 | +17 |  |  |  |
| 20 |  | +43 | +13 |  |  |  |
| 10 | 1 DECAWATT | +40 | +10 |  |  |  |
| 1 | 1 WATT | +30 | 0 | +77 | +137 | 7.07 V |
| 0.1 | 1 DECIWATT | +20 | -10 | +67 | +127 | 2.24 V |
| 0.01 | 1 CENTIWATT | +10 | -20 | +57 | +117 | 0.707 V |
| 0.001 | 1 MILLIWATT | 0 | -30 | +47 | +107 | 224 mV |
| 0.0001 | 100 MICROWATTS | -10 | -40 |  |  |  |
| 0.00001 | 10 MICROWATTS | -20 | -50 |  |  |  |
| 0.000001 | 1 MICROWATT | -30 | -60 |  |  |  |
| 0.0000001 | 100 NANOWATTS | -40 | -70 |  |  |  |
| 0.00000001 | 10 NANOWATTS | -50 | -80 |  |  |  |
| 0.000000001 | 1 NANOWATT | -60 | -90 |  |  |  |
| 0.0000000001 | 100 PICOWATTS | -70 | -100 |  |  |  |
| 0.00000000001 | 10 PICOWATTS | -80 | -110 |  |  |  |
| 0.000000000001 | 1 PICOWATT | -90 | -120 |  |  |  |

TEMPERATURE CONVERSION

$$
\begin{aligned}
{ }^{\circ} \mathrm{F} & =32+\left[(9 / 5)^{\circ} \mathrm{C}\right] \\
{ }^{\circ} \mathrm{C} & =\left[(5 / 9)\left({ }^{\circ} \mathrm{F}-32\right)\right]
\end{aligned}
$$

## USEFUL CONVERSI ON FACTORS

| TO CONVERT FROM | MULTIPLY BY |  |
| :---: | :---: | :---: |
| mile (US statute) | kilometer (km) | 1.609347 |
| inch (in) | millimeter (mm) | 25.4 |
| inch (in) | centimeter ( cm ) | 2.54 |
| inch (in) | meter (m) | 0.0254 |
| foot (ft) | meter (m) | 0.3048 |
| yard (yd) | meter (m) | 0.9144 |
| mile per hour (mph) | kilometer per hour(km/hr) | 1.60934 |
| mile per hour (mph) | meter per second ( $\mathrm{m} / \mathrm{s}$ ) | 0.44704 |
| pound (lb) | kilogram (kg) | 0.4535924 |
| gallon (gal) | liter | 3.7854118 |
| U.S. Iiquid <br> (One U.S. gallon equals 0.8327 Canadian gallon) |  |  |
| fluid ounce ( fl oz ) | milliliters (ml) | 29.57353 |
| British Thermal Unit | watt (W) | 0.2930711 |
|  |  | per hour (Btu/hr) |
| horsepower (hp) | watt (W) | 746 |

## NOMENCLATURE OF FREQUENCY BANDS

FREQUENCY RANGE

```
3 to 30 kHz
30 to 300 kHz
300 to 3000 kHz
3 to 30 MHz
30 to 300 MHz
300 to 3000 MHz
3 to 30 GHz
30 to 300 GHz
```


## DESIGNATION

VLF
LF
MF
HF
VHF
UHF
SHF
EHF

- Very Low Frequency
- Low Frequency
- Medium Frequency
- High Frequency
- Very High Frequency
- Ultrahigh Frequency
- Superhigh Frequency
- Extremely High Frequency


## LETTER DESI GNATI ONS FOR UPPER FREQUENCY BANDS

LETTER

L
$S$
$C$
X
Ku
K
Ka
V
W

FREQ. BAND

```
1000-2000 MHz
2000-4000 MHz
4000-8000 MHz
8000-12000 MHz
12-18 GHz
18-27 GHz
27-40GHz
40-75GHz
75-110GHz
```


## ABBREVIATI ONS/ ACRONYMS

| AC | Alternating Current | PCB |
| :--- | :--- | :--- | Printed circuit board 1 Quadrature Amplitude Modulation

## RETURN LOSS VS. VSWR



## Chapter 2

## System Description \& Remote Control Connections

The analog transmitters in the Innovator LX Series are complete 10 W to 100 W UHF Analog internally diplexed modular television transmitters that operate at a nominal visual output power of 10 to 100 watts peak sync and an average aural output power of 1 to 10 watts, at an A/V ratio of $10 \mathrm{~dB}, 10 \%$ sound, or .5 to 5 watts at $13 \mathrm{~dB}, 5 \%$ sound.

The LX Series can also be used as a driver. The output power of the driver is
determined by the level needed to attain the full output power of the transmitter. The driver's maximum output is 7 Watts peak of sync.

### 2.1 System Overview

The Analog LX Series driver/transmitter is made up of the modules and assemblies listed in Table 2-1.

Table 2-1: LX Series Trays and Assemblies

| ASSEMBLY DESI GNATOR | TRAY/ ASSEMBLY NAME | PART NUMBER |
| :---: | :--- | :--- |
| A2 | Modulator Module (not <br> present in translator) | 1301929 |
| A3 | IF Processor Module | 1301938 |
| A4 | Control/Power Supply Module | 1301936 (110 VAC) OR <br> 1303229 (220 VAC) |
| A5 | LO/Upconverter Module | 1301930 |
| A6 | Power Amplifier Module, used <br> in 10-100 Watt Transmitters | 1301923 |
| OR A6 | Driver Amplifier Module, used <br> in high power transmitters | 1302846 |
| A11 | Backplane Board | 1301941 |
| A12 | Switch Board | $1527-1406$ |
| A20 | LCD Display Board |  |

## Exciter Amplifier Chassis Assembly, 110 VAC ( 1301914 ) or 220 VAC (1303228); Appendix B

The chassis assembly is factory set for operation using 110 VAC or 220 VAC. All of the modules except the power amplifier module and the power supply section of the Control \& Monitoring/Power Supply Module, plug directly into a backplane board. The backplane board provides module to module interconnection as well as interconnection to remote command and control connectors.

### 2.1.1 (A2) Modulator Module Assembly (1301929; Appendix B)

NOTE: The Modulator module is not present in a translator system


The (A2) Modulator Assembly contains the Modulator Board (1301797). The modulator is broadcast quality and provides front panel access to control and monitoring points. The video level is controlled through a sync tip clamp and sync and white clipping circuitry. The IF oscillator is oven controlled and locked to a 10 MHz reference for stability. The IF

Table 2-2. Modulator Front Panel Switch
signal is fed through a SAW filter for precise sideband shaping. The Modulator operates using either the baseband audio and video inputs or the $4.5-\mathrm{MHz}$ composite input to produce a diplexed, modulated, and on-channel frequency visual + aural RF output that is cabled to the IF Processing Module.

| SWITCH | FUNCTI ON |
| :---: | :--- |
| MAN/AUTO CLAMP | When Manual Clamp is selected, the video level is set by the <br> SW1 <br> Manual Bias Pot R67 located on the board. (NOTE: The pot is <br> factory set and needs no adjustment by the customer). |
|  | When Auto Clamp is selected, the video level control circuit <br> will automatically increase or decrease the video to maintain <br> the desired video level. |

Table 2-3. Modulator Front Panel Status Indicators

| LED | FUNCTI ON |
| :---: | :--- |
| AUR UNLOCK <br> DS5 (Red) | When lit it indicates that the 4.5 MHz VCO and the 10 MHz reference <br> are not PLL locked. |
| VIS UNLOCK <br> DS6 (Red) | When lit it indicates that the 45.75 MHz VCXO and the 10 MHz <br> reference signal are not PLL locked. |
| AUD OV DEV <br> DS4 (Red) | When lit it indicates the deviation level is more than $\pm 80 \mathrm{kHz}$ |
| VIDEO LOSS <br> DS1 (Red) | When lit it indicates the Video Input to the transmitter is lost. |
| OVER MOD <br> DS3 (Red) | When lit it indicates the Video input level is too high. |
| ALT IF <br> DS7 (Green) | When lit it indicates that external or alternate 4.5MHZ is present. |
| $10 ~ M H z ~ P R E S ~$ <br> DS2 (Green) | When lit it indicates that a 10 MHz reference is present to the <br> transmitter. |

Table 2-4. Modulator Front Panel Control Adjustments

| POTENTI OMETERS | DESCRIPTI ON |
| :---: | :--- |
| Video Gain (R42) | Adjusts the level of the output video. |
| Visual Level (R214) | Adjusts the Visual IF level that combines with the Aural IF. |
| Aural Level (R243) | Adjusts the Aural IF level that combines with the Visual IF. |
| MONO (R110) | Adjusts the deviation level of the balanced audio input. |
| STEREO (R132) | Adjusts the deviation level of the composite audio input. |
| SAP/PRO (R150) | Adjusts the deviation level of the subcarrier audio input. |

Table 2-5. Modulator Front Panel Sample

| SMA CONNECTOR | DESCRI PTI ON |
| :---: | :---: |
| MOD IF SAMPLE (J10) | Sample of the combined Aural IF and Visual IF signals. |

### 2.1.2 (A3) IF Processor Module Assembly (1301938; Appendix B)



The (A3) IF Processor Assembly contains the IF Processor Board (1301977). The IF Processor provides pre-correction to ensure broadcast quality output signal. The pre-correction consists of amplitude linearity correction, Incidental Carrier Phase Modulation (ICPM) correction and frequency response correction.

The IF Processor module is configured either for an analog or digital system. Pin 13C of the IF Processor module is grounded in analog systems and left not connected in digital systems. An IF Processor Interlock signal is used to report the presence of the IF Processor module to the Control Monitoring board. If the IF Processor interlock signal is not present, the LX Series 100 Watt Transmitter/Exciter Driver RF output is Muted (turned off). If an analog IF Processor module is installed and the Modulation Present signal is not true, the LX Series 100 Watt Transmitter / Exciter Driver output is Muted (turned off).

The Control \& Monitoring/Power Supply module uses the IF Processor module for

System output power control. Through the front panel display or a remote interface, an operator can set the transmitter's RF output power. The range of RF power adjustment is between $0 \%$ (full off) and $105 \%$ (full power plus). A front panel IF Processor module potentiometer sets the upper limit of RF power at $120 \%$. The system's Control Monitoring board compares the RF Power Monitoring module RF power level with the desired level and uses the IF Power Control PWM line to correct for errors.

In digital systems, a digital level control (DLC) voltage is generated on the IF Processor module and sent to an external digital modulator (DT1C). RF power control is implemented by changing the DLC voltage provided to the external digital modulator. The 'RF High' potentiometer sets the upper adjusted range of RF control circuit output to $120 \%$.

The IF Processor module provides a reference ALC voltage to the system's Upconverter. When the ALC voltage decreases, the Upconverter automatically lowers the system output power through the AGC circuits.

The IF Processor module has a front panel switch to select Auto or Manual ALC. When Manual ALC is selected, the reference ALC voltage is set by a front panel potentiometer. In this condition, the RF power level control circuit is removed from use. When the ALC select switch is changed to Auto, the RF power level control circuit will start at low power and increase the RF output until the desired output power is attained.

The IF Processor module Modulation Present signal is monitored. If the modulation level is too low or nonexistent, a Modulation Present fault is reported to the Control Monitoring board. When the controller detects this fault, it can be set to Automatically Mute
the transmitter or in Manual mode the transmitter will continue to operate at 25\% output.

The IF Processor module Input Signal level is monitored. If the signal level is too low or non-existent, an Input fault is
reported on the Control Monitoring board. When the IF Processor board detects an Input Signal fault it automatically Mutes the transmitter. The system controller does not Mute on an IF Processor Input fault.

Table 2-6. IF Processor Front Panel Switch

| SWITCH | FUNCTI ON |
| :---: | :--- |
| MAN/AUTO ALC | When Manual ALC is selected, the reference ALC voltage is set <br> by the ALC Gain front panel potentiometer. <br> When Auto ALC is selected, the IF level control circuit will <br> automatically increase the IF output until the desired output <br> power is attained. |

Table 2-7. IF Processor Front Panel Status Indicators

| LED | FUNCTI ON |
| :---: | :--- |
| INPUT FAULT (Red) | When lit it indicates that there is a loss of the IF Input signal to the <br> IF Processor. Transmitter can be set to Mute on an IF Input Fault. |
| ALC Fault (Red) | When lit it indicates that the required gain to produce the desired <br> output power level has exceeded the operational range of the ALC <br> circuit. The LED will also be lit when ALC is in Manual. |
| MUTE (Red) | When lit it indicates that the IF input signal is cut back but the <br> enable to the Power Supply is present and the +32 VDC remains on. |

Table 2-8. IF Processor Front Panel Control Adjustments

| POTENTIOMETERS | DESCRIPTION |
| :---: | :--- |
| FREQUENCY <br> RESPONSE <br> EQUALIZER | These three variable resistors, R103, R106 \& R274, adjust the <br> depth of gain for the three stages of frequency response correction. |
| ALC GAIN | Adjusts the gain of the transmitter when the transmitter is in the <br> Auto ALC position. |
| MAN GAIN | Adjusts the gain of the transmitter when the transmitter is in the <br> Manual ALC position. |
| LINEARITY | These three variable resistors adjust the threshold cut in for the <br> three stages of linearity pre-correction. R211 and R216, the top <br> two pots, are adjusted to correct for in phase amplitude distortions. <br> R 231, the bottom pot, is adjusted to correct for quadrature phase <br> distortions. |

Table 2-9. IF Processor Front Panel Sample

| SMA CONNECTOR | DESCRI PTI ON |
| :---: | :---: |
| IF SAMPLE | Sample of the pre-corrected IF output of the IF Processor |

### 2.1.3 (A5) LO/ Upconverter Module Assembly (1301930; Appendix B)



The (A5) LO/Upconverter Module Assembly contains a front panel LED display board (1303033), a UHF Filter (1007-1101), a UHF Generator Board (1585-1265) and a LO/Upconverter Assembly (1303039). The LO/Upconverter Assembly contains the LO/Upconverter Board (1302132).

The LX Series Upconverter converts an IF input signal to a RF output signal on the desired channel frequency using a high stability oven controlled oscillator with very low phase noise and an Automatic Level Control (ALC) for stable output signal level.

Several control voltages are used for transmitter power control. Automatic gain control (AGC) circuits set the RF output level of the transmitter system.

AGC \#1 is provided by the Transmitter/Exciter Driver Power Amplifier module. This voltage is used by the Upconverter to maintain a constant RF output level at the Power Amplifier module output. If this voltage exceeds 0.9 VDC , the system is in an over-drive condition. The 0.9 VDC over-
driver threshold is set by a front panel Upconverter module potentiometer. When an over-drive condition is detected, the Upconverter module reduces its RF output level. For values less than 0.9 VDC, the Upconverter uses the AGC \# 1 voltage for automatic gain control by setting it's RF output to maintain AGC \#1 equal to the AGC voltage set by another front panel potentiometer. When the Upconverter is set for manual gain, the RF output of the Upconverter is set by the front panel AGC potentiometer. In manual gain operation, the AGC \#1 feedback voltage from the PA is not used to adjust the RF level unless an over-drive condition is detected.

AGC \#2 is provided by each of the optional external amplifier modules. Diodes are used in each of the external amplifier forward power circuits to capture the highest detected sample voltage. This voltage is used by the Upconverter to maintain a constant RF output of the system. As with AGC \#1, the Upconverter module reduces its RF output level if AGC \#2 is too high. AGC \#1 and ACG \#2 are diode ORed together in the Upconverter gain circuit. Both AGC voltages are first reduced by an onboard potentiometer before being amplified. If an over-drive condition does not exist, the higher of the two AGC voltages is used to control the Upconverter gain circuit. An AFC Voltage is generated to control the VCXO of the UHF Generator portion of the Upconverter module. The typical AFC voltage is 0.5 VDC but it can be as high as +1.5 VDC.

The Upconverter can operate on either it's internal 10 MHz source or on a 10 MHz external reference signal. When an external 10 MHz source is present on J10, it is automatically selected. An external reference present signal is provided to the controller for display purposes. The selected 10 MHz signal from the Upconverter is buffered then
sent to the backplane on two ports. One port is sent to the Modulator module, if present, and the other is routed to a BNC connector (J11) on the backplane for a system 10 MHz output signal.

A National Semiconductor frequency synthesizer IC is used in the frequency conversion of the IF signal to a RF signal. The frequency synthesizer IC uses a 10 MHz reference frequency for signal conversion. Typically the IF input frequency is 45.75 MHz for analog system and 44 MHz for DTV. To obtain different output RF frequencies, the synthesizer IC is serial programmed by the Control Monitoring board. The part is programmed to use a 5 kHz phase detection frequency. With a 10 MHz input signal, the R counter is set to 2000. With these settings the N counter
is set to the desired LO frequency in kHz $/ 5 \mathrm{kHz}$. The maximum LO frequency setting with these parameters is 1310.715 MHz .

Example:
For a Frequency RF Out $=517.125 \mathrm{MHz}$, $\mathrm{N}=517125 \mathrm{kHz} / 5 \mathrm{kHz}=103425$

An Upconverter PLL Lock indicator is used to insure that the frequency control circuits are operating properly. When the Upconverter PLL is locked, the frequency synthesizer IC is programmed and the Power Amplifier module(s) can be enabled.

The RF output of the LO/Upconverter Module is at J23 on the rear chassis.

Table 2-10. LO/Upconverter Front Panel Switch

| SWITCH | FUNCTI ON |
| :---: | :--- |
| MAN/AUTO AGC | When Manual AGC is selected, the reference AGC voltage is <br> set by the AGC Manual Gain front panel potentiometer. |
| When Auto AGC is selected, the RF power level control circuit <br> will automatically increase the RF output until the desired <br> output power is attained. |  |

Table 2-11. LO/Upconverter Front Panel Status Indicator

| LED | FUNCTI ON |
| :---: | :--- |
| AGC CUTBACK |  |
| (Red) |  | | When lit it indicates that the required gain to produce the desired |
| :--- |
| output power level has exceeded the level set by the AGC Cutback |
| (Override) adjust. Transmitter will cut back power to 25\% |

Table 2-12. LO/Upconverter Front Panel Control Adjustments

| POTENTI OMETERS | DESCRIPTI ON |
| :---: | :--- |
| MAN GAIN ADJ | Adjusts the gain of the transmitter when the transmitter is in the <br> Manual AGC position. |
| AGC CUTBACK ADJ | Adjusts the point at which the transmitter will cut back in power <br> when the Transmitter is in the Auto AGC position. |

Table 2-13. LO/Upconverter Front Panel Samples

| SMA CONNECTOR | DESCRIPTI ON |
| :---: | :--- |
| LO SAMPLE | Sample of the LO signal to the Upconverter as generated by the <br> UHF Generator Board. |
| RF SAMPLE | Sample of the On Channel RF Output of the Upconverter |

2.1.4 (A4) Control/ Power Supply Module Assembly ( 110 VAC, 1301936 or 220 VAC, 1303229; Appendix B)


The (A4) Control \& Monitoring/Power Supply Assembly is configured at the factory for operation at 110 VAC or 220 VAC. The assembly made up of a Control Board (1302021), a Power Protection Board (1302837) and a Switch Board (1527-1406). The Assembly also contains a switching power supply that provides $\pm 12$ VDC to the rest of the modules in the chassis and +32 VDC to the Power Amplifier module.

The Assembly provides all transmitter control and monitoring functions. The Front panel LCD allows monitoring of system parameters, including forward and reflected power, transistor currents, module temperatures and power supply voltages.

Table 2-14. Controller/Power Supply Display

| DISPLAY | FUNCTI ON |
| :---: | :--- |
| LCD | A 4 $\times 20$ display providing a four-line readout of the internal <br> functions, external inputs, and status. See Chapter 3, <br> Controller/Power Supply Display Screens, for a listing of displays. |

Table 2-15. Controller/Power Supply Status Indicator

| LED | FUNCTI ON |
| :---: | :--- |
| OPERATE | When lit it indicates that the transmitter is in the Operate Mode. If <br> transmitter is Muted the Operate LED will stay lit, the transmitter <br> will remain in Operate, until the input signal is returned. |
| FAULT <br> (red or green) | Red indicates that a problem has occurred in the transmitter. The <br> transmitter will be Muted or placed in Standby until the problem is <br> corrected. |
| DC OK <br> (red or green ) | Green indicates that the switchable fuse protected DC outputs that <br> connect to the modules in the transmitter are OK. |

Table 2-16. Controller/Power Supply Control Adjustments

| POTENTI OMETERS | DESCRIPTI ON |
| :---: | :---: |
| DISPLAY CONTRAST | Adjusts the contrast of the display for desired viewing of screen. |

### 2.1.5 (A6) Power Amplifier Module Assembly, Exciter, 100W Transmitter (1301923; Appendix B)



NOTE: The (A6) Power Amplifier Module Assembly (1301923) is used in the 10100 Watt Transmitter.

The (A6) Power Amplifier Module Assembly is made up of a Coupler Board Assembly (1301949), an Amplifier Control Board (1301962), a 1 Watt Module Assembly (1302891), a TFS 40W UHF Module (1206693) and a RF Module Pallet, Philips (1300116).

The Power Amplifier Module contains Broadband LDMOS amplifiers that cover the entire UHF band with no tuning required. They amplify the RF to the 10W to 100W output power level of the transmitter.

The Power Amplifier of the Transmitter/Exciter Driver is used to amplify the RF output of the Upconverter module. A cable, located on the rear chassis, connects the RF output from the LO/Upconverter at J23 to J24 the RF input to the PA Assembly. This module contains RF monitoring circuitry for both an analog and a digital system. Control and monitoring lines to the Power Amplifier module are routed through the floating blind-mate
connector of the Control \&
Monitoring/Power Supply module.
The 100 Watt Transmitter/Exciter Driver Power Amplifier module and any External Amplifier modules contain the same control and monitoring board. This board monitors RF output power, RF reflected power, the current draw of amplifier sections, the supply voltage, and the temperature of the PA heat sink.

The RF power detector circuit outputs vary with operating frequency. These circuits must be calibrated at their intended operating frequency. Front panel adjustment potentiometers are used to calibrate the following:

Table 1: Power Amplifier Calibration Adjustments in Analog Systems

R201 Reflected Power Cal
R202 Visual / Forward Power Cal
R203 Aural Power Cal
R204 Visual Offset Zero
R205 Aural Null
In analog systems, the Aural power of an Exciter Driver Power Amplifier and the Aural power of any external amplifier will not be reported by the system Control Monitoring module. Additionally the Visual power of these amplifiers, is reported as Forward Power just like in digital systems. In analog systems, aural and visual power will only be reported for the final system RF output.

In digital systems, the Forward power of an Exciter Driver Power Amplifier and the Forward power of any external amplifier, is reported by the system Control Monitoring module.

If the Control Monitoring module is monitoring a 5-50 Watt digital or 10-100 Watt analog Transmitter, system power is measured in the Power Amplifier module. The wired connections are transferred through the power supply connector to the backplane board on a five position header. All four positions
of control board switch SW1 must be set on to route these lines as the system's RF power signals. In systems of output power greater than 50 Watts digital or 100 Watts analog, system power is monitored by an external module that is connected to TB31 and control board SW1 switches must be set off.

The Forward Power of the Transmitter/Exciter Driver Power

Amplifier module is routed to the Upconverter module as AGC \#1. A system over-drive condition is detected when this value rises above 0.9 VDC. When an over-drive condition is detected, the Upconverter module reduces its RF output level. For values less than 0.9 VDC, the Upconverter uses this voltage for automatic gain.

Table 2-17. Power Amplifier Status Indicator

| LED | FUNCTI ON |
| :---: | :--- |
| ENABLED <br> (Green) | When lit Green, it indicates that the PA is in the Operate Mode. If a <br> Mute occurs, the PA will remain Enabled, until the input signal is <br> returned. |
| DC OK <br> (Green) | When lit Green, it indicates that the fuse protected DC inputs to the <br> PA module are OK. |
| TEMP <br> (Green) | When lit Green, it indicates that the temperature of the heatsink <br> assembly in the module is below $78^{\circ} \mathrm{C}$. |
| MOD OK <br> (Green) | When lit Green, it indicates that the PA Module is operating and has <br> no faults. |

Table 2-18. Power Amplifier Control Adjustments

| POTENTI OMETERS | DESCRI PTI ON |
| :---: | :--- |
| RFL CAL | Adjusts the gain of the Reflected Power monitoring circuit |
| VISUAL CAL | Adjusts the gain of the Visual / Forward Power monitoring circuit |
| AURAL CAL | Adjusts the gain of the Aural Power monitoring circuit |
| VISUAL ZERO | Adjusts the offset of the Forward Power monitoring circuit |
| AURAL NULL | Adjusts the offset of the Forward Power monitoring circuit based on <br> the Aural signal level. |

Table 2-19. Power Amplifier Sample

| DI SPLAY | FUNCTI ON |
| :---: | :--- |
| FWD SAMPLE | RF sample of the amplified signal being sent out the module on J25. |



NOTE: The (A6) Driver Amplifier Module Assembly (1302846) replaces the Power Amplifier Module Assembly (1301923) when the amplifier module is used as a driver for any external PA assemblies.

The (A6) Power Amplifier Module Assembly is made up of a Coupler Board

Assembly (1301949), an Amplifier Control Board (1301962), a 1 Watt Module Assembly (1302891) and a TFS 40W UHF Module (1206693).

The Driver Power Amplifier Module contains Broadband LDMOS amplifiers that cover the entire UHF band with no tuning required. They amplify the RF to the power level, 7 Watts Peak of Sync is maximum, that is needed to drive the external amplifiers to the output power level of the transmitter.

The Driver Power Amplifier is used to amplify the RF output of the Upconverter module. A cable, located on the rear chassis, connects the RF output from the LO/Upconverter at J23 to J24 the RF input to the driver PA Assembly. This module contains RF monitoring circuitry for both an analog and a digital system. Control and monitoring lines to the Driver Power Amplifier module are routed through the floating blind-mate connector of the Control \& Monitoring/Power Supply module.

The Driver Power Amplifier module and any External Amplifier modules contain the same control and monitoring board. This board monitors RF output power, RF reflected power, the current draw of amplifier sections, the supply voltage, and the temperature of the PA heat sink.

The RF power detector circuit outputs vary with operating frequency. These circuits must be calibrated at their intended operating frequency. Front panel adjustment potentiometers are used to calibrate the following:

Table 2: Power Amplifier Calibration Adjustments in Analog Systems

R201 Reflected Power Cal
R202 Visual / Forward Power Cal
R203 Aural Power Cal
R204 Visual Offset Zero
R205 Aural Null

In analog systems, the Aural power of an Exciter Driver Power Amplifier and the Aural power of any external PA amplifiers will not be reported by the system Control Monitoring module. Additionally the Visual power of these amplifiers, is reported as Forward Power just like in digital systems. In analog systems, aural and visual power will only be reported for the final system RF output.

In digital systems, the Forward power of an Exciter Driver Power Amplifier and the Forward power of any external amplifiers, are reported by the system Control Monitoring module.

If the Control Monitoring module is monitoring a 10-100 Watt Transmitter, system power is measured in the Power Amplifier module. The wired connections are transferred through the power supply connector to the backplane board on a five position header. All four positions of control board switch SW1 must be set on to route these lines as the system's RF power signals. In systems of output power greater than 100 Watts, system power is monitored by an external module that is connected to TB31. In this configuration switches SW1 on the control board must be set off.

The Forward Power of the Exciter Driver Power Amplifier module is routed to the Upconverter module as AGC \#1. A system over-drive condition is detected when this value rises above 0.9 VDC. When an over-drive condition is detected, the Upconverter module reduces its RF output level.
For values less than 0.9 VDC , the Upconverter uses this voltage for automatic gain.

Table 2-20. Driver Amplifier Status Indicator

| LED | FUNCTI ON |
| :---: | :--- |
| ENABLED <br> (Green) | When lit Green, it indicates that the PA is in the Operate Mode. If a <br> Mute occurs, the PA will remain Enabled, until the input signal is <br> returned. |
| DC OK <br> (Green) | When lit Green, it indicates that the fuse protected DC inputs to the <br> PA module are OK. |
| TEMP | When lit Green, it indicates that the temperature of the heatsink <br> assembly in the module is below $78{ }^{\circ} \mathrm{C}$. |
| MOD OK <br> (Green) | When lit Green, it indicates that the PA Module is operating and has <br> no faults. |

Table 2-21. Driver Amplifier Control Adjustments

| POTENTI OMETERS | DESCRI PTI ON |
| :---: | :--- |
| RFL CAL | Adjusts the gain of the Reflected Power monitoring circuit |
| VISUAL CAL | Adjusts the gain of the Visual / Forward Power monitoring circuit |
| AURAL CAL | Adjusts the gain of the Aural Power monitoring circuit |
| VISUAL ZERO | Adjusts the offset of the Forward Power monitoring circuit |
| AURAL NULL | Adjusts the offset of the Forward Power monitoring circuit based on <br> the Aural signal level.. |

Table 2-22. Driver Amplifier Sample

| DI SPLAY | FUNCTI ON |
| :---: | :---: |
| FWD SAMPLE | RF sample of the amplified signal being sent out the module on J25. |

### 2.1.6 RF Output Assemblies

The RF output from the driver power amplifier is at the RF output jack, an " N " connector J25, PA RF Output, of the chassis assembly. If this assembly is used as a driver the output connects to the input of the PA Assembly mounted beneath the Exciter Assembly. If this assembly is used as a 10 W to 100 W transmitter, then the output connects directly to the bandpass filter for the system.

The RF output of the transmitter is typically connected to a bandpass filter and then to a trap filter mounted on the rear of the assembly. The bandpass and trap filters are tuned to eliminate unwanted sideband and harmonic frequencies. Located on the output of the trap filter is a BNC output sample jack that can be used for test purposes.

### 2.2 Control and Status

The control and status of the exciter/amplifier Chassis assembly are found by operating the front panel display screen on the front of the assembly. Detailed information on the use of the screens is found in chapter 3.

### 2.2.1 Front Panel Display Screens

A $4 \times 20$ display located on the front of the Control \& Monitoring/Power Supply Module is used in the LX Series transmitter for control of the operation and display of the operating parameters of the transmitter.

### 2.3 System Operation

When the transmitter is in operate, as set by the menu screen located on the Control \& Monitoring Module. The IF

Processor will be enabled, the mute indicator on the front panel will be extinguished. The +32 VDC stage of the Power Supply in the Control \& Monitoring Module is enabled, the operate indicator on the front panel is lit and the DC OK on the front panel should also be green. The enable and DC OK indicators on the PA Module will also be green.

When the transmitter is in standby. The IF Processor will be disabled, the mute indicator on the front panel will be red. The +32 VDC stage of the Power Supply in the Control \& Monitoring Module is disabled, the operate indicator on the front panel will be extinguished and the DC OK on the front panel should remain green. The enable indicator on the PA Module is also extinguished.

If the transmitter does not switch to Operate when the operate menu is switched to Operate, check that all faults are cleared and that the remote control terminal block stand-by signal is not active.

The transmitter can be controlled by the presence of a modulated input signal. If the input signal to the transmitter is lost, the transmitter will automatically cutback and the input fault indicator on the IF Processor module will light. When the video input signal returns, the transmitter will automatically return to full power and the input fault indicator will be extinguished.

### 2.3.1 Principles of Operation

## Operating Modes

This transmitter is either operating or in standby mode. The sections below discuss the characteristics of each of these modes.

## Operate Mode

Operate mode is the normal mode for the transmitter when it is providing RF power output. To provide RF power to
the output, the transmitter will not be in mute. Mute is a special case of the operate mode where the +32 VDC section of the power supply is enabled but there is no RF output power from the transmitter. This condition is the result of a fault condition that causes the firmware to hold the IF Processor module in a mute state.

## Operate Mode with Mute Condition

The transmitter will remain in the operate mode but will be placed in mute when the following fault conditions exists in the transmitter.

- Upconverter is unlocked
- Upconverter module is not present
- IF Processor module is not present
- Modulator (if present) is in Aural/Visual Mute


## Entering Operate Mode

Entering the operate mode can be initiated a few different ways by the transmitter control board. A list of the actions that cause the operate mode to be entered is given below:

- A low on the Remote Transmitter Operate line.
- User selects "OPR" using switches and menus of the front panel.
- Receipt of an "Operate CMD" over the serial interface.

There are several fault or interlock conditions that may exist in the transmitter that will prevent the transmitter from entering the operate mode. These conditions are:

- Power Amplifier heat sink temperature greater than $78^{\circ} \mathrm{C}$.
- Transmitter is Muted due to conditions listed above.
- Power Amplifier Interlock is high indicating that the amplifier is not installed.


## Standby Mode

The standby mode in the transmitter indicates that the output amplifier of the transmitter is disabled.

## Entering Standby Mode

Similar to the operate mode, the standby mode is entered using various means. These are:

- A low on the Remote Transmitter Stand-By line.
- Depressing the "STB" key on selected front panel menus.
- Receipt of a "Standby CMD" over the serial interface.


## Operating Frequency

The LX Series transmitter controller is designed to operate on UHF frequencies. The exact output frequency of the transmitter can be set to one of the standard UHF frequencies, or it can be set to a custom frequency using software set-up menus. Since RF performance of the transmitter requires different hardware for different frequency bands, not all frequency configurations are valid for a specific transmitter. The Power detectors in the transmitter have frequency dependency, therefore detectors of power amplifiers are calibrated at their frequency of use. The detectors for System RF monitoring are also calibrated at the desired frequency of use.

Table 2-23: UHF Television Frequencies

| CH <br> $\#$ | FREQUENCY | CH <br> $\#$ | FREQUENCY | CH <br> $\#$ | FREQUENCY |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | $470-476 \mathrm{MHz}$ | 38 | $614-620 \mathrm{MHz}$ | 61 | $752-758 \mathrm{MHz}$ |
| 15 | $476-482 \mathrm{MHz}$ | 39 | $620-626 \mathrm{MHz}$ | 62 | $758-764 \mathrm{MHz}$ |
| 16 | $482-488 \mathrm{MHz}$ | 40 | $626-632 \mathrm{MHz}$ | 63 | $764-770 \mathrm{MHz}$ |
| 17 | $488-494 \mathrm{MHz}$ | 41 | $632-638 \mathrm{MHz}$ | 64 | $770-776 \mathrm{MHz}$ |
| 18 | $494-500 \mathrm{MHz}$ | 42 | $638-644 \mathrm{MHz}$ | 65 | $776-782 \mathrm{MHz}$ |
| 19 | $500-506 \mathrm{MHz}$ | 43 | $644-650 \mathrm{MHz}$ | 66 | $782-788 \mathrm{MHz}$ |
| 20 | $506-512 \mathrm{MHz}$ | 44 | $650-656 \mathrm{MHz}$ | 67 | $788-794 \mathrm{MHz}$ |
| 21 | $512-518 \mathrm{MHz}$ | 45 | $656-662 \mathrm{MHz}$ | 68 | $794-800 \mathrm{MHz}$ |
| 22 | $518-524 \mathrm{MHz}$ | 46 | $662-668 \mathrm{MHz}$ | 69 | $800-806 \mathrm{MHz}$ |
| 23 | $524-530 \mathrm{MHz}$ | 47 | $668-674 \mathrm{MHz}$ | 70 | $806-812 \mathrm{MHz}$ |
| 24 | $530-536 \mathrm{MHz}$ | 48 | $674-680 \mathrm{MHz}$ | 71 | $812-818 \mathrm{MHz}$ |
| 25 | $536-542 \mathrm{MHz}$ | 49 | $680-686 \mathrm{MHz}$ | 72 | $818-824 \mathrm{MHz}$ |
| 26 | $542-548 \mathrm{MHz}$ | 50 | $686-692 \mathrm{MHz}$ | 73 | $824-830 \mathrm{MHz}$ |
| 27 | $548-554 \mathrm{MHz}$ | 51 | $692-698 \mathrm{MHz}$ | 74 | $830-836 \mathrm{MHz}$ |
| 28 | $554-560 \mathrm{MHz}$ | 52 | $698-704 \mathrm{MHz}$ | 75 | $836-842 \mathrm{MHz}$ |
| 29 | $560-566 \mathrm{MHz}$ | 53 | $704-710 \mathrm{MHz}$ | 76 | $842-848 \mathrm{MHz}$ |
| 30 | $566-572 \mathrm{MHz}$ | 54 | $710-716 \mathrm{MHz}$ | 77 | $848-854 \mathrm{MHz}$ |
| 31 | $572-578 \mathrm{MHz}$ | 55 | $716-722 \mathrm{MHz}$ | 78 | $854-860 \mathrm{MHz}$ |
| 32 | $578-584 \mathrm{MHz}$ | 56 | $722-728 \mathrm{MHz}$ | 79 | $860-866 \mathrm{MHz}$ |
| 33 | $584-590 \mathrm{MHz}$ | 57 | $728-734 \mathrm{MHz}$ | 80 | $866-872 \mathrm{MHz}$ |
| 34 | $590-596 \mathrm{MHz}$ | 58 | $734-740 \mathrm{MHz}$ | 81 | $872-878 \mathrm{MHz}$ |
| 35 | $596-602 \mathrm{MHz}$ | 59 | $740-746 \mathrm{MHz}$ | 82 | $878-884 \mathrm{MHz}$ |
| 36 | $602-608 \mathrm{MHz}$ | 60 | $746-752 \mathrm{MHz}$ | 83 | $884-890 \mathrm{MHz}$ |
| 37 | $608-614 \mathrm{MHz}$ |  |  |  |  |

### 2.4 Customer Remote Connections

The remote monitoring and operation of the transmitter is provided through jacks TB30 and TB31 located on the rear of the chassis assembly. If remote connections
are made to the transmitter, they must be made through plugs TB30 and TB31 at positions noted on the transmitter interconnect drawing and Table 2-20.


Table 2-24: LX Series Chassis Assembly Hard Wired Remote Interface Connections to TB30 or TB31, 18 pos. Terminal Blocks Located on the Rear of the Assembly

| Signal Name | Pin <br> Designations | Signal Type/ Description |
| :--- | :--- | :--- |
| RMT Transmitter <br> State | TB30-1 | Discrete Open Collector Output - A low indicates that the <br> transmitter is in the operate mode. |
| RMT Transmitter <br> Interlock | TB30-2 | Discrete Open Collector Output - A low indicated the <br> transmitter is OK or completes a interlock daisy chain. <br> When the transmitter is not faulted, the interlock circuit <br> is completed. |
| RMT Transmitter <br> Interlock <br> Isolated Return | TB30-3 | Ground - Configurable ground return which can be either <br> jumpered directly to ground or it can be the "source" pin <br> of an FET so that the transmitter interlock can be daisy <br> chained with other transmitters. This signal does not <br> directly interface to the microcontroller. |
| RMT AUX IO 1 | TB30-4 | Discrete Open Collector Inputs, Discrete Open Drain <br> Outputs, or 0 - 5 VDC Analog Input - When used as an <br> output, this line is pulled to +5 VDC with a 1.0 k $\Omega$ <br> resistor for logic high and pulled to ground for a low. A <br> diode allows this line to be pulled up to 12 VDC. When <br> used as a digital input, this line considers all values over <br> 2 Volts as high and those under 1 volt as low. As an <br> analog input, this line is protected by a 5.1 zener diode. |
| RMT AUX IO 2 | TB30-5 | Discrete Open Collector Input - A pull down to ground on <br> this line indicates that the transmitter is to be placed into <br> the operate mode. |
| RMT <br> Transmitter <br> Operate | TB30-6 | TBO |


| Signal Name | Pin Designations | Signal Type/ Description |
| :---: | :---: | :---: |
| RMT <br> Transmitter Stand-By | TB30-7 | Discrete Open Collector Input - A pull down to ground on this line indicates that the transmitter is to be placed into the standby mode. |
| RMT Power Raise | TB30-8 | Discrete Open Collector Input - A pull down to ground on this line indicates that the transmitter power is to be raised. |
| RMT Power Lower | TB30-9 | Discrete Open Collector Input - A pull down to ground on this line indicates that the transmitter power is to be lowered. |
| RMT <br> System Reflect Power | TB30-10 | Analog Output - 0 to 4.0 V - This is a buffered loop through of the calibrated "System Reflected Power" and indicates the transmitter's reflected output power. The scale factor is $25 \% / 3.2 \mathrm{~V}$. |
| RMT System Visual/Forward Power | TB30-11 | Analog Output - 0 to 4.0 V - This is a buffered loop through of the calibrated "System Visual/Avg. Power". Indicates the transmitter's Visual / Average power. Scale factor is $100 \% / 3.2 \mathrm{~V}$. |
| RMT <br> System Aural Power | TB30-12 | Analog Output - 0 to 4.0 V - This is a buffered loop through of the calibrated "System Aural Power". Indicates the transmitter's forward Aural output power. The scale factor is $100 \% / 3.2 \mathrm{~V}$. |
| RMT Spare 1 | TB30-13 | Remote connection to spare module - Use is TBD. |
| RMT Spare 2 | TB30-14 | Remote connection to spare module - Use is TBD. |
| System Reflect Power | TB31-13 | Analog Input - 0 to 1.00 V - This is the input of the "System Reflected Power" indicating the transmitter's reflected output power. The scale factor is $25 \% / 0.80 \mathrm{~V}$. |
| System Visual / Forward Power | TB31-14 | Analog Input - 0 to 1.00 V - This is the input of the "System Visual / Forward Power" indicating the transmitter's forward Visual / Forward output power. The scale factor is $100 \% / 0.80 \mathrm{~V}$. |
| System Aural Power | TB31-15 | Analog Input - 0 to 1.00 V - This is the input of the "System Aural Power " indicating the transmitter's forward Aural output power. The scale factor is 100\%/0.80V. |
| IF Processor <br> IF Signal Select | TB31-3 | Discrete Open Collector Input - A low indicates that the modulator IF source is to be used by the IF Processor module. When floating an analog IP Processor module may use the Modulated IF Input if the IF Processor sled is so configured. |
| IF Processor DLC Voltage | TB31-4 | Analog Output - 0 to 5.00 V - This is the input of IF Processor module for digital system RF output power control. |
| UC AGC \#2 <br> Voltage | TB31-5 | Auxiliary Analog Input - 0 to 1 V - This voltage is used by the Upconverter for gain control. Linear signal with display resolution of 0.01 \%. Primary signal source is J34-1. |
| RMT Ground | $\begin{aligned} & \text { TB30-15, and } \\ & 17 \end{aligned}$ | Ground pins available through Remote |
| RMT Ground | $\begin{aligned} & \hline \text { TB31-1, 2, } 6 \\ & \text { to } 12, \text { and } 17 \\ & \hline \end{aligned}$ | Ground pins available through Remote |


| Signal Name | Pin <br> Designations | Signal Type/ Description |
| :--- | :--- | :--- |
| RMT +12 VDC | TB30-16 <br> TB31-16 | +12 VDC available through Remote w/ 2 Amp re-settable <br> fuse |
| RMT -12 VDC | TB30-18 <br> TB31-18 | -12 VDC available through Remote w/ 2 Amp re-settable <br> fuse |

## Chapter 3 <br> Site Considerations, Installation and Setup Procedures

There are special considerations that need to be taken into account before the Innovator LX Series analog driver/transmitter can be installed. For example, if the installation is completed during cool weather, a heat-related problem may not surface for many months, suddenly appearing during the heat of summer. This section provides planning information for the installation and set up of the driver/transmitter.

### 3.1 Site Considerations

The transmitter requires an AC input line of 117 VAC/220 VAC @ 5 amps for the 10W transmitter and driver or 117 VAC/ 220 VAC @ 10 amps for the 100W Transmitter. The transmitter is factory set for 110 VAC or 230 VAC operation.

The LX Series Analog Transmitters are designed and built to provide long life with a minimum of maintenance. The environment in which they are placed is important and certain precautions must be taken. The three greatest dangers to the transmitter are heat, dirt, and moisture. Heat is usually the greatest problem, followed by dirt, and then moisture. Over-temperature can cause heat-related problems such as thermal runaway and component failure. Each amplifier module in the transmitter contains a thermal interlock protection circuit that will shut down that module until the temperature drops to an acceptable level.

A suitable environment for the transmitter can enhance the overall performance and reliability of the transmitter and maximize revenues by minimizing downtime. A properly designed facility will have an adequate supply of cool, clean air, free of airborne particulates of any kind, and no excessive humidity. An ideal environment will require temperature in the range of
$40^{\circ} \mathrm{F}$ to $70^{\circ} \mathrm{F}$ throughout the year, reasonably low humidity, and a dust-free room. It should be noted that this is rarely if ever attainable in the real world. However, the closer the environment is to this design, the greater the operating capacity of the transmitter.

The fans are designed and built into the transmitter will remove the heat from within the modules, but additional means are required for removing this heat from the building. To achieve this, a few issues need to be resolved. The first step is to determine the amount of heat to be removed from the transmitter room. There are generally three sources of heat that must be considered. The first and most obvious is the heat from the transmitter itself. This amount can be determined for a 100W transmitter by subtracting the average power to the antenna ( 69.5 watts) from the AC input power ( 675 watts) and taking this number in watts (605.5) and then multiplying it by 3.41 . This gives a result of 2,065 , the BTUs to be removed every hour. 12,000 BTUs per hour equals one ton. Therefore, a $1 / 4$-ton air conditioner will cool a 100W transmitter.

The second source of heat is other equipment in the same room. This number is calculated in the same way as the equation for BTUs. The third source of heat is equally obvious but not as simple to calculate. This is the heat coming through the walls, roof, and windows on a hot summer day. Unless the underside is exposed, the floor is usually not a problem. Determining this number is usually best left up to a qualified HVAC technician. There are far too many variables to even estimate this number without reviewing the detailed drawings of the site that show all of the construction details. The sum of these three sources is the bulk of the heat that must be removed. There may be other
sources of heat, such as personnel, and all should be taken into account.

Now that the amount of heat that must be removed is known, the next step is to determine how to accomplish this. The options are air conditioning, ventilation, or a combination of the two. Air conditioning is always the preferred method and is the only way to create anything close to an ideal environment.

Ventilation will work quite well if the ambient air temperature is below $100^{\circ} \mathrm{F}$, or about $38^{\circ} \mathrm{C}$, and the humidity is kept at a reasonable level. In addition, the air stream must be adequately filtered to ensure that no airborne particulates of any kind will be carried into the transmitter. The combination of air conditioning for summer and ventilation during the cooler months is acceptable when the proper cooling cannot be obtained through the use of ventilation alone and using air conditioning throughout the year is not feasible.

## Caution: The use of air conditioning and ventilation simultaneously is not recommended. This can cause condensation in the transmitters.

The following precautions should be observed regarding air conditioning systems:

1. Air conditioners have an ARI nominal cooling capacity rating. In selecting an air conditioner, do not assume that this number can be equated to the requirements of the site. Make certain that the contractor uses the actual conditions that are to be maintained at the site in determining the size of the air conditioning unit. With the desired conditioned room temperature under $80^{\circ} \mathrm{F}$, the unit must be derated, possibly by a substantial amount.
2. Do not have the air conditioner blowing directly onto the transmitter. Under certain conditions, condensation may occur on, or worse in, the transmitter.
3. Do not separate the front of the transmitter from the back with the thought of air conditioning only the front of the unit. Cooling air is drawn in at the front of all transmitters and in the front and back of others. Any attempt to separate the front of the transmitter from the rear of the unit will adversely affect the flow of cooling air.
4. Interlocking the transmitter with the air conditioner is recommended to keep the transmitter from operating without the necessary cooling.
5. The periodic cleaning of all filters is a must.

When using ventilation alone, the following general statements apply:

1. The blower, with attendant filters, should be on the inlet, thereby pressurizing the room and preventing dirt from entering the transmitter.
2. The inlet and outlet vents should be on the same side of the building, preferably the leeward side. As a result, the pressure differential created by wind will be minimized. Only the outlet vent may be released through the roof.
3. The inlet and outlet vents should be screened with 1/8-inch hardware cloth (preferred) or galvanized hardware cloth (acceptable).
4. Cooling air should enter the room as low as practical but in no case
higher than four feet above the floor. The inlet must be located where dirt, leaves, snow, etc., will not be carried in with the cooling air.
5. The exhaust should be located as high as possible. Some ducting is usually required to insure the complete flushing of heated air with no stagnant areas.
6. The filter area must be large enough to insure a maximum air velocity of 300 feet per minute through the filter. This is not a conservative number but a neverexceed number. In a dusty or remote location, this number should be reduced to 150 CFM.
7. The inlet and outlet(s) must have automatic dampers that close any time the ventilation blower is off.
8. In those cases in which transmitters are regularly off for a portion of each day, a temperature-differential sensor that controls a small heater must be installed. This sensor will monitor inside and outside temperatures simultaneously. If the inside temperature falls to within $5^{\circ} \mathrm{F}$ of the outside temperature, the heater will come on. This will prevent condensation when the ventilation blower comes on and should be used even in the summer.
9. A controlled-air bypass system must be installed to prevent the temperature in the room from falling below $40^{\circ} \mathrm{F}$ during transmitter operation.
10. The blower should have two speeds, which are thermostatically controlled, and be interlocked with the transmitter.
11. The blower on high speed must be capable of moving the required volume of air into a half inch of water pressure at the required elevation. The free air delivery method must not be used.
12. Regular maintenance of the filters, if used, can not be overemphasized.
13. Above 4000 feet, for external venting, the air vent on the cabinet top must be increased to an 8 -inch diameter for a 1-kW transmitter and to a 10 -inch diameter for $5-\mathrm{kW}$ and $6-\mathrm{kW}$ transmitters. An equivalent rectangular duct may be used but, in all cases, the outlet must be increased by $50 \%$ through the outlet screen.
14. It is recommended that a site plan be submitted to Axcera for comments before installation begins.

In calculating the blower requirements, filter size, and exhaust size, if the total load is known in watts, 2000 CFM into $1 / 2$ inch of water will be required for each 5000 watts. If the load is known in BTUs, 2000 CFM into $1 / 2$ inch of water will be required for each 17,000 BTUs. The inlet filter must be a minimum of seven square feet, larger for dusty and remote locations, for each 5000 watts or 17,000 BTUs. The exhaust must be at least four square feet at the exhaust screen for each 5000 watts or 17,000 BTUs.

The information presented in this section is intended to serve only as a general guide and may need to be modified for unusually severe conditions. A combination of air conditioning and ventilation should not be difficult to design (see Figure 3-1).

System interlocking and thermostat settings should be reviewed with Axcera. As with any equipment installation, it is
always good practice to consult the manufacturer when questions arise.

Axcera can be contacted at (724) 8738100.


Figure 3-1. 1 kW Minimum Ventilation Configuration

### 3.2 Unpacking the Chassis w/ modules, bandpass and trap filters

Thoroughly inspect the chassis with modules and all other materials upon their arrival. Axcera certifies that upon leaving our facility the equipment was undamaged and in proper working order. The shipping containers should be inspected for obvious damage that indicates rough handling.

Remove the chassis and modules, along with bandpass filter and trap Filter, from the crates and boxes.

Check for dents and scratches or broken connectors, switches, display, or connectors. Any claims against in-transit damage should be directed to the carrier. Inform Axcera as to the extent of any damage as soon as possible.

The modules are mounted to the chassis assembly with slides that are on the top and the bottom of the modules. There are two thumb screws on the front panel that hold each of the modules in place.

### 3.3 I nstalling the Chassis w/ modules and filters

The chassis assembly is made to mount in a standard 19 " rack. The chassis assembly mounts using the four \#10 clearance mounting holes on the ends. The chassis should be positioned; to provide adequate air intake into the front and the air exhaust of the fan in the rear; the ability to slide the modules out for replacement purposes; the installation of the bandpass filter and trap filter; the coupler assembly; and output transmission line. The chassis or cabinet in which it is mounted should be grounded using copper strapping material.

NOTE: To pull out the power amplifier module for replacement purposes, the input and output coaxial cables must first be removed from the rear of the chassis assembly.


Connect the bandpass filter and trap filter to the output of the chassis assembly.

Figure 3-2. Front and Rear View Reconnection Drawing

Connect the transmission line for the antenna system to the output of the trap filter. A BNC sample jack of the output on the trap filter can be used for test purpose.

### 3.4 AC Input

The Exciter/Amplifier chassis assembly needs an AC outlet in which to plug, of 115 or 230 VAC, as set at the factory, at 5 amps for the 10 W and driver or 10 amps for the 100W transmitter.

When the AC power cord for the exciter/amplifier chassis is plugged in, the $A C$ is always connected to the transmitter.

Once the chassis and output connections are in place, the AC cord from the chassis can plug into an AC outlet, 110 or 220 VAC as configured at the factory, of 5 Amps for the 10W transmitter and driver or 10 Amps for the 100 W transmitter.

This completes the unpacking and installation of the LX Series UHF television transmitter. Refer to the setup and operation procedures that follow before applying power to the transmitter.

### 3.5 Setup and Operation

Initially, the transmitter should be turned on with the RF output at the Trap Filter terminated into a dummy load of 10W or 100W depending on the power rating of the transmitter. If a load is not available, check that the output of the trap filter is connected to the antenna for your system.

### 3.5.1 Input Connections

The input connections to the transmitter are to the rear of the Chassis Assembly for the transmitter or to the receiver tray in a translator.

Refer to the tables and description that follows for detailed information on the input connections.

Figure 3-3: Rear View of LX Series Analog Transmitter


Table 3-1: Rear Chassis Connections for the LX Series Analog Transmitter.

| Port | Type | Function | Ohm |
| :---: | :--- | :--- | :---: |
| J1 | IEC | AC Input |  |
| TB02 | Term | Base Band Audio Input | 600 |
| J3 | BNC | Composite Audio Input | 75 |
| J4 | BNC | SAP / PRO Audio Input | 50 |
| J5 | BNC | CW IF Input | 50 |
| J6 | BNC | Modulated IF Input | 75 |
| J7 | BNC | Video Input (Isolated) | 50 |
| J8 | BNC | Visual IF Loop-Thru Output | 50 |
| J9 | BNC | Aural IF Loop-Thru Output | 50 |
| J10 | BNC | 10 MHz Reference Input | 50 |
| J11 | BNC | 10 MHz Reference Output | 75 |
|  |  |  | 50 |
| J17 | BNC | Video Loop-Thru (Isolated) | 50 |
| J18 | BNC | Visual IF Loop-Thru Input |  |
| J19 | BNC | Aural IF Loop-Thru Input | 50 |
|  |  |  | 50 |
| J23 | BNC | Upconverter RF Output | 50 |
| J24 | BNC | Power Amplifier RF Input |  |
| J25 | N | Power Amplifier RF Output |  |
|  |  |  | Remote Control \& Monitoring |
| TB30 | Term | Rem |  |
| TB31 | Term | Remote Control \& Monitoring | CAT5 |
| J32 | RJ-45 | SCADA (Input / Loop-Thru) | CAT5 |
| J33 | RJ-45 | SCADA (Input / Loop-Thru) | CAT5 |
| J34 | RJ-45 | System RS-485 Serial |  |

### 3.5.2 Front Panel Screens for the Exciter/ Amplifier Chassis Assembly

A $4 \times 20$ display located on the front of the Control \& Monitoring/Power Supply Module is used in the LX Series transmitter for control of the operation and display of the operating parameters of the transmitter. Below are the display screens for the system. The $\uparrow$ and $\downarrow$
characters are special characters used to navigate up or down through the menu screens. Display text flashes on discrete fault conditions for all screens that display a fault condition.

When the transmitter is in operate mode, the STB menu appears. When the transmitter is in standby mode, the OPR menu appears.

## Display Menu Screens for the LX Series Transmitter

Table 3-2: Menu 01 - Splash Screen \#1

| A | X | C | E | R | A |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 0 | 3 |  | $F$ | R | E | E | D | O | M |  | D | R | I | V | E |  |  |
| L | A | W | R | E | N | C | E | , |  | P | A | . |  | 1 | 5 | 0 | 5 | 5 |
| 1 | 7 | 2 | 4 | $)$ |  | 8 | 7 | 3 | - | 8 | 1 | 0 | 0 |  |  |  |  |  |

This is the first of the two transmitter splash screens that is shown for the first few seconds after reset.

Table 3-3: Menu 02- Splash Screen \#2

| P | I | O | N | E | E | R |  |  |  | L | D | U | 4 | 0 | 0 | 0 | A | T | D |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| C | O | D | E |  | V | E | R | S | I | O | N |  |  |  |  | 1 | . | 0 |  |
| F | I | R | M | W | A | R | E |  |  |  |  |  | 1 | 3 | 0 | 2 | 1 | 6 | 4 |
| S | C | A | D | A |  | A | D | D | R | E | S | S |  |  |  |  |  |  | 5 |

This is the second of the two transmitter splash screens

Table 3-4: Menu 10 - Main Screen


This is the default main screen of the transmitter. When the transmitter is in operate, the 'STB' characters appear allowing an operator to place the transmitter in STAND-BY. When the transmitter is in standby the 'STB' characters are replaced with 'OPR' and an operator can place the transmitter into OPERATE by pressing the right most switch on the front panel display. If the $\downarrow$ key is activated the system changes to Menu 11, go to Menu 11. If the $\uparrow$ key is activated the system displays to Menu 13, go to Menu 13.

Table 3-5: Menu 11 - Error List Access Screen


This screen of the transmitter shows the current number of errors and provides operator access to view the error list. This is the entry point to Menu 20. If ENT is pushed, go to Menu 20. If the $\downarrow$ key is activated the system changes to Menu 12 , go to Menu 12. If the $\uparrow$ key is activated the system returns to Menu 10, go to Menu 10.

Table 3-6: Menu 12 - Transmitter Device Data Access Screen


This screen of the transmitter allows access to various parameters of the transmitter system. This is the entry point to Menu 30. If ENT is pushed, go to Menu 30. If the $\downarrow$ key is activated the system changes to Menu 13, go to Menu 13. If the $\uparrow$ key is activated the system returns to Menu 11, go to Menu 11.

Table 3-7: Menu 13 - Transmitter Configuration Access Screen


This screen of the transmitter allows access to various software setting of the transmitter system. This is the entry point to Menu 40. If ENT is pushed, go to Menu 40. If the $\downarrow$ key is activated the system returns to Menu 10, go to Menu 10. If the $\uparrow$ key is activated the system returns to Menu 12, go to Menu 12.

Table 3-8: Menu 20 - Error List Display Screen


This screen of the transmitter allows access to system faults. Fault logging is stored in non-volatile memory. The transmitter's operating state can not be changed in this screen. The 'CLR' switch is used to clear previously detected faults that are no longer active. The $\uparrow$ key and $\downarrow$ key allow an operator to scroll through the list of system errors that have occurred. The ESC switch is used to leave this screen.

Table 3-9: Menu 30 - Transmitter Device Details Screen


This screen of the transmitter allows access to the transmitter parameters of installed devices. The system is configured to know which devices are present. Current values for all installed devices are shown. If a module is not installed, only a "MODULE NOT PRESENT" message will be displayed. The $\uparrow$ and $\downarrow$ arrows scroll through the different parameters of each device as shown in table 3-11. Each System Component is a different screen. One IF Processor or the other will be programmed for your system. One Power Amplifier or the other will be programmed for your system. External Amplifier will only be used in high power transmitters.

Table 3-10: Menu 30-1 - System Details Screen


Table 3-11: Transmitter Device Parameters Detail Screens

| System Component | Parameter | Normal | Faulted (Blinking) |
| :---: | :---: | :---: | :---: |
| Modulator Details | PLL CIRCUIT | LOCKED | UNLOCKED |
|  | OUTPUT LEVEL | 0-200 IRE | N/A |
|  | AURAL DEVIATION | 0-125 kHz | N/A |
|  | CW INPUT | PRESENT | NOT USED |
|  | STATION ID | SEND soft key | N/A |
| IF Processor Details (Analog Systems) | INPUT SIGNAL STATE | OK | FAULT |
|  | MODULATION | OK | FAULT |
|  | INPUT IF | MODULATOR or J6 | N/A |
|  | DLC LEVEL | $0-5.00 \mathrm{~V}$ | N/A |
|  | ALC LEVEL | 0-5.00 V | N/A |
|  | ALC MODE | AUTO or MANUAL | N/A |
| (OR) IF Processor Details (Digital Systems) | ALC LEVEL | 0-5.00 V | N/A |
|  | ALC MODE | AUTO or MANUAL | N/A |
|  | DLC LEVEL | $0-5.00 \mathrm{~V}$ | N/A |
| Upconverter Details | PLL CIRCUIT | LOCKED | FAULT |
|  | AFC LEVEL | $0-5.00 \mathrm{~V}$ | N/A |
|  | AGC 1 LEVEL | $0-5.00 \mathrm{~V}$ | N/A |
|  | AGC 2 LEVEL | 0-5.00 V | N/A |
|  | EX. 10 MHz | PRESENT or NOT USED | N/A |
|  | LO FREQ | xxx.xxx MHz | N/A |
| Driver and PA Details | POWER SUPPLY STATE | ON or OFF | N/A |
|  | $\pm 12 \mathrm{~V}$ SUPPLY | OK or OFF | FAULT |


| System Component | Parameter | Normal | Faulted (Blinking) |
| :---: | :---: | :---: | :---: |
|  | FORWARD POWER | xxx\% | xxx\% |
|  | REFLECTED POWER | xxx\% | xxx\% |
|  | AMP 1 CURRENT | xx.xA | xx.xA |
|  | AMP 2 CURRENT | xx.xA | XX. XA |
|  | TEMPERATURE | xxC | xxC |
|  | CODE VERSION | X. X | N/A |
| Ext. Power Amplifier Modules Details (Only in high power systems) | POWER SUPPLY STATE | ON or OFF | N/A |
|  | $\pm 12 \mathrm{~V}$ SUPPLY | OK or OFF | FAULT |
|  | FORWARD POWER | xxx\% | xxx\% |
|  | REFLECTED POWER | xxx\% | xxx\% |
|  | AMP CURRENT 1 | xx.xA | xx.xA |
|  | AMP CURRENT 2 | xx.xA | XX. XA |
|  | AMP CURRENT 3 | xx.xA | xx.xA |
|  | AMP TEMPERATURE | xxC | xxC |
|  | CODE VERSION | X. X | N/A |

Table 3-12: Menu 40-Transmitter Set-up: Power Raise/Lower Screen


This screen of the transmitter is the first of several that allows access to transmitter setup parameters. When + is selected, the Power will increase. When - is selected, the Power will decrease.

Table 3-13: Menu 40-1 - Transmitter Set-up: Model Select Screen


This screen is used to specify which components are expected to be part of the system. By specifying the model number, the transmitter control firmware knows which components should be installed and it will be able to display faults for components that are not properly responding to system commands.

Table 3-14: Menu 40-2 - Transmitter Set-up: Frequency Select Screen


This screen of the transmitter is allows access to transmitter frequency set-up parameters. The choices of this screen are 'TABLE' or 'CUSTOM'. When table is selected, the next menu will be used to select the desired operating frequency. When custom is selected, the next menu is used to select a specific operating frequency.

Table 3-15: Menu 40-3 - Transmitter Set-up: Frequency Table Select Screen


The choices of this screen are from the standard UHF / VHF tables. + and - change the desired value of the transmitter. Any change to frequency is immediately set to the LO / Upconverter Frequency Synthesizer PLL circuit.

Table 3-16: Menu 40-4 - Transmitter Set-up: IF Frequency Screen


This screen is used to specify the IF Input frequency. This value plus the desired channel value is used to calculated the desired LO frequency. + is used to increase the selected value from 0 to 9 . The $>$ key is used to select from each of the different fields that make up the desired frequency. Any change to frequency is immediately set to the LO / Upconverter Frequency Synthesizer PLL circuit.

Table 3-17: Menu 40-5 - Transmitter Set-up: Custom Frequency Select Screen


This screen is used to specify the operating frequency to an exact value. + is used to increase the selected value from 0 to 9 . The > key is used to select from each of the different fields that make up the desired frequency. Any change to frequency is immediately set to the LO / Upconverter Frequency Synthesizer PLL circuit.

Table 3-18: Menu 40-6 - Transmitter Set-up: Serial Address Screen


This screen allows the user to set the serial address of the transmitter. The default address is 5 . This value and all other set-up parameters, are stored in non-volatile memory.

Table 3-19: Menu 40-7 - Transmitter Set-up: Station ID Screen


This screen allows the user to set the serial address of the transmitter. The default address is 5 . This value and all other set-up parameters, are stored in non-volatile memory.

Table 3-20: Menu 40-8 - Transmitter Set-up: System Visual Power Calibration


This screen is used to adjust the calibration of the system's visual power. A symbol placed under the ' 6 ' character is used to show minor changes in the calibration value. When the calibration value is at full value, the character will be full black. As the value decreases, the character pixels are gradually turned off.

Table 3-21: Menu 40-9 - Transmitter Set-up: System Aural Power Calibration


This screen is used to adjust the calibration of the system's aural forward power. A symbol as on the previous screen is under the '6' character on this screen.

Table 3-22: Menu 40-10 - Transmitter Set-up: System Reflected Power Calibration

|  | R | A | N | S | M | 1 | T | T | E | R |  | S | E | T | - |  |  | P |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 6 |  | S | Y | S | T | E | M |  | C | A | L | 1 | B | R | A |  | T | E |  |
|  |  |  | R | E | F | L | E | C | T |  | P | W | R |  | X |  |  | X | \% |  |
|  | $\uparrow$ |  |  |  | $\downarrow$ |  |  | $($ | + | ) |  | E | S | C |  |  |  | 1 | - |  |

This screen is used to adjust the calibration of the system's reflected power.
Table 3-23: Menu 40-11 - Transmitter Set-up: Forward Power Fault Threshold Screen


This screen is used to set the minimum forward power fault threshold. When the transmitter is operating, it must operate above this value otherwise the system will shut down with fault for 5 minutes. If after five minutes the fault is not fixed, the transmitter will enable, measure power less than this value and again shut down for five minutes.

Table 3-24: Menu 40-12 - Transmitter Set-up: Reflected Power Fault Threshold


This screen is used to set the maximum reflected power fault threshold. When the transmitter is operating, it must not operate above this value otherwise the system will shut down with fault for 5 minutes. If after five minutes the fault is not fixed, the transmitter will enable, measure power above this value and again shut down for five minutes.

Table 3-25: Menu 40-13- Transmitter Set-up: Remote Commands Control


This screen is used to allow or deny the use of remote control commands. When disabled, remote commands are not used. Remote commands are commands received either through the rear terminal blocks or through serial messages.

This completes the description of the screens for the LX Series exciter/amplifier chassis assembly.

If the transmitter is already connected to the antenna, check that the output is $100 \%$. If necessary, adjust the
amplifier power detection circuitry or LO / Upconverter AGC settings. The power raise / lower settings are only to be used for temporary reductions in power. The power set-back values do not directly correspond to the power of the transmitter. Setting for $50 \%$
output sets a linear circuit voltage that is controlling a non-linear power circuit.

If a problem occurred during the setup and operation procedures, refer to Chapter 5, Detailed Alignment Procedures, of this manual for more information.

### 3.5.3 I nitial Turn On

Once the unit has been installed and all connections have been made, the process of turning on the equipment can begin. First verify that AC power is present and connected to the transmitter. Verify all cables are properly connected and are the correct type. Once all of these things are done, the unit is ready to be turned on following the procedures below.

Turn on the main AC power source that supplies the $A C$ to the transmitter. Check that the AC power plug is connected to J1 on the rear of the chassis assembly.

Monitor the LCD display located on the front of the control/monitoring module as you proceed through this section. When the transmitter is in the operate mode, the STB menu appears. When in the standby mode, the OPR menu appears. Press the NXT key after each menu to continue through the sequence.

## MODULATOR MODULE LEDs ON FRONT PANEL

## Fault I ndicators:

AUR UNLOCK: This illuminates Red when the Aural IF PLL is unlocked.

VIS UNLOCK: This illuminates RED when the Visual IF PLL is unlocked.

AUD OV DEV: This indicator will illuminate Red when the audio overdeviates the aural carrier.

VIDEO LOSS: This indicates the loss of Video to the modulator, when Red.

OVER MOD: This illuminates Red when the video is overmodulated.

## Status Indicators:

ALT IF CW: This indicates that there is an external IF CW signal applied to the Modulator

10MHz PRES: This indicates the presence of a 10 MHz reference input.

## IF PROCESSOR MODULE LEDs ON FRONT PANEL

## Fault Indicators:

INPUT FAULT: This illuminates Red if the input to the module is missing or low.

ALC FAULT: This illuminates RED when the needed ALC value to maintain the output level is beyond the range of the circuitry.

MUTE: This indicator will illuminate Red when the transmitter is muted.

## UPCONVERTER MODULE LED ON FRONT PANEL

## Fault Indicator:

AGC CUTBACK-This illuminates Red if the required gain to produce the desired output level is beyond the value set by the AGC Cutback circuit.

## CONTROLLER MODULE LEDs ON FRONT PANEL

Status Indicators:
OPERATE - This illuminates Green when transmitter is in operate.

FAULT - This illuminates Red when a fault has occurred in the transmitter.

DC OK - This illuminates Green when the DC outputs that connect to the modules in the transmitter are present.

## POWER AMPLIFIER OR DRI VER MODULE LEDs ON FRONT PANEL

NOTE: Both the PA Module and Driver Module have the same front panel LEDs.

## Status I ndicators:

ENABLED - This illuminates Green when the PA is in operate.

DC OK - This illuminates Green when the DC inputs to the PA module are present.

TEMP - This illuminates Green when the temperature of the heatsink in the PA is below $78^{\circ} \mathrm{C}$.

MOD OK - This illuminates Green when the PA module is operating and has no faults.

This completes the Installation, Set Up and Turn On of the Driver/Transmitter.

# Chapter 4 Circuit Descriptions 

## 4.1 (A2) Modulator Module (1301929; Appendix B)

NOTE: Not used in a translator system.

### 4.1.1 Analog Modulator Board (1301797; Appendix B)

The board takes the audio and video inputs and produces a modulated visual IF + aural IF output.

## Main Audio and Aural IF portion of the board

The analog modulator board takes each of the three possible audio inputs and provides a single audio output.
4.1.1.1 MONO, Balanced Audio Input

The first of the three possible baseband inputs to the board is a $600-\Omega$, balancedaudio input ( 0 to +10 dBm ) that enters through jack J41A, pins 10A (+), 12A (GND), and 11A ( - ), and is buffered by U11A and U11B. Diodes CR9, CR10, CR12 and CR13 protect the input to U11A and U11B if an excessive signal level is present on the input. The outputs of U11A and U1B are applied to differential amplifier U11C. U11C eliminates any common mode signals (hum) on its input leads. A pre-emphasis of 75 ms is provided by R97, C44, and R98 and can be eliminated by removing jumper W6 on J22. The signal is then applied to amplifier U11D whose gain is controlled by jumper W7 on J23. Jumper W7 on jack J23 is positioned according to the input level of the audio signal ( 0 or +10 dBm ). If the input level is approximately 0 dBm , the mini-jumper should be in the high gain position between pins 1 and 2 of jack J23. If the input level is approximately +10 dBm , the minijumper should be in low gain position between pins 2 and 3 of jack J23. The balanced audio is then connected to buffer amplifier U12A whose input level is
determined by the setting of the MONO, balanced audio gain pot R110, accessed through the front panel. The output of the amplifier stage is wired to the summing point at U13C, pin 9.

### 4.1.1.2 STEREO, Composite Audio Input

The second possible audio input to the board is the composite audio (stereo) input that connects to the board at J41A Pin 14A $(+)$ and J41A Pin 13A (-).

NOTE: For the transmitter to operate using the composite audio input the Jumper W1 on J4 must be between Pins 2 and 3, the Jumper W2 on J6 must be between Pins 2 and 3 and the Jumper W4 on J5 must be between Pins 1 and 2. These jumpers connect the composite audio to the rest of the board.

Jumper W14 on jack J26 provides a $75 \Omega$ input impedance when the jumper is between pins 1 and 2 and a high impedance when it is between pins 2 and 3. Diodes CR17, CR18, CR20 and CR21 protect the input stages of U14A and U14B if an excessive signal level is applied to the board. The outputs of U14A and U14B are applied to differential amplifier U13A, which eliminates common mode signals (hum) on its input leads. The composite input signal is then applied to amplifier U13B; whose gain is controlled by the STEREO, composite audio gain pot R132, accessed through the front panel. The composite audio signal is then connected to the summing point at U13C, pin 9.

### 4.1.1.3 SAP/PRO, Subcarrier Audio Input

The third possible input to the board is the SAP/PRO, SCA audio input at J41A pin $16 A(+)$ and 17A(-). The SCA input has an input matching impedance of $75 \Omega$ that can be eliminated by removing jumper W15 from pins 1 and 2 of J28. The SCA input is bandpass filtered by C73, C74, R145, C78, C79, and R146 and is fed to buffer
amplifier U13D. The amplified signal is then applied though the SAP/PRO, SCA gain pot R150, accessed through the front panel, to the summing point at pin 9 of U13C.

### 4.1.1.4 Audio Modulation of the 4.5 MHz VCO

The Mono balanced audio, or the Stereo composite audio, or the SAP/PRO SCA buffered audio signal, is fed to the common junction of resistors R111, R130, and R152 that connect to pin 9 of amplifier U13C. The output audio signal at pin 8 of U 13 C is typically .8 Vpk -pk at a $\pm 25-\mathrm{kHz}$ deviation for Mono balanced audio or $.8 \mathrm{Vpk}-\mathrm{pk}$ at $\pm 75-\mathrm{kHz}$ deviation for Stereo composite audio as measured at Test Point TP1. This audio deviation signal is applied to the circuits containing the 4.5 MHz aural VCO U16. A sample of the aural deviation level is amplified, detected by U15A and U15B, and connected to J41A pin 5A on the board. This audio-deviation level is connected to the front panel display on the Control/Power Supply Assembly.

The audio from U13C is connected thru C71, a frequency response adjustment, to varactor diodes, CR24 to CR27, that frequency modulates the audio signal onto the generated $4.5-\mathrm{MHz}$ signal by U16. U16 is the $4.5-\mathrm{MHz}$ VCO that generates the $4.5-\mathrm{MHz}$ continuous wave (CW) signal. The output frequency of the 4.5 MHz signal is maintained and controlled by the correction voltage output of the U21 PLL integrated circuit (IC), at " N ", that connects to the varactor diodes. The audio-modulated, $4.5-\mathrm{MHz}$ signal is fed through the emitter follower Q13 to the amplifiers U17A and U17B. The amplified output of U17A is connected to a $4.5-\mathrm{MHz}$ filter and then to U17B. The output of U17B is connected to the $4.5-\mathrm{MHz}$ output sample jack at J29 and through the Jumper W4 on J5 pins 1 \& 2, " J ", to the I input of the mixer Z 1 .

### 4.1.1.5 Phase Lock Loop (PLL) Circuit

A sample of the signal from the $4.5-\mathrm{MHz}$ aural VCO at the output of Q13, " M ", is applied to PLL IC U21 at pin 1 the $\mathrm{F}_{\text {in }}$ connection. In U21, the signal is divided down to 50 kHz and is compared to a 50kHz reference signal. The reference signal is a divided-down sample of the $45.75-\mathrm{MHz}$ visual IF signal that is applied to the oscillator-in connection at Pin 27 on the PLL chip. These two $50-\mathrm{kHz}$ signals are compared in the IC and the fV, and fR is applied to the differential amplifier U18A. The output of $\mathrm{U} 18 \mathrm{~A}, ~ " \mathrm{~N}$ ", is fed back through CR28 and C85 to the $4.5-\mathrm{MHz}$ VCO IC U16; this sets up a PLL circuit. The $4.5-\mathrm{MHz}$ VCO will maintain the extremely accurate $4.5-\mathrm{MHz}$ separation between the visual and aural IF signals; any change in frequency will be corrected by the AFC error voltage.

PLL chip U21 also contains an internal lock detector that indicates the status of the PLL circuit. When U21 is in a "locked" state, pin 28 is high. If the $4.5-\mathrm{MHz}$ VCO and the $45.75-\mathrm{MHz}$ oscillator become "unlocked," out of the capture range of the PLL circuit, pin 28 of U21 will go to a logic low and cause the LED DS5 to light red. The Aural Unlock LED is viewed through the front panel of the Assembly. An Aural unlock, PLL Unlocked, output signal from Q16 is also applied to jack J41B pin 1B.

## Sync tip clamp and the visual and aural modulator portions of the board

The sync tip clamp and modulator portion of the board is made up of four circuits: the main video circuit, the sync tip clamp circuit, the visual modulator circuit and the aural modulator circuit.

The clamp portion of the board maintains a constant peak of sync level over varying average picture levels (APL). The modulator portion of the board contains the circuitry that generates an amplitudemodulated vestigial sideband visual IF signal output that is made up of the baseband video input signal ( 5 to 1 Vpkpk ) modulated onto a $45.75-\mathrm{MHz}$ IF carrier
frequency. The visual IF signal and the aural IF signal are then combined in the diplexer circuit to produce the visual IF + aural IF output, " G ", that is connected to J41C pin 28C the Combined IF output of the board.

### 4.1.1.6 Main Video Signal Path (Part 1 of 2)

The baseband video input connects to the board at J41A pins 19A (-), "W", and 20A (+), "V". The +, "V" and -, "W", video inputs are fed to Diodes CR1 to CR4 that form a voltage-limiter network in which, if the input voltages exceed the supply voltages for U2B, the diodes conduct, preventing damage to U2B. CR1 and CR3 conduct if the input voltage exceeds the negative supply and CR2 and CR4 conduct if the input voltage exceeds the positive supply voltage. The baseband video input connects to the non-inverting and inverting inputs of U2B, a differential amplifier that minimizes any commonmode problems that may be present on the incoming signal

The video output of U2B is connected through the Video Gain pot R42, accessed through the front panel, to the amplifier U2A. The output of U2A connects to the delay equalizer circuits

### 4.1.1.7 Delay Equalizer Circuits

The delay equalizer circuits provide a delay to the video signal, correction to the frequency response, and amplification of the video signal.

The video output of U2A is wired to the first of four delay-equalizing circuits that shape the video signal to the FCC specification for delay equalization or to the shape needed for the system. The board has been factory-adjusted to this FCC specification and should not be readjusted without the proper equipment.

Resistors R53, R63, R61, and R58 adjust the sharpness of the response curve while inductors GD1, GD2, GD3, and GD4
adjust the position of the curve. The group delayed video signal at the output of U3A is split with a sample connected to J 8 on the board that can be used for testing purposes of the Post Video Delay signal. The other portion of the video signal connects through the Jumper W5 on J9 pins 2 and 3 . The video is slit with one part connecting to a sync tip clamp circuit and the other part to the main video output path through R44. A sample of the video at " P " connects to U32 and U33 that provide a zero adjust and a 1 Volt output level, which connects at "T" to J41A pin 3A. This video level is wired to the Control/Power Supply assembly.

### 4.1.1.8 Sync Tip Clamp Circuit

The automatic sync tip clamp circuit is made up of U6A, Q8, U5C, and associated components. The circuit begins with a sample of the clamped video that buffered by U3A, which is split off from the main video path that connects to U6A. The level at which the tip of sync is clamped, to -1.04 VDC as set by the voltage-divider network, R77, R78, R75, R76 and R80 connected to U6A. If the video level changes, the sample applied to U6A changes. The voltage from the clamp circuit that is applied to the summing circuit at the base of Q8 will change; this will bring the sync tip level back to -1.04 VDC. Q8 will be turned off and on according to the peak of sync voltage level that is applied to U6A. The capacitors C35 and C24, in the output circuit of Q8, will charge or discharge to the new voltage level. This will bias U5C more or less, through the front panel MANUAL/AUTO CLAMP switch, SW1, when it is in the Auto Clamp-On position, between pins 2 and 3. In AUTO CLAMP, U5C will increase or decrease its output, as needed, to bring the peak of sync back to the correct level. The voltage level is applied through U5C to U2A. In the Manual CLAMP position, SW1 in manual position, between pins 1 and 2, the adjustable resistor R67 provides the manual clamp bias adjustment for the video that connects to U5C. This level is set at the factory and is not adjustable by the customer. In Manual clamp the peak
of sync auto clamp circuit will not automatically be clamped to the pre set level.

### 4.1.1.9 Main Video Signal Path <br> (Part 2 of 2)

A sample of the clamped video output from the group delay circuitry at the junction of R44, R62 and R300 is connected to a white clipper circuit consisting of Q1 and associated circuitry. The base voltage of Q1 is set by the voltage divider network consisting of R1, R9 and R5. R5 is variable and sets the level of the white clipper circuit to prevent video transients from over modulating the video carrier.

The clamped video output of amplifier U3A is split with one part connected through R35 to J8 that provides a sample of the Post Video Delay Signal.

The other clamped video path from U3A is through jumper W5 on 19 pins $2 \& 3$ through R44 to a sync-stretch circuit that consists of Q3 and Q4. The sync-stretch circuit contains R19, which adjusts the Sync Stretch Magnitude (amount), R11, which adjusts the Sync Stretch Cut-In and R6, which adjusts the Sync Clipping point. This sync-stretch adjustment should not be used to correct for output sync problems, but it can be used for video input sync problems. The output of the sync-stretch circuit is amplified by U31A and connected, " $K$ ", to pin 5 , the I input of Mixer Z2, the Visual IF Mixer.

### 4.1.1 10 45.75 MHz Oven Oscillator Circuit

The oven oscillator portion of the board generates the visual IF CW signal at 45.75 MHz for NTSC system "M" usage.

The +12 VDC needed to operate the oven is applied through jack J30 pin 1 on the crystal oven HR1. The oven is preset to operate at $60^{\circ} \mathrm{C}$. The oven encloses the 45.75 MHz crystal Y 1 and stabilizes the crystal temperature. The crystal is the principal device that determines the
operating frequency and is the most sensitive in terms of temperature stability.

Crystal Y1 operates in an oscillator circuit consisting of transistor Q24 and its associated components. Feedback that is provided by a voltage divider, consisting of C173, L38 and R295, is fed to the base of Q24 through C169. This circuitry operates the crystal in a common-base amplifier configuration using Q24. The operating frequency of the oscillator is maintained by a PLL circuit, which consists of ICs U20 and U22 and associated components, whose PLL output connects to R293 in the crystal circuit.

The oscillator circuit around Q24 has a regulated voltage, +6.8 VDC , which is produced from the +12 VDC by a combination of dropping resistor R261, diodes CR37 and CR38 and Zener diode VR2. The output of the oscillator at the collector of Q24 is capacitively coupled through C165 to the base of Q23. The small value of C165, 15 pF , keeps the oscillator from being loaded down by Q23. Q23 is operated as a common-emitter amplifier stage whose bias is provided through R259 from the +12 VDC line. The output of Q23, at its collector, is connected to an emitter-follower transistor stage, Q21. The output of Q21 at its emitter is split. One path connects to the input of the IC U20 in the PLL circuit. The other path is through R270 to establish an approximate 50 -ohm source impedance through C166 to the Pin 1 contact of the relay K2. The 45.75 MHz connects through the closed contacts Oof K2 to a splitter network consisting of L31 and L32.

NOTE: The relay contacts for the internally generated 45.75 MHz signal will be closed unless an external IF signal, such as the IF for offset and precise frequency 45.74 or 45.76 MHz , connects to the board. The external IF CW Input connects at J41A pin 32A and is connected to J19 and through the external cable assembly W10 back to the board at J20. The external IF CW input is split on the board. One branch connects through C157 to a buffer amplifier Q20 to the K2 relay at pin 14. The other path is
through C152 to the amplifier U23A. The output of U23A is split with one part connecting to Q26 that shuts down the 45.75 MHz oscillator. Another path connects to Q25 the conducts and lights the LED DS7, Alternate IF, viewed on the front panel. The final path connects through R268 to Q22 that is biased on and energizes the relay, K2. The external IF CW Input at contact 14 now connects through the closed contact to the splitter network consisting of L31 and L32.

Either the internal or external CW IF from the K2 relay is split with one path through L31 to the amplifier U28 to the L input of $Z 1$ the Aural IF Mixer. The other path is through L32 to the amplifier U29 to the $L$ input of $Z 2$ the Visual IF Mixer.

### 4.1.1.11 Visual Modulator Circuit

The video signal is heterodyned in mixer Z2 with the visual IF CW signal ( 45.75 MHz ). The visual IF CW signal from L32 of the splitter connects to U29, where it is amplified and wired to pin 1 , the L input of mixer Z2. Adjustable capacitor C168 and resistor R275 are set up to add a small amount of incidental carrier phase modulation (ICPM) correction to the output of the mixer stage to compensate for any non-linearities generated by the mixer.

The modulated $45.75-\mathrm{MHz}$ RF output of mixer $Z 2$, at pin 4 the $R$ output, is amplified by U30 and is fed to J17 through W8, the external cable assembly, "WB", to J13 on the board. J17 is the visual IF loop-through output jack that is normally jumpered to J13 on the board. The modulated visual IF through J13 connects to J41C pin 17C the Visual IF Output of the board.

### 4.1.1.12 Aural Modulator Circuit

The 4.5 MHz aural modulated signal is heterodyned in mixer Z 1 with the 45.75 MHz IF CW signal. The mixer Z1 heterodynes the aural-modulated, 4.5MHz signal with the $45.75-\mathrm{MHz}$ CW signal
to produce the modulated $41.25-\mathrm{MHz}$ aural IF signal. The audio modulated 4.5 MHz from 4.5 MHz VCO IC U16 connects, " J ", to the I input at pin 5 of Z 1 . The visual IF CW signal from L31 of the splitter connects to U28, where it is amplified and wired to pin 1 , the $L$ input of mixer $Z 1$. The $R$ output of the mixer at pin 4 is fed to a bandpass filter, consisting of L18-L21, L25-L28 and C136, C137 and C142-144, that is tuned to pass only the modulated $41.25-\mathrm{MHz}$ aural IF signal. The filtered 41.25 MHz is fed to the amplifier U27. The amplified 41.25MHz signal is connected by a coaxial cable, W9, from J21, "WC", to J18 on the board. The modulated $41.25-\mathrm{MHz}$ aural IF signal from $J 18$ is connected to 341 C pin 6 C the Aural IF Output of the board.

### 4.1.1.13 Combining the 45.75 MHz Visual IF and 41.25 MHz Aural IF Signals

The Visual IF connects back to the board at J41C pin 3C, through a Visual IF jumper cable connected to the rear chassis of the exciter/driver. IF processing equipment can be connected in place of the jumper if needed. The visual IF is connected to J12, through jumper W7, "WA", to J14. The visual IF is amplified by U24 and filtered by FL1 with T1 and T2 providing isolation. The filtered IF is amplified by U25 and adjusted in level by R214 before it is connected to a summing circuit at the common connection of L16 and L17.

The Aural IF connects back to the board at J41C pin 23C, through an Aural IF jumper cable connected to the rear chassis of the exciter/driver. IF processing equipment can be connected in place of the jumper if needed. The aural IF, " $F$ ", is connected through C132, R234, R235 and adjusted in level by R243 before it is connected to a summing circuit at the common connection of L17 and L16.

The Aural IF and Visual IF signals are combined through L16 and L17. The frequency response of the combined 41.25 $\mathrm{MHz}+45.75 \mathrm{MHz}$ signal is set by R238 and R239 and associated components. The corrected combined IF signal is amplified by U25 and connected to a splitter
matching network consisting of T3 and T4. One part of signal connects to J10, the $41.25 \mathrm{MHz}+45.75 \mathrm{MHz}$ sample output jack, located on the front panel. The other part, " ${ }^{\prime}$ ", connects to J41C pin 28C the Combined IF Output of the board.

### 4.1.1.14 Voltage Requirements

The $\pm 12$ VDC needed for the operation of the board enters through jack J41A pins 25A (+12 VDC) and 26A (-12 VDC). The +12 VDC is filtered by L6, L7, and C27 before it is connected to the rest of the board. The +12 VDC also connects to U7, a 5 -volt regulator IC, that provides +5 VDC to the rest of the board.

The -12 VDC is filtered by L5, C16, and C17 before it is connected to the rest of the board.

## 4.2 (A3) IF Processor Module Assembly (1301938; Appendix B)

The IF from the 8 VSB modulator enters the module and the signal is precorrected as needed for amplitude linearity correction, Incidental Carrier Phase Modulation (ICPM) correction and frequency response correction.

The Module contains the following board.

### 4.2.1 IF Processor Board (1301977; Appendix B)

The automatic level control (ALC) portion of the board provides the ALC and amplitude linearity correction of the IF signal. The ALC adjusts the level of the IF signal that controls the output power of the transmitter.

The IF from the 8 VSB modulator enters the board at J1B pin 32B. If the (optional) receiver tray is present, the IF input ( -6 dBm ) from the 8 VSB modulator tray connects to the modulated IF input jack J1C Pin 21C. The modulated IF input connects to relay K3 and the receiver IF input connects to
relay K4. The two relays are controlled by the Modulator Select command that is connected to J1C Pin 14C on the board. Modulator select enable/disable jumper W11 on J29 controls whether the Modulator Select command at J1C Pin 14C controls the operation of the relays. With jumper W11 on J29 between pins 1 and 2, the Modulator Select command at J1C Pin 14C controls the operation of the relays; with jumper W11 on J29, pins 2 and 3, the modulator is selected all of the time.

### 4.2.1.1 Modulator Selected

With the modulator selected, J1C-14C low, this shuts off Q12 and causes Pin 8 on the relays to go high that causes relays K3 and K4 to de-energize. When K4 is deenergized, it connects the receiver IF input at J1C-21C, if present, to a $50 \Omega$ load. When K3 is de-energized, it connects the modulator IF input at J1B-32B to the rest of the board; Modulator Enable LED DS5 will be illuminated.

### 4.2.1.2 External Modulated IF Selected

With the External Modulated IF selected, J1C-14C high, this turns on Q12 and makes pin 8 on the relays low that causes the relays K3 and K4 to energized. When K 4 is energized, it connects the receiver IF input at J at J1C-21C, if present, to the rest of the board. When K3 is energized, it connects to the modulator IF input at J1B32B to a $50 \Omega$ load. The Modulator Enable LED DS5 will not be illuminated.

### 4.2.1.3 Main IF Signal Path (Part 1 of 3)

The selected IF input ( -6 dBm average) signal is split, with one half of the signal entering a bandpass filter that consists of L3, L4, C4, L5, and L6. This bandpass filter can be tuned with C4 and is substantially broader than the IF signal bandwidth. It is used to slightly steer the frequency response of the IF to make up for any small discrepancies in the frequency response in the stages that precede this point. The filter also serves the additional function of rejecting unwanted frequencies that may occur if the tray cover is off and
the tray is in a high RF environment. (If this is the case, the transmitter will have to be serviced with the tray cover off in spite of the presence of other RF signals). The filtered IF signal is fed through a pitype matching pad consisting of R2, R3, and R4 to the pin-diode attenuator circuit consisting of CR1, CR2, and CR3.

### 4.2.1.4 Input Level Detector Circuit

The other part of the split IF input is connected through L2 and C44 to U7. U7 is an IC amplifier that is the input to the input level detector circuit. The amplified IF is fed to T4, which is a step-up transformer that feeds diode detector CR14. The positive-going detected signal is then low-pass filtered by C49, L18, and C50. This allows only the positive digital peaks to be applied through emitter follower Q1. The signal is then connected to detector CR15 to produce a peak digital voltage that is applied to op-amp U9A. There is a test point at TP3 that provides a voltage-reference check of the input level. The detector serves the dual function of providing a reference that determines the input IF signal level to the board and also serves as an input threshold detector.

The input threshold detector prevents the automatic level control from reducing the attenuation of the pin-diode attenuator to minimum, the maximum signal output, if the IF input to the board is removed. The ALC, input loss cutback, and the threshold detector circuits will only operate when jumper W2 on jack J5 is in the Enabled position, between pins 2 and 3. Without the threshold detector, and with the pin-diode attenuator at minimum, the signal will overdrive the stages following this board when the input is restored.

As part of the threshold detector operation, the minimum IF input level at TP3 is fed through detector CR15 to opamp IC U9A, pin 2 . The reference voltage for the op-amp is determined by the voltage divider that consists of R50 and R51, off the +12 VDC line. When the
detected input signal level at U9A, pin 2, falls below this reference threshold, approximately 10 dB below the normal input level, the output of U9A at pin 1 goes high, toward the +12 VDC rail. This high is connected to the base of Q2 that is forward biased and creates a current path. This path runs from the -12 VDC line and through red LED DS1, the input level fault indicator, which lights, resistor R54, and transistor Q2 to +12 VDC. The high from U9A also connects through diode CR16 and R52, to U24D pin 12, whose output at pin 14 goes high. The high connects through the front panel accessible ALC Gain pot R284 and the full power set pot R252 to U24C Pin 9. This high causes U24C pin 8 to go low. A power raise/lower input from the Control/Monitoring Module connects to J42C pin 24C and is wired to Q14. This input will increase or decrease the value of the low applied to U24B and therefore increase or decrease the power output of the transmitter.

The low connects to U24B pin 5 whose output goes low. The low is wired to U24A pin2 whose output goes high. The high is applied to U10A, pin 2, whose output goes low. The low connects through the switch SW1, if it is in the auto gain position, to the pin-diode attenuator circuit, CR1, CR2 \& CR3. The low reverse biases them and cuts back the IF level, therefore the output level, to 0 . When the input signal level increases above the threshold level, the output power will increase, as the input level increases, until normal output power is reached.

The digital input level at TP3 is also fed to a pulse detector circuit, consisting of IC U8, CR17, Q3, and associated components, and then to a comparator circuit made up of U9C and U9D. The reference voltage for the comparators is determined by a voltage divider consisting of R243, R65, R66, and R130, off the -12 VDC line. When the input signal level to the detector at TP3 falls below this reference threshold, which acts as a loss-of-digital peak detector circuit, the output of U9C and U9D goes towards the -12 VDC rail and is split, with one part biasing on transistor Q5. A current
path is then established from the +12 VDC line through Q5, the resistors R69 and R137, and the red LED DS3, input loss indicator, which is illuminated. When Q5 is on, it applies a high to the gate of Q6. This causes it to conduct and apply a modulation loss pull-down output to J42C, pin 7C, which is applied to the front panel display on the Control/Monitor module.

The other low output of U9C and U9D is connected through CR18, CR19 \& CR20 to jack J5. Jumper W2 on J5, in the Cutback Enable position, which is between pins 2 and 3, connects the low to the base of Q4 that is now forwardbiased. NOTE: If jumper W2 is in the Disable position, between pins 1 and 2, the auto cutback will not operate. With Q4 biased on, a negative level determined by the setting of cutback level pot R71 is applied to U24D, pin 12. The level is set at the factory to cut back the output to approximately $25 \%$. The output of U24D at pin 14 goes low and is applied through the power adjust pot to U24C, pin 9, whose output goes low.

The low connects to U24B, pin 5, whose output goes low. The low then connects to U24A, pin 2, whose output goes high. The high is applied to U10A, pin 2, whose output goes low. The low connects through the switch SW1, if it is in the auto gain position, to the to the pin-diode attenuator circuit, CR1, CR2 \& CR3. The low reverse biases them and cuts back the level of the output to approximately 25\%.

### 4.2.1.5 Pin-Diode Attenuator Circuit

The input IF signal is fed to a pin-diode attenuator circuit that consists of CR1, CR2 \& CR3. Each of the pin diodes contains a wide intrinsic region; this makes the diodes function as voltagevariable resistors at this intermediate frequency. The value of the resistance is controlled by the DC bias supplied to the diode. The pin diodes are configured in a pi-type attenuator configuration where CR1 is the first shunt element, CR3 is the
series element, and CR2 is the second shunt element. The control voltage, which can be measured at TP1, originates either from the ALC circuit when the switch SW1 is in the ALC Auto position, between pins 2 and 3, or from pot R87 when SW1 is in the Manual Gain position, between pins 1 and 2.

In the pin diode attenuator circuit, changing the amount of current through the diodes by forward biasing them changes the IF output level of the board. There are two extremes of attenuation ranges for the pin-diode attenuators. In the minimum attenuation case, the voltage, measured at TP1, approaches the +12 VDC line. There is a current path created through R6, through series diode CR3, and finally through R9 to ground. This path forward biases CR3 and causes it to act as a relatively low-value resistor. In addition, the larger current flow increases the voltage drop across R9 that tends to turn off diodes CR1 and CR2 and causes them to act as high-value resistors. In this case, the shunt elements act as a high resistance and the series element acts as a low resistance to represent the minimum loss condition of the attenuator (maximum signal output). The other extreme case occurs as the voltage at TP1 is reduced and goes towards ground or even slightly negative. This tends to turn off (reverse bias) diode CR3, the series element, causing it to act as a high-value resistor. An existing fixed current path from the +12 VDC line, and through R5, CR1, CR2, and R9, biases series element CR3 off and shunt elements, diodes CR1 and CR2, on, causing them to act as relatively low-value resistors. This represents the maximum attenuation case of the pin attenuator (minimum signal output). By controlling the value of the voltage applied to the pin diodes, the IF signal level is maintained at the set level.

### 4.2.1.6 Main IF Signal Path (Part 2 of 3)

When the IF signal passes out of the pindiode attenuator through C11, it is applied to modular amplifier U1. This device contains the biasing and impedance-
matching circuits that makes it operate as a wide-band IF amplifier. The output of U1 connects to J40 that is jumpered to J41. The J 40 jack is available, as a sample of the pre-correction IF for troubleshooting purposes and system setup. The IF signal is connector to a splitter Z1 that has an in phase output and a $90^{\circ}$ Quadrature output, which are then connected to the linearity corrector portion of the board.

### 4.2.1.7 Amplitude and Phase <br> Pre-Correction Circuits

The linearity corrector circuits use three stages of correction, two adjust for any amplitude non-linearities and one for phase non-linearities of the output signal. Two of the stages are in the in phase amplitude pre-correction path and one stage is in the quadrature phase precorrection path. Each stage has a variable threshold control adjustment, R211 and R216, in the in phase path, and R231, in the quadrature path, that determines the point at which the gain is changed for that stage.

Two reference voltages are needed for the operation of the corrector circuits. The Zener diode VR3, through R261, provides the +6.8 VDC reference. The VREF is produced using the path through R265 and the diodes CR30 and CR31. They provide a .9 VDC reference, which temperature compensates for the two diodes in each corrector stage.

The first corrector stage in the in phase path operates as follows. The in phase IF signal is applied to transformer T6, which doubles the voltage swing by means of a 1:4 impedance transformation. Resistors R222 and R225 form an L-pad that lowers the level of the signal. The input signal level when it reaches a certain level causes the diodes CR24 and CR25 to turn on, generating current flow that puts them in parallel with the L-pad. When the diodes are put in parallel with the resistors, the attenuation through the L-pad is lowered, causing signal stretch.

The signal is next applied to amplifier U17 to compensate for the loss through the L-pad. The breakpoint, or cut-in point, for the first corrector is set by controlling where CR24 and CR25 turn on. This is accomplished by adjusting the threshold cut-in resistor R211. R211 forms a voltage-divider network from +6.8 VDC to ground. The voltage at the wiper arm of R211 is buffered by the unity-gain amplifier U16B. This reference voltage is then applied to R215, R216, and C134 through L44 to the CR24 diode. C134 keeps the reference from sagging during the vertical interval. The . 9 VDC reference voltage is applied to the unity-gain amplifier U16D. The reference voltage is then connected to diode CR25 through choke L45. The two chokes L44 and L45 form a high impedance for RF that serves to isolate the op-amp ICs from the IF.

After the signal is amplified by U17, it is applied to the second corrector stage in the in phase path through T7. These two correctors and the third corrector stage in the quadrature path operate in the same fashion as the first. All three corrector stages are independent and do not interact with each other.

The correctors can be disabled by moving jumper W12 on J30 to the Disable position, between pins 1 and 2, this moves all of the breakpoints past the greatest peaks of digital so that they will have no affect.

The pre-distorted IF signal in the in phase path, connects to an op amp U18 whose output level is controlled by R238. R238 provides a means of balancing the level of the amplitude pre-distorted IF signal that then connects to the combiner $Z 2$.

The pre-distorted IF signal in the quadrature path connects to op amp U20 and then step up transformer T9, next op amp U21 and step up transformer T10 and finally op amp U22 whose output level is controlled by R258. R258 provides a means of balancing the level of the Phase pre-distorted IF signal that then connects to the combiner $\mathrm{Z2}$.

The amplitude and phase pre-distorted IF signals are combined by Z2 and connected to J37 that is jumpered to J36 on the board. J37 can be used for testing or monitoring purposes of the IF signal after amplitude and phase predistortion. The pre-distorted IF signal connects through a resistor buffer network that prevents loading of the combiner before it is wired to the frequency response circuitry.

### 4.2.1.8 Main IF Signal Path (Part 3 of 3)

The IF signal, at the input to the frequency-response corrector circuit, is split using L24, L25 and R89. One path is through L24, which is the main IF path through the board. The main IF is fed through a resistor network that controls the level of the IF by adjusting the resistance of R99, the output level adjust. The IF signal is then applied to a three-stage, frequency-response corrector circuit that is adjusted as needed.

The frequency-response corrector circuit operates as follows. Variable resistors R103, R106 and R274 are used to adjust the depth and gain of the notches and variable caps C71, C72 and C171 are used to adjust the frequency position of the notches. These are adjusted as needed to compensate for frequency response problems.

The frequency-response corrected IF is connected to J38 that is jumpered to J39 on the board. J38 can be used for testing or monitoring purposes of the IF signal after frequency response precorrection.

The IF is next amplified by U13 and U14. After amplification, the IF is split with one path connected to J42C pin 1C the IF output to the LO/Upconverter Module. The other path is fed through a divider network to J35 a SMA IF Sample Jack, located on the front panel, which provides a sample of the corrected IF for test purposes.

### 4.2.1.9 ALC Circuit

The other path of the corrected IF signal at the input to the frequency response corrector circuit is used in the ALC circuit. The IF flows through L25, of the L24 L25 splitter, and connects to the op-amp U12. The IF signal is applied through a resistor divider network to transformer T5. T5 doubles the voltage swing by means of a 1:4 impedance transformation before it is connected to the ALC detector circuit, consisting of C70, CR23 and R91. The detected ALC level output is amplified by U10B and wired to U10A, pin 2, where it is summed with the power control setting, which is the output power setting that is maintained by the ALC. The output of U10A connects through SW1, if it is in the auto gain position, to the pin-diode attenuator circuit, CR1, CR2 \& CR3. The high forward biases them more or less, that increases or decreases the IF level, therefore the output level, opposite the input level. When the input signal level increases, the forward bias on the pin attenuator decreases, therefore the output power will decrease, which keeps the output power the same as set by the customer.

An external power raise/lower switch can be used by connecting it to TB30, at TB308 power raise and TB30-9 power lower, on the rear of the exciter/amplifier chassis. The ALC voltage is set for .8 VDC at TP4 with a $0-\mathrm{dBm}$ output at J42C pin 1C of the module. A sample of the ALC at J42C pin 11 C , is wired to the Control Monitoring/Power Supply module where it is used on the front panel display and in the AGC circuits.

The ALC voltage, and the DC level corresponding to the IF level after signal correction, are fed to U10A, pin 2, whose output at pin 1 connects to the ALC pindiode attenuator circuit. If there is a loss of gain somewhere in an IF circuit, the output power of the transmitter will drop. The ALC circuit senses this drop at U10A and automatically decreases the loss through the pin-diode attenuator circuit therefore
increasing its gain maintaining the same output power level.

The ALC action starts with the ALC detector level monitored at TP4. The detector output at TP4 is nominally +.8 VDC and is applied through resistor R77 to a summing point at op-amp U10A, pin 2. The current available from the ALC detector is offset, or complemented, by current taken away from the summing junction. In normal operation, U10A, pin 2 , is at 0 VDC when the loop is satisfied. If the recovered or peak-detected IF signal level at IF input to this board should drop, which normally means that the output power will decrease, the null condition would no longer occur at U10A, pin 2. When the level drops, the output of U10A, pin 1 , will go more positive. If SW1 is in the Automatic position, it will cause the ALC pin-diode attenuators CR1, CR2, and CR3 to have less attenuation and increase the IF level; this will compensate for the decrease in the level. If the ALC cannot increase the input level enough to satisfy the ALC loop, due to there not being enough range, an ALC fault will occur. The fault is generated because U10D, pin 12, increases above the trip point set by R84 and R83 until it conducts. This makes U10D, pin 14, high and causes the red ALC Fault LED DS2 to light.

### 4.2.1.10 Fault Command

The board also has circuitry for an external mute fault input at J 42 pin 10 C . This is a Mute command that protects the circuits of high-gain output amplifier devices against VSWR faults. This action needs to occur faster than just pulling the ALC reference down. Two different mechanisms are employed: one is a very fast-acting circuit to increase the attenuation of the pin-diode attenuator, CR1, CR2, and CR3, and the second is the reference voltage being pulled away from the ALC amplifier device. An external Mute is a pull-down applied to J42 pin 10C, which completes a current path from the +12 VDC line through R78 and R139, the LED DS4 (Mute indicator),
and the LED section of opto-isolator U11. These actions turn on the transistor section of U11 that applies -12 VDC through CR21 to U10A pin 3, and pulls down the reference voltage. This is a fairly slow action controlled by the low-pass filter function of R81 and C61. When the transistor section of U11 is on, -12 VDC is also connected through CR22 directly to the pin-diode attenuator circuit. This establishes a very fast muting action, by reverse biasing CR3. This action occurs in the event of an external VSWR fault.

### 4.2.1.11 $\pm 12$ VDC Needed to Operate the Board

The $\pm 12$ VDC connects to the board at J42C. The +12 VDC connects to J42C pin 16C and is filtered by L30, L41, and C80 before it is applied to the rest of the board. The -12 VDC connects to J42C pin 18C and is filtered by L31 and C81 before it is applied to the rest of the board.

The +12 VDC also connects through R261 to the zener diode VR3 that connects to ground, which generates the +6.8 VDC output to the rest of the board.

The +12 VDC also connects through R265 to the diodes CR30 and CR31 provide a . 9 VDC reference output voltage VREF that temperature compensates for the two diodes in each corrector stage.

## 4.3 (A5) LO/ Upconverter Module (1301930; Appendix B)

This module contains the LO/Upconverter board, the UHF Generator Board, LED Display Board and channel filters. This module takes an external IF and converts it to the final RF output frequency using an internally generated local oscillator.

The local oscillator consists of a VCXO that is phase locked to an external 10 MHz reference. The 10 MHz reference and the VCO are both divided down to 5 kHz and compared by the phase lock loop circuit. Any error from this comparison is generated in the form of an error current
that is converted to a bias voltage that connects to the VCO. This voltage adjusts the output frequency of the VCO until it is on the desired frequency.

The Phase lock loop is programmed by loading in data generated by the control module. This data sets the dividers so that the 10 MHz and the VCXO frequency are divided to 5 kHz . These divide numbers are loaded into U6 using the clock, data and LE lines. This data is sent whenever the module is first plugged into the backplane board or when power is applied to the transmitter. This is necessary because the divide numbers are lost when power is removed from the module.

There is an alarm generated if the phase locked loop is unlocked. This alarm is displayed locally and is also sent to the control module in the transmitter to be displayed as a fault. The bias voltage to the VCO is also available to be monitored at TP1 and also can be viewed on the front panel display of the Transmitter. Typical values for this voltage are 0.1 to 0.5 V . The 10 MHz reference is normally an external reference. There is also a high stability internal reference option that is available if there is a desire to operate the transmitter without an external reference. Jumper W1 determines whether an external or internal high stability reference is to be used.

The IF signal is applied at a level of -15 dBm average and is converted to the final RF channel frequency. The RF signal is applied to a filter that selects the right conversion product. Next, the signal is amplified to -7 dBm by A3 and exits the front of the module at J2.
There are also a front panel samples of the RF output at J3 and the LO at J1. The RF sample level is approximately 20 dB below the RF output. The LO sample level is -7 dBm .

### 4.3.1 (A4) UHF Generator Board (1585-1265; Appendix B)

The UHF generator board is mounted in the UHF Generator Enclosure for EMI and RFI protection. The board contains a VCXO circuit and additional circuitry to multiply the VCXO frequency by eight.

The VCXO circuit uses the crystal Y1, mounted in a crystal oven for stability, to produce an output of $\approx 67 \mathrm{MHz}$ to 132 MHz , depending on the desired channel frequency. Course adjustment to the frequency of the crystal is made by C11, while fine adjustments are accomplished by the AFC voltage at J2 from (A1) the LO/Upconverter board (1302132). The VCXO output level is adjusted by C6, L2, L4 and C18. The output is split and provides an input to the $x 8$ multiplier circuitry as well as a VHF Output sample at J1.

The $x 8$ circuitry consists of three identical $x 2$ broadband frequency doublers. The input signal at the fundamental frequency is fed through a $6-\mathrm{dB}$ pad consisting of R21, R24, and R25 through C29 to amplifier U3. The output of the amplifier stage is directed through a bandpass filter consisting of L8 and C32, which is tuned to the fundamental frequency ( 67 MHz to 132 MHz ). The voltage measured at TP1 is typically +. 6 VDC. The first doubler stage consists of Z1 with bandpass filter L9 and C34 tuned to the second harmonic (134 MHz to 264 MHz ). The harmonic is amplified by U4 and again bandpass filtered at the second harmonic by C38 and L11 ( 134 MHz to 264 MHz ). The voltage measured at TP2 is typically +1.2 VDC. The next doubler stage consists of $Z 2$ with bandpass filter C40 and L12 tuned to the fourth harmonic of the fundamental frequency ( 268 MHz to 528 MHz ). The fourth harmonic is then amplified by U5 and fed through another bandpass filter tuned to the fourth harmonic consisting of L14 and C44 ( 268 MHz to 528 MHz ). The voltage measured at TP3 is typically +2.0 VDC. The final doubler stage consists of Z3 with bandpass filter C46 and L15 tuned to the eighth harmonic of the fundamental frequency ( 536 MHz to 1056 MHz ). The signal is amplified by $U 6$ and $U 7$ to a typical value of from +2 to +4 VDC as measured at TP4. The amplified eighth harmonic is
then fed to the SMA RF output jack of the board at J3. Typical output level of the signal is +16 dBm nominal. This output connects through A5 a channel filter to the LO/Upconverter Board.

The DC voltages needed to operate the UHF generator board are supplied by the LO/Upconverter Board. The +12 VDC for the board enters through jack J4-3 and is filtered by L22 and C54-C58 before being distributed to the circuits on the board.

The +9 VDC for the board enters through jack J4-1 and is distributed to the rest of the board.

### 4.3.2 (A2 and A5) UHF Filters (1007-1101; Appendix B)

Both UHF filters are tunable two-section cavity filters that are typically tuned for a bandwidth of 6 MHz and have a loss of -1 dB through the filter.

### 4.3.3 (A1) LO/ Upconverter Board (1302132; Appendix B)

The upconverter portion of the board
The LO/Upconverter board provides upconversion processing by mixing the IF and LO signals in mixer Z1 to produce the desired RF frequency output. The RF output is connected through J4 to A5, an external channel filter, and applied back to the board at J6. The RF is amplified and connected to the RF output jack of the board at J43-25B.

The IF signal ( -6 dBm average) enters the board at J43-2B and is applied through a matching pad and filter circuit to the mixer. The pad consists of R6, R2 and R7, which presents a relatively good source impedance. The IF is then connected through a voltage divider network consisting of R3, R4, R8 and R14. R14 is variable and adjusted to set the 0 dBm IF input level to the mixer. The IF in next filtered by L3, C84 and C83 and connected to pin 5, the I input of the mixer Z 1 .

The local oscillator signal ( +13 dBm ) from UHF Generator Board, through (A5) a UHF channel filter, connects to the board at jack J1, an SMA connector. THE LO is connected directly to pin 1 , the $L$ input of the mixer Z .

The frequency of the LO is the sum of the IF frequency above the required digital carrier. For instance, in system M, for digital applications, the LO is the center frequency of the digital channel added to the $44-\mathrm{MHz}$ IF frequency. By picking the local oscillator to be 44 MHz above the digital carrier, a conversion in frequency occurs by selecting the difference product. The difference product, the local oscillator minus the IF, will be at the desired digital carrier frequency output. There will also be other signals present at the RF output connector J3 at a lower level. These are the sum conversion product: the LO and the IF frequencies. Usually, the output product that is selected by the tuning of the external filter is the difference product: the LO minus the $44-\mathrm{MHz}$ IF.

If a bad reactive load is connected to the mixer, the LO signal that is fed through it can be increased because the mixer no longer serves as a double-balanced mixer. The mixer has the inherent property of suppressing signals that may leak from one input port to any of the other ports. This property is enhanced by having inputs and outputs of the mixer at $50 \Omega$ impedance. The RF output of the mixer connects through a pad made up of R12, R15, and R17 before it is wired to the amplifier U2. The RF signal is amplified by U2, a modular amplifier, and includes within it biasing and impedance matching networks that makes U2 act as a wideband-RF amplifier device. This amplifier, in a $50 \Omega$ system, has approximately 12 dB of gain. U 2 is powered from the +12 VDC line through RF decoupling components R24, C14, and L4. Inductor L4 is a broadband-RF choke and is resonance free through the UHF band. The amplified RF connects through a pad to the SMA RF output jack J4 and is cabled to (A2) an external channel filter. The reactive channel filter that is externally connected to J 4 of the board does not
appear as a good $50-\Omega$ load at all frequencies. The pad, in the output line of the board, consisting of R20, R18, and R21 buffers the bad effects of the reactive filter load and makes it appear as a $50 \Omega$ impedance.

The RF input signal from the external filter re-enters the board at J6 (-11 to 17 dBm ) and is capacitively coupled to the pin-diode attenuator circuit consisting of CR2, CR3, and CR4. The pin-diode attenuator acts as a voltage-variable attenuator in which each pin diode functions as a voltage-variable resistor that is controlled by the DC bias connected to the diodes. The pin diodes, because of a large, intrinsic region, cannot rectify signals at this RF frequency; therefore, they only act as a linear voltage-variable resistor. These diodes are part of the AGC for the transmitter.

The automatic gain control (AGC) portion of the board

The automatic gain control (AGC) provides automatic gain control for the power amplifier module(s).

The AGC circuitry attempts to maintain the ratio between an input reference proportional to the input power and the output power of either the exciter/amplifier PA output, AGC \#1, Inner Loop, or the output of external power amplifiers, AGC \#2, Outer Loop, farther downstream. NOTE: The AGC \#2 Outer Loop is not used in 5W-50W digital transmitters.

An ALC reference input is applied to the board at J43-16A, amplified by U10A, and sent to the front panel board through J5-7 where it is connected to a AGC Manual Gain pot, accessed through the front panel. A switch AUTO/MAN AGC is also located on the front panel. When switched in MAN the MAN GAIN Pot adjusts the output power level. The Gain Control voltage is reapplied to the board at J5-6. The gain control voltage is summed to the added together inner
and outer loop AGC reference voltage at U10D.

The AGC output reference from the exciter/amplifier PA module, AGC \#1 INNER LOOP, is applied at J43-14C and from the external PA module, AGC \#2 OUTER LOOP, is applied at J43-15C.

The larger voltage of either the inner or the outer loop is used to control the AGC loop. Since the outer loop is not used in this system, the inner loop controls the AGC. R82 is adjusted so that the inner loop voltage at TP7 is larger than the voltage at TP4 by approximately .1 VDC. This ensures that the output of the exciter/amplifier is the reference used for AGC. In systems that use the outer loop, that level is adjusted to . 1 VDC above the inner loops reference. This ensures that the output of the system is the reference used for AGC. If that reference drops to the point where it is smaller than the inner loop reference, the system switches over to using the inner loop reference.

The AGC reference that is being used is buffered by U10C and connected to U10D. U10D generates an output voltage that is used to bias the pin attenuators, CR2, CR3 and CR4, which sets the gain of the exciter/amplifier.

This Auto AGC circuit can be disabled by the AGC Auto/Man switch, located on the front panel, which switches the pinattenuator bias to a variable voltage that is set by the Manual Gain Adjust.

The level-controlled RF signal, from the pin-diode attenuator circuit, is amplified by the wideband-hybrid amplifier IC U13 that is configured in the same way as U2. The RF signal is converted by T 1 to a balanced, dual feed output that is applied to the push-pull Class A amplifier IC U1. Capacitors C2 and C5 provide DC blocking for the input signal to the IC. The RF outputs of the IC are applied through C3 and C4, which provide DC blocking for the output signals. The RF signals connect to combiner T2 that combines the RF back to a single-RF output at a $50 \Omega$ impedance.

The RF then enters a coupler stage, which provides a sample of the RF at J7 (-20dB), the front panel RF sample jack. The main path through coupler is to J 43 pin 25B, the Upconverter RF output jack of the module ( +0 to +10 dBm ).

The PLL and $10-\mathrm{MHz}$ Reference section of the Board

The PLL and $10-\mathrm{MHz}$ reference portion of the board utilizes either an external 10 MHz reference or an internally generated 10 MHz as the reference for the PLL circuit that generates the AFC voltage, which controls the frequency of the VCXO on the UHF Generator Board.

The (PLL) phase lock loop circuit, provides the automatic frequency control (AFC) voltage, that connects to the VCXO, located on the UHF generator board, and maintains the accurate output frequency of the VCXO. The AFC is generated by comparing a sample of the $10-\mathrm{MHz}$ reference to a sample of the VCXO frequency. The PLL uses an external $10-\mathrm{MHz}$ signal as the reference, unless it is missing, then an internally generated $10-\mathrm{MHz}$ signal is used. The two $10-\mathrm{MHz}$ reference signals are connected to the K1 relay and the selected reference connects to the comparator synthesizer IC U9. The switching between the two references is accomplished by the K1 relay. When the relay is de-energized, it applies the external $10-\mathrm{MHz}$ reference to U 9 . The relay will remain de-energized as long as an externally generated $10-\mathrm{MHz}$ reference signal is present and the Jumper W3 on J10 is placed in the external position, between Pins 1 \& 2 . An alternate 10 MHz reference can be connected to J11 on the board. The jumper W3 on J10 must then be moved to pins 2 \& 3, internal, to connect the alternate 10 MHz to K1. The alternate 10 MHz will then act in the circuit like the external 10 MHz .

If the external $10-\mathrm{MHz}$ reference is lost, the relay will energized and the internally generated $10-\mathrm{MHz}$ reference is then
applied through the K1 relay pin 14 to pin 1 to the IC U9.

With the relay de-energized, the externally generated $10-\mathrm{MHz}$ from jack J 43 pin 22B connects through the normally closed contacts of the relay from pin 1 to pin 7 to the IC U9.

## External 10-MHz Reference Present Circuitry

The external $10-\mathrm{MHz}$ reference signal enters the board at J43 pin 22B and is isolated by L8 and connected to the External/Internal Jack J10. W3 on J10 is a manual jumper that must be connected between pins $1 \& 2$, External, for the external 10 MHz to connect to the rest of the circuit. The external 10 MHz is filtered by C44, R55, L9 and C46 before it split with one path connected to the K1 relay at pin 1 of the normally closed contacts. The other path takes the 10 MHz and rectifies it by CR5 and filters it before it is connected to U7A pin 2. If the sample level of the external 10 MHz is above the reference set by R46 and R48, which is connected to pin 3 of U7A, the output of U7A stays low. The low connects to the gates of Q3, Q5 and Q6, which are biased off and cause their drains to go high. The high from the drain of Q6 is wired to J43, pin 14A, for connection to a remote external $10-\mathrm{MHz}$ present indicator. The high from the drain of Q5 connects to the yellow LED DS2, internal reference indictor, which will not light. This indicates that an external 10MHz reference is present. The low from U7A also connects to the gate of Q3, biasing it off and causing its drain to go high. This high de-energizes the K1 relay and applies the external $10-\mathrm{MHz}$ reference signal to pin 6 on U9 for use as the reference in the PLL circuits.

## Internal 10-MHz Reference Circuitry

The internally generated $10-\mathrm{MHz}$ reference signal connects from U6, the $10-\mathrm{MHz}$ oscillator IC, to pin 14, the Normally Open contacts of relay K1.

With no external $10-\mathrm{MHz}$ reference input, the level connected to U7A Pin 2 will be low. This will be less than the reference set by R46 and R48, which is connected to pin 3 of U7A, that causes the output of U7A to go high. The high connects to the gates of Q3, Q5 and Q6, which are biased on and causes their drains to go low. The low from the drain of Q6 is wired to J43, pin 14A, for connection to a remote external $10-\mathrm{MHz}$ present indicator. The low from the drain of Q5 connects to the yellow LED DS2, internal reference indictor, which will light. This indicates that an external $10-\mathrm{MHz}$ reference is not present and that the internal $10-\mathrm{MHz}$ is being used as the reference. The high from U7A also connects to the gate of Q3, biasing it on and causing its drain to go low. This low energizes the K1 relay and applies the internal $10-\mathrm{MHz}$ reference signal through K1 pin 14 to pin 7 to pin 6 on U9 for use as the reference in the PLL circuits.

Selected $10-\mathrm{MHz}$ Reference Samples
A sample of the selected $10-\mathrm{MHz}$ is split off the main path through L13 and R95 using L14 and C74 and C73. The sample path connects to another splitter circuit consisting of L2, R94, L11, C71 and C70. One output of the splitter connects to J43 pin 28B that is used by the external digital modulator tray. The other output of the splitter connects to 343 pin 31B that is used by the external analog modulator tray.

## Comparator Phase Lock Loop Circuit

The selected $10-\mathrm{MHz}$ reference connects to pin 6, Oscillator In, of the IC U9. The LO generated by the VCXO located on the UHF Generator Board connects to J1 on the LO/Upconverter Board. A sample of the LO is divided off the main line by R105, R106 and R107. The LO sample connects to pin 4, F In, of U9.

The U9 IC takes the 10 MHz reference and divides it down to 5 kHz . It also takes the LO sample input and divides it down to 50 kHz . The two 5 kHz divided
down signals are compared inside of U9 and any differences are connected to U9 pin 16. The output of $U 9$ at pin 16 are 5 kHz pulses whose pulse width varies as any differences between the $10-\mathrm{MHz}$ and VCXO frequencies are detected. These pulses are changed to a DC voltage level by the capacitor-resistor filter network, C32, C36, C42, C38 and R49. The AFC voltage is then connected to the + input of U4B that amplifies it and connects it to jack J9. W2 on 19 must be in the operate position, between pins 1 and 2, for the PLL circuit to operate. With jumper W2 between pins 2 and 3 on J6, set up, the AFC bias is set by R43. NOTE: With the VCXO, located on the UHF Generator Board, set on frequency, the voltage as measured at TP2 should be -2 VDC.

The AFC output of $\mathrm{J9}$ is split with one path connected to J43 pin 13A. The other path is amplified by U7B and connected to J12, VCXO AFC Output, on the board that connects to the VCXO on the UHF generator board. The PLL circuit, when locked, will maintain the very accurate VCXO output frequency because any change in frequency will be corrected by the AFC error voltage.

## Lock Detector Circuit

IC chip U9 contains an internal lock detector that indicates the status of the PLL circuit. When U9 is in a locked state, pin 12 goes high; the high is applied to Q1, which is biased off. With Q1 off, pin 3 goes low and is connected to DS1, the Red Unlock LED, which does not lit. Q1 pin 3 low also connects to Q2 that is biased off. The drain of Q2, a high, is wired to J 43 pin 15A, the PLL Lock Indicator output of the board.

If the $5-\mathrm{kHz}$ from the $10-\mathrm{MHz}$ reference and the $5-\mathrm{kHz}$ from the VCXO become unlocked, out of the capture range of the PLL, pin 12 of U9 goes to a logic low that connects to the base of Q1. This biases On Q1 causing pin 3 to go high. The high connects to DS1, the red Unlock LED, which lights, and to Q2, which is biased on. When Q2 is biased on, it connects a low to
jack J43 pin 15A, the PLL Lock Indicator output of the board.

## Voltage Requirements

The board is powered by $\pm 12$ VDC that is produced by an external power supply. +12 VDC enters the board through J43 pins 18A, B \& C, and is filtered and isolated by L5, L6 and the shunt capacitor C24. The +12 VDC is then applied to the rest of the board and to J14 pin 3 for use by the UHF Generator Board.

One connection of the +12 VDC is to IC U12. U12 and associated circuitry produce a +9 VDC that connects to J14 pin 1 for use by the UHF Generator Board.

Another connection of the +12 VDC is to $a+5$ VDC regulator. The +12 VDC connects to diodes CR6 and CR7 that along with the pi type filter consisting of C56, L10, C54 and C55 removes any noise from the +12 VDC before it connects to the +5 VDC regulator IC U8. The output of the IC U8, +5 VDC, connects to the rest of the board.

The - 12 VDC enters the board through J43 pins 19A, B \& C and is filtered and isolated by L 7 and the shunt capacitor C28. The -12 VDC is then applied to the rest of the board and to J14 pin 5 for use by the UHF Generator Board.

## 4.4 (A4) Control Monitoring/ Power Supply Module (110 VAC, 1301936 OR 220 VAC, 1303229;Appendix B)

The Control Monitoring/Power Supply Module Assembly contains (A1) a Power Protection Board (1302837), (A2) a 600
Watt Switching Power Supply, (A3) a Control Board (1302021), (A4) a Switch Board (1527-1406) and (A5) a LCD Display.

AC Input to Pioneer Exciter/Amplifier Chassis Assembly

The AC input to the Pioneer
Exciter/Amplifier Chassis Assembly is connected from J1, part of a fused entry module, located on the rear of the chassis assembly to $\mathrm{J50}$ on the Control Monitoring/Power Supply Module. There are two possible modules that can be part of your system, 1301936 for 110 VAC or 1303229 for 220 VAC operation. J50-10 is line \#1 input, J50-8 is earth ground and J50-9 is line \#2 input. The input AC connects to J1 on the Power Protection Board where it is fuse protected and connected back to J50, at J50-11 AC Line \#1 and J50-12 AC Line \#2, for distribution to the cooling Fan.

### 4.4.1 (A1) Power Protection Board (1302837; Appendix B)

The input AC connects through J1 to two 10 Amp AC fuses F1 and F2. The AC line \#1 input connects from J1-1 to the F1 fuse. The AC line \#1 input after the F1 fuse is split with one line connected back to Jack J1 Pin 4, which becomes the AC Line \#1 to the Fan. The other line of the split connects to J4. The AC line \#2 input connects from J1-3 to the F2 fuse. The AC line \#2 input after the F2 fuse is split with one line connected back to Jack J1 at Pin 5, which becomes the AC Line \#2 to the Fan. The other line of the split connects to J2. J1-2 is the earth ground input for the AC and connects to J3.

Three 150-VAC, for 115 VAC input, or three $275-\mathrm{VAC}$, for 230 VAC input, MOVs are connected to the input $A C$ for protection. One connects from each AC line to ground and one connects across the two lines. VR1 connects from J4 to J2, VR2 connects from J4 to 33 and VR3 connects from J2 to J 3 .
+12 VDC Circuits
+12 VDC from the Switching Power Supply Assembly connects to 36 on the board. The +12 VDC is divided into four separate circuits each with a 3 amp self resetting fuse, PS3, PS4, PS5 and PS6.

The polyswitch resettable fuses may open on a current as low as 2.43 Amps at $50^{\circ} \mathrm{C}, 3 \mathrm{Amps}$ at $25^{\circ} \mathrm{C}$ or 3.3 Amps at $0^{\circ} \mathrm{C}$. They definitely will open when the current is 4.86 Amps at $50^{\circ} \mathrm{C}, 6 \mathrm{Amps}$ at $25^{\circ} \mathrm{C}$ or 6.6 Amps at $0^{\circ} \mathrm{C}$.

PS3 protects the +12 VDC 2 Amp circuits for the System Controller, the Amplifier Controller and the Spare Slot through J62 pins 7, 8, 9 and 10. If this circuit is operational, the Green LED DS3, mounted on the board, will be lit.

PS4 protects the +12 VDC 2 Amp circuits for the Modulator and the IF Processor through J62 pins 13, 14, 15 and 16. If this circuit is operational, the Green LED DS4, mounted on the board, will be lit

PS5 protects the +12 VDC 2 Amp circuits for the Upconverter through J62 pins $17,18,19$ and 20. If this circuit is operational, the Green LED DS5, mounted on the board, will be lit

PS6 protects the +12 VDC 2 Amp circuits for the Remote through J63 pins 17, 18, 19 and 20. If this circuit is operational, the Green LED DS6, mounted on the board, will be lit

## -12 VDC Circuits

-12 VDC from the Switching Power Supply Assembly connects to J5 on the board. The -12 VDC is divided into two separate circuits each with a 3 amp self resetting fuse, PS1 and PS2.

PS1 protects the -12 VDC 2 Amp circuits for the System through J63 pins 1, 2, 3 and 4. If this circuit is operational, the Green LED DS1, mounted on the board, will be lit

PS2 protects the -12 VDC 2 Amp circuits for the Remote through J62 pins 1, 2, 3 and 4. If this circuit is operational, the Green LED DS2, mounted on the board, will be lit

The connections from J62 and J63 of the Power Protection Board are wired to J62 and J 63 on the Control Board.

### 4.4.2 (A3) Control Board (1302021; Appendix B)

In this transmitter, control monitoring functions and front panel operator interfaces are found on the Control Board. Front panel operator interfaces are brought to the control board using a 26 position conductor ribbon cable that plugs into J60. The control board controls and monitors the Power Supply and Power Amplifier module through a 16 position connector 361 and two 20 position connectors J 62 \& J 63.

## Schematic Page 1

U 1 is an 8 bit RISC microcontroller that is in circuit programmed or programmed using the serial programming port J4 on the board. When the microcontroller, U1, is held in reset, low on pin 20, by either the programming port or the external watchdog IC (U2), a FET Q1 inverts the reset signal to a high that connects to the control lines of U5, an analog switch. The closed contacts of U5 connects the serial programming lines from J4 to U1. LED DS10 will be lit when programming port J4 is used.

U2 is a watchdog IC used to hold the microcontroller in reset, if the supply voltage is less the 4.21 VDC ; (1.25 VDC < Pin 4 (IN) < Pin 2 (Vcc). The watchdog momentarily resets the microcontroller, if Pin 6 (ST) is not clocked every second. A manual reset switch S1 is provided but should not be needed.

Diodes DS1 through DS8 are used for display of auto test results. A test board is used to execute self test routines. When the test board is installed, Auto_Test_1 is held low and Auto_Test_2 is allowed to float at 5 VDC . This is the signal to start the auto test routines.

U3 and U4 are used to selectively enable various input and output ICs found on pages $2 \& 3$ of the schematic.

U1 has two serial ports available. In this application, one port is used to communicate with transmitter system components where U 1 is the master of a RS-485 serial bus. The other serial port is used to provide serial data I/O where U1 is not the master of the data port. A dual RS-232 port driver IC and a RS-485 Port driver is also in the second serial data I/O system. The serial ports are wired such that serial data input can come through one of the three serial port channels. Data output is sent out through each of the three serial port channels.

Switch SW1, transmitter operation select, is used to select either transmitter operation or exciter/driver operation. When the contacts of SW1 are closed, transmitter operation is selected and the power monitoring lines of the transmitter's power amplifier are routed to the system power monitoring lines.

## Schematic Page 2

U9 is a non-inverting transceiver IC that provides 2 way asynchronous communication between data busses. . The IC is used as an input buffer to allow the microcontroller to monitor various digital input values.

Digital output latch circuits are used to control system devices. Remote output circuits are implemented using open drain FETs, Q13, Q14, Q16, and Q17, with greater than 60 Volt drain to source voltage ratings.

Remote digital inputs are diode protected, using CR6, CR7, CR8 and CR9 with a $1 \mathrm{k} \Omega$ pull-up resistor, to +5 VDC . If the remote input voltage is greater than about 2 Volts or floating, the FET is turned on and a logic low is applied to the digital input buffer, U9. If the remote input voltage is less than the
turn on threshold of the FET (about 2 VDC), a logic high is applied to the digital input buffer, U9.

Four of the circuits on page two of the schematic, which include Q2, Q9, Q19 and Q21, are auxiliary I/O connections wired for future use. They are wired similar to the remote digital inputs but include a FET, Q5, Q12, Q20 and Q22, for digital output operations. To operate these signals as inputs, the associated output FET must be turned off. The FETs are controlled by U10 and U12, analog input multiplexer ICs.

Schematic Page 3
U13, U14, U15, U16, U17 and U18 are 3 state non-inverting transceiver ICs that provide 2 way asynchronous communication between data busses. The ICs are used as input buffers to allow the microcontroller to monitor various digital input values. The digital inputs to the ICs utilize a $10 \mathrm{k} \Omega$ pull-up resistor. The buffer IC, U18, used for data transfer to the display is wired for read and write control.

## Schematic Page 4

U19 and U20 are digitally controlled analog switches that provide samples back to the microprocessor. Each analog input is expected to be between 0 and 5 VDC. If a signal exceeds 5.1 VDC , a 5.1 Volt zener diode clamps the signals voltage, to prevent damage to the IC. Most signals are calibrated at their source, however two dual serial potentiometers ICs are used to calibrate four signals, System Visual/Average Power, System Aural Power, System Reflected Power and the Spare AIN 1. For these four circuits, the input value is divided in half before it is applied to an op-amp. The serial potentiometer is used to adjust the output signal level to between 80 and $120 \%$ of the input signal level. Serial data, serial clock and serial pot enables are supplied by the microprocessor to the dual serial potentiometer ICs. J62 and J63 are two 20 position connectors that provide the +12 VDC and -12 VDC power through the

Power Protection Board. The $\pm 12$ VDC generated by the switching power supply connects to J62 and J63 after being fuse protected on the Power Protection Board.

## Schematic Page 5

There are three dual element, red/green, common cathode LED indicators mounted on the front panel of the sled assembly; DC OK, Operate and Fault.

There are three, the fourth is a spare, identical circuits that drive the front panel mounted LED indicators. The levels on the 1, 2, 3 and 4 LED Control Lines, for both the red and green LEDs, are generated by the IC U11 as controlled by the DATABUS from the microprocessor U1.

Each LED controller circuit consists of an N -Channel MOSFET w/internal diode that controls the base of an $\mathrm{N}-\mathrm{P}-\mathrm{N}$ transistor in an emitter follower configuration. The emitter of the transistor connects the LED.

With the LED control line LOW, the MOSFET is Off, which causes the base of the transistor to increase towards +12 VDC, forward biasing the transistor. With the transistor forward biased, current will flow from ground through the LED, the transistor and the current limiting resistors in the collector to the +12 VDC source. The effected LED will light.

With the LED control line HIGH, the MOSFET is On, which causes the base of the transistor go toward ground potential, reverse biasing the transistor. With the transistor reverse biased, no current through the transistor and LED, therefore the effected LED will not light.

A third color, amber, can also be generated by having both transistors conducting, both control lines LOW. The amber color is produced because the current applied to the green element is
slightly greater than the red element. This occurs because the current limiting resistors have a smaller ohm value in the green circuit.

There are four voltage regulators, three for +5 VDC and one for +7 VDC, which are used to power the Control Board. +12 VDC is applied to U25 the +7 VDC regulator that produces the +7 V , which is applied to the LEDs mounted on the board. The +7 V is also connected to the input of U26 a precision +5.0 Volt regulator. The +5.0 Vdc regulator output is used to power the analog circuits and as the microcontroller analog reference voltage. Another two +5 Volt regulator circuits U27, +5V, and U8, +5 Vserial, are used for most other board circuits.

### 4.4.3 (A4) Switch Board (1527-1406; Appendix B)

The switch board provides five front-panel momentary contact switches for user control and interface with the front-panel LCD menu selections. The switches, SW1 to SW5, complete the circuit through connector J1 to connector J2 that connects to J1 on (A5) the 20 Character by 4 line LCD Display. J1 on the switch board is also cabled to the Control Board. When a switch is closed, it connects a logic low to the control board that supplies the information from the selected source to the display. By pushing the button again, a different source is selected. This occurs for each push button. Refer to Chapter 3 Section 3.5.4, for more information on the Display Menu Screens.

### 4.4.4 (A2) Switching Power Supply Assembly

The power supply module contains a switching power supply, an eight position terminal block for distributing the DC voltages, a three position terminal block to which the AC Input connects, Jacks J1, V1 and V2. Jack J1 connects to the Control Board and supplies DC OK, at J1-4 \& 3, and AC OK, at J1-2 \& 1, status to the control board. A Power Supply enable connects from the control board to the
power supply at V1-6 \& 7. The power supply is configured for three output voltages $+12 \mathrm{~V},-12 \mathrm{~V}$, at the 8 position terminal block, and a main output power of +32 VDC at J 50 pin $\mathrm{A}(+)$ and J 50 pin $B$ (Rtn). The power supply is power factor corrected to .98 for optimum efficiency and decrease in energy consumption. For safety purposes all outputs are over voltage and over current protected. This supply accepts input voltages from 85 to 264 volts AC, but the power entry module, for the exciter/amplifier chassis, must be switched to the proper input voltage setting, for the transmitter to operate.

## 4.5 (A4) Power Amplifier Module Assembly (1301923; Appendix B)

NOTE: Used in 10W-100W Transmitters.
The Power Amplifier Module Assembly contains (A1) a 1 Watt UHF Amplifier Module Assembly (1302891), (A2) a 40 Watt UHF Module Assembly (1206693), (A3) UHF RF Module Pallet Assembly (1300116), (A4) a Coupler Board Assembly (11301949), (A5) an Amplifier Control Board (1301962) and (A6) a Temperature Sensor IC.

The RF from the Upconverter Module Assembly connects from the Upconverter RF Output BNC Jack J23, through a cable, to the PA RF Input BNC Jack J24, located on the rear of the exciter/amplifier chassis assembly.

### 4.5.1 (A1) 1-Watt UHF Module Assembly (1302891; Appendix B)

The 1-watt UHF module assembly provides radio frequency interference (RFI) and electromagnetic interference (EMI) protection, as well as the heatsink, for the 1-watt UHF amplifier board (1302762) that is mounted inside the assembly. The assembly has approximately 17 dB of gain.

The RF input to the assembly connects to SMA Jack J3. The amplified RF output of
the assembly is at the SMA Jack J4. Typically, with an input signal of +4 dBm at J1 of the assembly, an output of +21 dBm can be expected at J 2 .

The +12-VDC bias voltage connects through J5, a RF-bypassed, feed-through capacitor, to the amplifier board. The -12-VDC bias voltage connects through J6, a RF-bypassed, feed-through capacitor, to the amplifier board. E1 on the assembly connects to Chassis ground.

### 4.5.2 (A1-A1) 1-Watt UHF Amplifier Board (1302761; Appendix B)

The 1-watt UHF amplifier board is mounted in the 1 -watt UHF amplifier assembly (1302891) and provides approximately +17 dB of gain.

The UHF signal enters the board at J3, a SMA connector, and is applied to U3 an IC hybrid coupler assembly that splits the input signal into two equal parts. The two amplifier paths are identical using Q4 and Q5, 1-Watt HFETs as the amplifier devices. Each HFET has approximately 14 dB of gain.

The drain voltage needed to operate each HFET is obtained from the +12 VDC line that connects to the board at J5 and is regulated down to +8.25 volts by U 4 . The gate negative bias voltage is obtained from the -12 VDC line that connects to the board at J 6 .

The amplified outputs of the HFETs are applied to U2 an IC hybrid coupler assembly that combines the amplified signals into a single output that connects to $\mathrm{J4}$ of the board.

### 4.5.3 (A4-A1) 40 Watt UHF Amplifier Assembly (1206693; Appendix B)

The output of the UHF filter is connected to the input J1 of (A2) the 40 Watt UHF amplifier assembly (Figure 4-1). The assembly is made up of a (51-5378-30800 ) module, which operates class $A B$ and is a highly linear broadband amplifier for the frequency range of 470 to 860 MHz . It can
deliver an output power of 40 watts (CW) with approximately 14 dB of gain.

The amplification circuit consists of LDMOS transistors V804 and V805 connected in parallel and operating in class $A B$. The paralleling network is achieved with the aid of 3 dB couplers Z802 and Z803. A further 3 dB coupler Z801, in conjunction with capacitors C800 and C819, serves as a phase shifter. Phase alignment (for the complete amplifier), as well as quiescent current settings are achieved by means
of potentiometers R807 and R808. The settings are factory implemented and should not be altered.

PIN diodes V810 \& V811 form a variabledamping circuit that is used to adjust the amplification of the 40 -watt module. The adjustment is performed with the Gain potentiometer R838. A readjustment of the amplification may be required, after repair work, to ensure that the PAs in multiple PA transmitters deliver the same output power


Figure 4-1: 40 Watt UHF Amplifier Module

### 4.5.4 (A3) UHF Module Assembly, RF Module Pallet, Philips (1300116; Appendix B)

The UHF Module Assembly, 250-watt module (Figure 4-2) is a broadband amplifier for the frequency range 470 to 860 MHz . The amplifier is capable of delivering an output power of $70 \mathrm{~W}_{\text {rms }}$. The amplification is approximately 13 dB.

The amplification circuit consists of the parallel connected push-pull amplifier
blocks V1 and V2 operating in class AB. In order to match the transistor impedance to the characteristic impedance of the input and output sides, matching networks are placed ahead and behind the amplifier blocks. Transformers Z3 to Z6 serve to balance the input and output signals. The paralleling circuit is achieved with the aid of $3-\mathrm{dB}$ couplers Z 1 and Z 2 .

The working point setting is factory implemented by means of potentiometers R9, R11, and R12 and should not be altered.


Figure 4-2. UHF Amplifier Module, 250 Watts

### 4.5.5 (A4) Coupler Board Assembly (1301949; Appendix B)

The UHF coupler board assembly provides a forward and reflected power samples of the output to (A5) the amplifier control board where it connects to the input of the overdrive-protection circuit.

The RF input to the UHF coupler assembly, from the 250 Watt UHF amplifier module, connects to SMA jack J1. The RF is connected by a stripline track to the SMA type connector RF Output jack J2. A hybrid-coupler circuit picks off a power sample that is connected to SMA type connector jack J3 as the forward power sample. Another power sample is taken from the coupler circuit that is connected to SMA type connector jack J6 as the reflected power sample. Two $50 \Omega$ terminations, used as dissipation loads, connect to the reject and reflected ports, J 5 and J4, of the coupler.

### 4.5.6 (A5) Amplifier Control Board (1301962; Appendix B)

The amplifier control board provides LED fault and enable indications on the front panel of the module and also performs the following functions: overdrive cutback, when the drive level reaches the amount needed to attain $110 \%$ output power; and overtemperature, VSWR, and overdrive faults. The board also provides connections to the LCD Display for monitoring the \% Reflected Power, \% Output Power, and the power supply voltage.

## Page 1

U4, located upper center of page, is an in circuit microcontroller. The controller is operated at the frequency of 3.6864 MHz using crystal Y1. Programming of this device is performed through the serial programming port J2. U4 selects the desired analog channel of U1 through the settings of PAO-PA3. The outputs of Port

A must be set and not changed during an analog input read of channels PA5-PA7. PA4 of U4 is a processor operating LED that monitors the $+/-12$ VDC. PA5 is used to monitor the +12 VDC supply to the board. PA6 is the selected channel of analog switch U1. PA7 is connected to a via, V10, for future access.

U6 is a serial to RS-485 driver IC. U7 is a watchdog IC used to hold the microprocessor in reset, if the supply voltage is less than 4.21 VDC. U7 momentarily resets the microcontroller if Pin 6 (!ST) is not clocked every second. A manual reset switch is provided but should not be needed.

Upper left corner U3 is used to determine where the amplifier control board is located. The eight inputs come from the main amp connector and are used to set the SCADA address of the controller. Pullup resistors set a default condition of logic high.

U5 below U3 is used for getting digital input information of the board. Page two has several monitoring circuits that provide information on the amplifier's status. Many of these circuits automatically shut down the amplifier if a specific fault occurs.

U8 below U5 is used to control four board mounted status LEDs. A FET is turned On to shunt current away from the LED to turn it Off. U9 below U8 is used to enable different features within the software. Actual use is to be determined.

## Page 2

In the lower right corner are voltage regulator circuits. U22 should allow for 0.14 amps of power using its 92 C/W rating if $\mathrm{Ta}=60^{\circ} \mathrm{C}$ max and $\mathrm{Tj}=125^{\circ} \mathrm{C}$ $\max 0.26$ amps can be obtained from U22 if the mounting pad is 0.5 square inches. The controller will not need this much current.

[^0]than or equal to $1 \%$. 100 mA of current is available from each device but again the controller will not need this much current.

In the upper left section are circuits with U12 and U13. U12 is used to generate a regulated voltage that is about 5 volts less than the +32 VDC supply, approximately +26.25 VDC. When the +32 VDC supply is enabled, the circuitry around U13B is used to provide gate voltage to Q10 that is 5 volts greater than the source pin of this FET. The gate of Q10 can be turned Off by any one of a few different circuits.

U10A is used to turn Off the gate of Q10 in the event of high current in amplifier \#1. At 0.886 VDC the current to amplifier \#1 should be greater than 5 Amps. U11B is used to turn off the Q10 FET, if high current is detected in amplifier \#2. U11A is used to turn off the Q10 FET, if high current is detected in amplifier \#3. With 2.257 VDC at Pin 5 of U11B or Pin 3 of U11A, the voltage output of current sense amplifier U17 or U18 at high current shut down should be greater than 15 Amps.

U14B is used to turn Off the gate of Q10 in the event of high power supply voltage, approximately +35.4 VDC. U14A is used to keep the FET disabled in the event of low power supply voltage, approximately +25.4 VDC.

Current monitoring sections of the board.
The ICs U16, U17 and U18 along with associated components set up the current monitoring sections of the board. R67, R68 and R69 are 0.01 $/ 5 \mathrm{~W}$ 1\% through hole resistor is used for monitoring the current through several sections of the amplifier. The voltage developed across these resistors are amplified for current monitoring by U16, U17 or U18. The LT1787HVCS8 precision high side current sense IC amplifier accepts a maximum voltage of 60 VDC. The $43.2 \mathrm{k} \Omega$ resistor from pin 5 to
ground sets the gain of the amplifier to about 17.28. This value is not set with much accuracy since the manufacturer internally matches the resistors of this part but their actual resistance value is not closely defined. A trimming resistor is suggested to give a temperature stability of $-200 \mathrm{ppm} / \mathrm{C}$, but instead the microcontroller will determine the exact gain of the circuit and use a correction factor for measurements. Circuit loading components are located in the lower portion of each current monitoring circuit. These components allow for short duration high current loading of the supply. By measuring the current through the sense resistor with and without the additional four $30.1 \Omega 1 \%$ resistors. For very short duration pulses, a 1206 resistor can handle up to 60 watts. The processor requires 226 uSec per conversion. A supply voltage of +32 VDC will pass $1.06 \mathrm{amps}+1 \%$ through the load resistors.

A6 is a temperature sensor thermistor that is used to monitor the temperature of the module's heat sink. It connects to J6 pins $1 \& 2$ on the board wand is wired to the comparator IC U10B. If the temperature increases above $75^{\circ} \mathrm{C}$ the output will go Low that is used as a temperature fault output, which generates a Fault alert at U15A and disables Amplifier \#1.

Aural, Visual/Average and Reflected power detector sections of the board.

## Page 3

A Forward Power Sample enters the board at SMA Jack J3 and is split. One part connects to J4 on the board that is cabled to J1, the SMA Forward Power Sample Jack, located on the front panel of the assembly. The other part of the split forward power sample is detected by CR17 and the DC level amplified by U25A. The output of U25A at pin 1 is split with one part connected to the Aural Power sample, which is not used in this digital transmitter. The other split output connects to U265A that is part of the Forward Average Power
circuit. The detected level is connected to L4 that is part of an intercarrier notch filter circuit that is tuned to eliminate the 4.5 MHz aural intercarrier, if present. The Average power sample is amplified by U26D and connected through the average calibration pot R166 to U26C. The output of U26C is connected to the comparator IC U26B that has Aural Null and Offset Null, if present in the system, connected to the other input. The output Average Forward power level connects to J9 pin 2 of the board.

A Reflected Power Sample enters the board at SMA Jack J5 and is detected by CR20 and the DC level amplified by U28B. The output of U28B at pin 7 is connected through the reflected calibration pot R163 to U28C. The output is split with one part connected to J9 pin 5, the Reflected Power Output level of the board. The other part of the split from U28C connects to the comparator IC U28D that has a reference level connected to the other input. If the reflected level increases above the reference level a low output is produced and connected to the Reflected Power Shutdown circuit at CR28. The low shuts off Q14 causing pin 3 to go high that is connected to the inverter U15C. The output of U15C goes low producing a Reflected Power Fault that is connected to an output of the board, the Fault Alert circuit and also shuts down Amplifier \#1.

Gain of the power measurements is completed through software. Only the Aural Null and Offset Null need to be done through front panel pots.

This completes the description of the Power Amplifier Module Assembly that is used with 10 W to 100 W transmitters.

### 4.5.7 (A9) Bandpass and (A10) Trap Filter

The RF Output of the Tray is connected to (A9) the Bandpass Filter and then to (A10) the UHF Trap Filter Assembly. Both filters are tuned to provide high out
of band rejection of unwanted products. The filtered RF Output at the " N " connector jack (J2) of the Trap Filter is cabled to the Antenna for your System.

## 4.6 (A4) Driver Amplifier Module Assembly (1302846; Appendix B)

NOTE: Used with high power transmitters with external PA assemblies.

The Power Amplifier Module Assembly contains (A1) a 1 Watt UHF Amplifier Module Assembly (1302891), (A2) a 40 Watt UHF Module Assembly (1206693), (A4) a Coupler Board Assembly (11301949), (A5) an Amplifier Control Board (1301962) and (A6) a Temperature Sensor IC.

The RF from the Upconverter Module Assembly connects from the Upconverter RF Output BNC Jack J23, through a cable, to the PA RF Input BNC Jack J24, located on the rear of the exciter/amplifier chassis assembly.

### 4.6.1 (A1) 1-Watt UHF Module Assembly (1302891; Appendix B)

The 1-watt UHF module assembly provides radio frequency interference (RFI) and electromagnetic interference (EMI) protection, as well as the heatsink, for the 1-watt UHF amplifier board (1302762) that is mounted inside the assembly. The assembly has approximately 17 dB of gain.

The RF input to the assembly connects to SMA Jack J3. The amplified RF output of the assembly is at the SMA Jack J4. Typically, with an input signal of +4 dBm at J1 of the assembly, an output of +21 dBm can be expected at J2.

The $+12-\mathrm{VDC}$ bias voltage connects through J5, a RF-bypassed, feed-through capacitor, to the amplifier board. The -12-VDC bias voltage connects through J6, a RF-bypassed, feed-through capacitor, to the amplifier board. E1 on the assembly connects to Chassis ground.

### 4.6.2 (A1-A1) 1-Watt UHF Amplifier Board (1302761; Appendix B)

The 1-watt UHF amplifier board is mounted in the 1-watt UHF amplifier assembly (1302891) and provides approximately +17 dB of gain.

The UHF signal enters the board at J3, a SMA connector, and is applied to U3 an IC hybrid coupler assembly that splits the input signal into two equal parts. The two amplifier paths are identical using Q4 and Q5, 1-Watt HFETs as the amplifier devices. Each HFET has approximately 14 dB of gain.

The drain voltage needed to operate each HFET is obtained from the +12 VDC line that connects to the board at J5 and is regulated down to +8.25 volts by U 4 . The gate negative bias voltage is obtained from the - 12 VDC line that connects to the board at J6.

The amplified outputs of the HFETs are applied to U2 an IC hybrid coupler assembly that combines the amplified signals into a single output that connects to J4 of the board.

### 4.6.3 (A4-A1) 40 Watt UHF Amplifier Assembly (1206693; Appendix B)

The output of the UHF filter is connected to the input J1 of (A2) the 40 Watt UHF


Figure 4-3: 40 Watt UHF Amplifier Module

### 4.6.4 (A4) Coupler Board Assembly (1301949; Appendix B)

amplifier assembly (Figure 4-1). The assembly is made up of a (51-5378-30800 ) module, which operates class $A B$ and is a highly linear broadband amplifier for the frequency range of 470 to 860 MHz . It can deliver an output power of 40 watts (CW) with approximately 14 dB of gain. It is set as needed to provide the drive level to the external PA Assemblies.

The amplification circuit consists of LDMOS transistors V804 and V805 connected in parallel and operating in class $A B$. The paralleling network is achieved with the aid of 3 dB couplers Z802 and Z803. A further 3 dB coupler Z801, in conjunction with capacitors C800 and C819, serves as a phase shifter. Phase alignment (for the complete amplifier), as well as quiescent current settings are achieved by means of potentiometers R807 and R808. The settings are factory implemented and should not be altered.

PIN diodes V810 \& V811 form a variabledamping circuit that is used to adjust the amplification of the 40 -watt module. The adjustment is performed with the Gain potentiometer R838. A readjustment of the amplification may be required, after repair work, to ensure that the PAs in multiple PA transmitters deliver the same output power.
board where it connects to the input of the overdrive-protection circuit.

The RF input to the UHF coupler assembly, from the 40 Watt UHF amplifier module, connects to SMA jack J1. The RF is connected by a stripline track to the SMA type connector RF Output jack J2. A hybrid-coupler circuit picks off a power sample that is connected to SMA type connector jack J3 as the forward power sample. Another power sample is taken from the coupler circuit that is connected to SMA type connector jack J6 as the reflected power sample. Two $50 \Omega$ terminations, used as dissipation loads, connect to the reject and reflected ports, J5 and J4, of the coupler.

### 4.6.5 (A5) Amplifier Control Board (1301962; Appendix B)

The amplifier control board provides LED fault and enable indications on the front panel of the module and also performs the following functions: overdrive cutback, when the drive level reaches the amount needed to attain $110 \%$ output power; and overtemperature, VSWR, and overdrive faults. The board also provides connections to the LCD Display for monitoring the \% Reflected Power, \% Output Power, and the power supply voltage.

## Page 1

U4, located upper center of page, is an in circuit microcontroller. The controller is operated at the frequency of 3.6864 MHz using crystal Y1. Programming of this device is performed through the serial programming port J2. U4 selects the desired analog channel of U1 through the settings of PAO-PA3. The outputs of Port A must be set and not changed during an analog input read of channels PA5-PA7. PA4 of U4 is a processor operating LED that monitors the $+/-12$ VDC. PA5 is used to monitor the +12 VDC supply to the board. PA6 is the selected channel of
analog switch U1. PA7 is connected to a via, V10, for future access.

U6 is a serial to RS-485 driver IC. U7 is a watchdog IC used to hold the microprocessor in reset, if the supply voltage is less than 4.21 VDC. U7 momentarily resets the microcontroller if Pin 6 (!ST) is not clocked every second. A manual reset switch is provided but should not be needed.

Upper left corner U3 is used to determine where the amplifier control board is located. The eight inputs come from the main amp connector and are used to set the SCADA address of the controller. Pullup resistors set a default condition of logic high.

U5 below U3 is used for getting digital input information of the board. Page two has several monitoring circuits that provide information on the amplifier's status. Many of these circuits automatically shut down the amplifier if a specific fault occurs.

U8 below U5 is used to control four board mounted status LEDs. A FET is turned On to shunt current away from the LED to turn it Off. U9 below U8 is used to enable different features within the software. Actual use is to be determined.

## Page 2

In the lower right corner are voltage regulator circuits. U22 should allow for 0.14 amps of power using its $92 \mathrm{C} / \mathrm{W}$ rating if $\mathrm{Ta}=60^{\circ} \mathrm{C}$ max and $\mathrm{Tj}=125^{\circ} \mathrm{C}$ max 0.26 amps can be obtained from U22 if the mounting pad is 0.5 square inches. The controller will not need this much current.

U23 and U24 are low drop out +5 VDC, voltage regulators with a tolerance greater than or equal to $1 \%$. 100 mA of current is available from each device but again the controller will not need this much current.

In the upper left section are circuits with U12 and U13. U12 is used to generate a
regulated voltage that is about 5 volts less than the +32 VDC supply, approximately +26.25 VDC. When the +32 VDC supply is enabled, the circuitry around U13B is used to provide gate voltage to Q10 that is 5 volts greater than the source pin of this FET. The gate of Q10 can be turned Off by any one of a few different circuits.

U10A is used to turn Off the gate of Q10 in the event of high current in amplifier \#1. At 0.886 VDC the current to amplifier \#1 should be greater than 5 Amps. U11B is used to turn off the Q10 FET, if high current is detected in amplifier \#2. U11A is used to turn off the Q10 FET, if high current is detected in amplifier \#3. With 2.257 VDC at Pin 5 of U11B or Pin 3 of U11A, the voltage output of current sense amplifier U17 or U18 at high current shut down should be greater than 15 Amps.

U14B is used to turn Off the gate of Q10 in the event of high power supply voltage, approximately +35.4 VDC. U14A is used to keep the FET disabled in the event of low power supply voltage, approximately +25.4 VDC.

Current monitoring sections of the board.
The ICs U16, U17 and U18 along with associated components set up the current monitoring sections of the board. R67, R68 and R69 are 0.01 $/$ /5W 1\% through hole resistor is used for monitoring the current through several sections of the amplifier. The voltage developed across these resistors are amplified for current monitoring by U16, U17 or U18. The LT1787HVCS8 precision high side current sense IC amplifier accepts a maximum voltage of 60 VDC. The $43.2 \mathrm{k} \Omega$ resistor from pin 5 to ground sets the gain of the amplifier to about 17.28. This value is not set with much accuracy since the manufacturer internally matches the resistors of this part but their actual resistance value is not closely defined. A trimming resistor is suggested to give a temperature
stability of $-200 \mathrm{ppm} / \mathrm{C}$, but instead the microcontroller will determine the exact gain of the circuit and use a correction factor for measurements. Circuit loading components are located in the lower portion of each current monitoring circuit. These components allow for short duration high current loading of the supply. By measuring the current through the sense resistor with and without the additional four $30.1 \Omega 1 \%$ resistors. For very short duration pulses, a 1206 resistor can handle up to 60 watts. The processor requires 226 uSec per conversion. A supply voltage of +32 VDC will pass 1.06 amps $+1 \%$ through the load resistors.

A6 is a temperature sensor thermistor that is used to monitor the temperature of the module's heat sink. It connects to J6 pins $1 \& 2$ on the board wand is wired to the comparator IC U10B. If the temperature increases above $75^{\circ} \mathrm{C}$ the output will go Low that is used as a temperature fault output, which generates a Fault alert at U15A and disables Amplifier \#1.

Aural, Visual/Average and Reflected power detector sections of the board.

## Page 3

A Forward Power Sample enters the board at SMA Jack J3 and is split. One part connects to $\mathrm{J4}$ on the board that is cabled to J1, the SMA Forward Power Sample Jack, located on the front panel of the assembly. The other part of the split forward power sample is detected by CR17 and the DC level amplified by U25A. The output of U25A at pin 1 is split with one part connected to the Aural Power sample, which is not used in this digital transmitter. The other split output connects to U265A that is part of the Forward Average Power circuit. The detected level is connected to L4 that is part of an intercarrier notch filter circuit that is tuned to eliminate the 4.5 MHz aural intercarrier, if present. The Average power sample is amplified by U26D and connected through the average calibration pot R166 to U26C. The output
of U26C is connected to the comparator IC U26B that has Aural Null and Offset Null, if present in the system, connected to the other input. The output Average Forward power level connects to 19 pin 2 of the board.

A Reflected Power Sample enters the board at SMA Jack $J 5$ and is detected by CR20 and the DC level amplified by U28B. The output of U28B at pin 7 is connected through the reflected calibration pot R163 to U28C. The output is split with one part connected to 19 pin 5, the Reflected Power Output level of the board. The other part of the split from U28C connects to the comparator IC U28D that has a reference level connected to the other input. If the reflected level increases above the reference level a low output is produced and connected to the Reflected Power Shutdown circuit at CR28. The low shuts off Q14 causing pin 3 to go high that is connected to the inverter U15C. The output of U15C goes low producing a

Reflected Power Fault that is connected to an output of the board, the Fault Alert circuit and also shuts down Amplifier \#1.

Gain of the power measurements is completed through software. Only the Aural Null and Offset Null need to be done through front panel pots.

This completes the description of the Driver Amplifier Module Assembly, which is used in high power transmitters with external PA assemblies.

The output of the driver amplifier module assembly connects to the output of the Exciter/Amplifier chassis assembly at the "N" type connector Jack J25. The RF output at J25 connects to J200 the RF input to the external Power Amplifier Assembly.

This also completes the description for the entire Exciter/Amplifier chassis assembly.

## Chapter 5 <br> Detailed Alignment Procedures

This transmitter was aligned at the factory and should not require additional adjustments to achieve normal operation.

This transmitter takes the baseband audio and video inputs or, if the (Optional) $4.5-\mathrm{MHz}$ composite input kit is purchased, either a single composite video $+4.5-\mathrm{MHz}$ input or separate baseband video and audio inputs, and converts them to the desired UHF On Channel RF Output at the systems output power level.

The exciter/amplifier of the LX Series transmitter is of a Modular design and when a Module fails that module needs to be changed out with a replacement module. The failed module can then be sent back to Axcera for repair. Contact Axcera Customer Service Department at 724-873-8100 or fax to 724-873-8105, before sending in any module.

### 5.1 Module Replacement

Module replacement on the LX series products is a relatively simple process. All modules plug directly into the backplane board except for the power amplifier module, and in higher power units, the power supply and power amplifier modules, that plug into a blind mating connector. To replace a module, refer to the following procedure.

Loosen the two grip lock connectors, located on the front panel, at the top and bottom of the module, counterclockwise until the module releases. The Modulator, IF Processor, Upconverter and Controller/Power Supply can then be gently pulled from the unit. There are two cables connected to the rear of the Power Amplifier Module in the exciter/amplifier chassis assembly. These two cables must first be removed before the PA module will slide out.

After removal of the failed module, slide the replacement module in place and make certain it connects to the backplane board. If the replacement module is a PA Module replace the two cables on the rear of the exciter/amplifier chassis assembly. If the replacement module does not slide in easily, verify it is properly aligned in the nylon tracks, located on both the top and bottom of the module.

Note: Each Module has an assigned slot and will not fit properly in the incorrect slot. Do not try to place a Module in the wrong slot as this may damage the slot or the connectors on the backplane board.

Each module has the name of the module on the front, bottom for identification and correct placement. The Modules are placed in the unit from left to right; (1) Blank panel, (2) Modulator (for analog transmitters) or a Blank panel for a Translator or digital transmitter, (3) IF Processor, (4) Upconverter, (5) Controller/Power Supply and (6) Power Amplifier.

### 5.1.1 I nitial Test Set Up

Check that the RF output at the coupler is terminated into a dummy load of at least 100 watts. While performing the alignment, refer to the Test Data Sheet for the transmitter and compare the final readings from the factory with the readings on each of the modules. The readings should be very similar. If a reading is way off, the problem is likely to be in that module.

Switch On the main AC for the system.

### 5.2 LX Series Exciter/ Amplifier Chassis Assembly

This transmitter operates using the baseband audio and video inputs or, if the (optional) $4.5-\mathrm{MHz}$ composite input kit is purchased, either a single composite video $+4.5-\mathrm{MHz}$ input or separate baseband video and audio inputs.

On the LCD Display, located on the Controller/Power Supply Module, in Transmitter Set-Up, push the button to switch the transmitter to Operate. The check of and the setup of the Audio and Video input levels are completed using the LCD Display and the front panel adjustments on the Modulator assembly. The level of the RF output includes adjustments of the drive level to the Power Amplifier and the adjustment of the linearity and phase predistortion to compensate for any nonlinear response of the Power Amplifier. The adjustments are located on the front panel of the IF Processor module.

## Modulator Module Assembly

NOTE: Not present in a Translator systems.

The Modulator Assembly has adjustments for video levels and audio modulation levels, and other related parameters.

Connect an NTSC baseband video test signal input ( $1 \mathrm{Vpk}-\mathrm{pk}$ ) to the transmitter video input jack J7 on the rear of the tray. Jacks J7 and J 17 are loop-through connected; the J 17 jack can be used as a video source for another transmitter. Connect a baseband audio input ( +10 dBm ) to the balanced audio input terminal block TB02-1 [+], TB02-2 [-], and TB02-3 [ground] or, if stereo/composite audio is provided, connect it to BNC jack J3, the composite audio input jack.

Verify that all LEDs located on the front panel of the Modulator are Green. The
following details the meaning of each LED:

AURAL UNLOCK (DS5) - Red Indicates that 4.5 MHz Aural IF is unlocked from the Nominal 45.75 MHz visual IF.

VISUAL UNLOCK (DS6) - Red Indicates that the Nominal 45.75 MHz visual IF is unlocked from the 10 MHz reference.

AUDIO OVER DEVIATION (DS4) - Red Indicates that the input Audio level is too high. ( $\pm 75 \mathrm{kHz}$ max)

VIDEO LOSS (DS1) - Red Indicates that the input Video level is too Iow.

OVER MODULATION (DS3) - Red Indicates that the input Video level is too high.

ALTERNATE IF (DS7) - Red Indicates that an external Nominal 45.75 MHz IF is not present to the modulator.

10 MHz PRESENT (DS2) - Red Indicates that an external 10 MHz reference is not present to the modulator.

Look at the front panel LCD meter on the Control/Power Supply Module Assembly. Set the LCD screen to the Modulator Details video output level screen, the screen indicates active video from 0 to 1 Vpk-pk. The normal video input level is 1 Vpk-pk on the front panel screen. If this reading is not at the proper level, the overall video level can be changed by adjusting the VIDEO LEVEL control R42 on the front panel of the Modulator to the 1 Vpk-pk level on the front panel screen.

NOTE: An NTSC or FCC composite signal should be used for video metering calibration.

Switch the LCD display to the Modulator Details screen that indicates the AUDIO DEVIATION (modulation level) of the signal up to 75 kHz .

MONO SET UP: The modulator was factory set for a $\pm 25-\mathrm{kHz}$ deviation with a mono, balanced, audio input of +10 dBm . If the reading is not at the correct level, adjust the MONO Audio Gain pot R110, located on the front panel of the modulator, as necessary, to attain the $\pm 25-\mathrm{kHz}$ deviation on the front panel screen.

STEREO SET UP: The modulator was factory set for a $\pm 75-\mathrm{kHz}$ deviation with a stereo, composite, audio input of 1 Vpk-pk. If this reading is not correct, adjust the STEREO Audio Gain pot R132, located on the front panel of the modulator, as necessary, for the $\pm 75$ kHz deviation.

## SECONDARY AUDI O SET UP: NOTE:

Remove any stereo or mono audio modulation input to the transmitter during the set up of the secondary audio. The modulator was factory set for a $\pm 15$ kHz deviation with a secondary audio input of 1 Vpk -pk. If this reading is not correct, adjust the SAP/PRO Audio Gain pot R150, located on the front panel of the modulator, as necessary, for the $\pm 15-\mathrm{kHz}$ deviation.

## IF Processor Module Assembly

Verify that all red LEDs located on the IF Processor front panel are extinguished. The following details the meaning of each LED when illuminated:

- DS1 (input fault) - Indicates that either abnormally low or no IF is present at the input of the IF Processor module.
- DS2 (ALC fault) - Indicates that the ALC circuit is unable to maintain the signal level requested by the ALC reference. This is normally due to excessive attenuation in the linearity signal path or the IF phase corrector signal path, or that switch SW1 is in the Manual ALC Gain position.
- DS4 (Mute) - Indicates that a Mute command is present to the system.

Switch the transmitter to Standby. The ALC is muted when the transmitter is in Standby. To monitor the ALC, preset R3, the manual gain adjust pot, located on the front panel of the Upconverter module, fully CCW. Move switch SW1, Auto/Man AGC, on the front panel of the Upconverter module, to the Manual position. Place the transmitter in Operate. Adjust the ALC GAIN pot on the front panel of the IF Processor to obtain 100\% output power on the LCD Display mounted on the Controller/Power Supply in the ALC screen. Move the MAN/AUTO ALC switch back to Auto, which is the normal operating position.

To adjust the AGC Cutback setting, raise the output power of the transmitter to $120 \%$. Adjust R2, AGC Cutback, located on the front panel, CCW until the LED DS1, AGC Cutback, just starts to flash. Return the output power of the transmitter to $100 \%$.

### 5.2.1 Linearity Correction Adjustment

As shipped, the exciter was preset to include amplitude and phase predistortion. The pre-distortion was adjusted to approximately compensate the corresponding non-linear distortions of the Power Amplifier.

NOTE: On the IF processor board inside the module the correction enable/disable jumper W12 on J 30 will be in the Enable position, on pins $2 \& 3$.

Set up a spectrum analyzer with 100 kHz resolution bandwidth and 100 kHz video bandwidth to monitor the intermodulation products of the RF output signal of the Power Amplifier.

A typical red field spectrum is shown in Figure 5-1. There are three Linearity Corrector stage adjustments located on the front panel of the IF Processor

Module. The adjustments are threshold settings that are adjusted as needed to correct for any amplitude or phase intermod problems. Adjust the top linearity correction adjustment R211 threshold cut in for the in phase amplitude distortion pre-correction that is needed. Next adjust the middle linearity correction adjustment R216 threshold cut in also for the in phase amplitude distortion pre-correction that is needed. Finally adjust the bottom
linearity correction adjustment R231 threshold cut in for the quadrature phase distortion pre-correction that is needed. The above pots are adjusted for the greatest separation between the peak visual carrier and the intermod products. NOTE: These pots affect many other video parameters, so care should be taken when adjusting the linearity correction.


Figure 5-1. Typical Red Field Spectrum

### 5.2.2 Frequency Response Delay Equalization Adjustment

The procedure for performing a frequency response delay equalization adjustment for the transmitter is done at IF and is described in the following steps:

The center frequency for the first stage is 45 MHz . Adjust R103, the top frequency response equalizer pot, located on the front panel of the IF Processor Module, for the best depth of frequency response correction at 45 MHz .

The center frequency for the second stage is 42 MHz . Adjust R106, the middle frequency response equalizer pot, located on the front panel of the IF Processor Module, for the best depth of frequency response correction at 42 MHz .

The center frequency for the second stage is 43.5 MHz . Adjust R274, the
bottom frequency response equalizer pot, located on the front panel of the IF Processor Module, for the best depth of frequency response correction at 43.5 MHz.

After the three delay attenuation equalizers have been adjusted, fine tune, as needed, for the best frequency response across the channel.

### 5.2.3 Calibration of Output Power and Reflected Power of the transmitter

## Note: Perform the following procedure only if the power calibration is suspect.

Switch the transmitter to Standby and place the Upconverter into Manual Gain. Preset R205, the aural null pot on the Amp Control board, fully CCW. Adjust R204, the null offset pot on the Amp

Control board, for 0\% visual output. Perform the following adjustments with no aural present by removing the aural IF carrier jumper on the back of the chassis assembly. Connect a sync and black test signal to the video input jack of the test modulator. Switch the transmitter to Operate.

Next, set up the transmitter for the appropriate average output power level:

Example is for 100 Watt Transmitter.

- Sync + black 0 IRE
setup/ wattmeter=59.5 watts
- Sync + black 7.5 IRE
setup/ wattmeter=54.5 watts


## Note: The transmitter must have 40 IRE units of sync.

Adjust R202, visual calibration, on the Amp Control board for $100 \%$ on the front panel LCD display in the \% Visual Output position.

With the spectrum analyzer set to zero span mode, obtain a peak reference on the screen. Reconnect the aural carrier jumper on the rear of the chassis assembly. Turn the power adjust pot on the front panel until the original peak reference level is attained. Adjust R203 for a 100\% aural power reading. Switch to the Visual Output Power position and adjust R205 (aural null pot) for 100\% visual power.

To calibrate the reflected output power reading of the transmitter. Reduce manual gain pot R3 to a $10 \%$ reading on the LCD front panel display in the \% Output Power position. Place the transmitter in Standby. Remove the PA Module Sled. Remove the load from J4 on the (A4) Directional Coupler Board and switch the LCD Display screen to the Reflected Output Power position. Reinstall the PA Module. Switch the transmitter to operate. Adjust the reflected power calibration adjust pot

R163 on the power amplifier module to a $10 \%$ reading. A reflected power fault should be present on the LCD Display. Reconnect the load to J4 in the module.

After this calibration is completed, move switch SW1 on the upconverter module to the Automatic AGC position. This is the normal operating position for the switch. Adjust the ALC pot on the IF Processor is needed to attain 100\% output power. Switch to Manual Gain (Manual AGC) and adjust the Manual Gain pot for 100 \% output power. Switch the upconverter back to Automatic AGC.

The Transmitter is now aligned, calibrated, and ready for normal operation.

This completes the detailed alignment procedures for the LX Series transmitter.

If a problem occurred during the alignment, help can be found by calling Axcera field support at 724-873-8100.

### 5.3 Alignment Procedure for the Bandpass Filter Assembly

The Bandpass Filter Assembly is tuned to reject unwanted distortion products generated when the signals are diplexed and also during the amplification process.

The Bandpass Filter is factory tuned to the proper bandwidth and should not need tuned. If you think tuning is needed consult Axcera Field Support Department before beginning the adjustment.

The Traps are labeled with their Center Frequency relative to the Frequency of the Carrier. (For Example: The Traps labeled -4.5 MHz are tuned for a Center Frequency of 4.5 MHz Lower than the Frequency of the Visual Carrier.)

The Trap Sections are Reflective Notches, adjustable across the entire UHF
Frequency Band. The electrical length of
the Outer Sleeve and the Center Rod of the Notch can be adjusted to tune the Notch Frequency. The Depth of the Notch is set by the gap between the Center Conductor of the Trap Section and the Center Conductor of the Main Line. Tight Coupling makes a Deep Notch, while Loose Coupling makes a Shallow Notch.

NOTE: The Trap Sections have been factory tuned and should not need major adjustments. The Frequency, relative to Visual Carrier, that the Trap is tuned to is marked on the Notch. Fine Tuning of the Notches Center Frequency can be accomplished with the Tuning Bolts located on the side of the Filter Section. Loosen the nut locking the Bolt in place and adjust the Bolt to change the Frequency of the Notch. Monitor the output of the Transmitter with a Spectrum Analyzer and Null the Distortion Product with the Bolt.

Red Field is a good Video Test Signal to use to see the out-of-band Products. Tighten the nut when the tuning is completed. Hold the bolt in place with a screwdriver as the nut is tightened to prevent it from slipping.

For major tuning, such as changing the Notch Depth or moving the Notch Frequency more than 1 MHz , the Outer Conductor and the Center Conductor of the Trap Section must both be moved. This requires an RF Sweep Generator to accomplish. Apply the Sweep signal to the Input of the Trap Filter and monitor the Output. Loosen the Clamp holding the Outer Conductor in place and make the length longer to Lower the frequency of the Notch or shorter to Raise the frequency of the Notch. Loosen the

Center Conductor with an Allen Wrench and move it Deeper for a Lower Frequency Notch or out for a Higher Frequency Notch. These adjustments must both be made to change the Notch Frequency. Moving only the Center Conductor or the Outer Conductor will effect the Notch Depth in addition to the Center Frequency. The variable that is being adjusted with this procedure is the length of the Center Conductor inside the Trap Filter. The gap between the Trap and the Main Line should not be changed. Moving only the Inner or the Outer Conductors by itself will effect the Gap and the Notch depth.

To effect the Notch Depth Only, both sections will have to be moved. The Notch Depth is controlled by the Gap between the Center Conductor and the Trap Section. This Gap also has an effect on the Center Frequency. To Deepen the Notch, Shorten the Outer Conductor and pull the Center Conductor Out until the Notch is back in the same place. Move the Sections in the opposite direction to make a Shallow Notch.

After tuning has been completed, tighten the Clamp and the Allen Screws which hold the Conductors. Use the Fine Tuning Bolts to bring the Frequency In. The Final Tuning Adjustments should be completed with the Transmitter driving the Output Trap Filter for at least one hour to allow for warm-up drift.

This completes the Alignment Procedure for the Bandpass Filter Assembly and the exciter/amplifier assembly of the LX Series Transmitter.

## APPENDIX A

LX SERIES ANALOG SYSTEM SPECIFICATIONS


Designed to provide broadcasters with a product that will meet their needs like no other solution on the market, this new low to medium power transmitter line uses the latest LDMOS devices for broadband operation across the entire UHF band. This allows users to minimize spare parts stock, which is especially important to group owners and networks, and also enables simple and inexpensive channel changes.

The very compact and completely modular design uses a chassis/backplane configuration with parallel amplifier and power supply modules that can be removed and replaced while the transmitter is on the air. Additionally, the Innovator LX series was designed to be field upgradable to digital operation.

Configurations are available in power levels from 10 watts to 6 kilowatts analog and up to 3 kilowatts DTV, and all are manufactured in the USA by Axcera - The RF Experts.

## Low Power Transmitter 10W - 6kW

| Visual Performance |  |
| :---: | :---: |
| Frequency Range | 470 to 806 MHz |
| Carrier Stability (Transmitters) <br> Standard <br> Optional <br> w/PFC | $\begin{aligned} & \pm 1 \mathrm{kHz} \\ & \pm 350 \mathrm{~Hz} \\ & \pm 1 \mathrm{~Hz} \end{aligned}$ |
| Frequency Translation Stability ( <br> Standard <br> Optional <br> w/PFC | $\begin{aligned} & \text { ators) } \\ & \pm 1 \mathrm{kHz} \\ & \pm 350 \mathrm{~Hz} \\ & \pm 1 \mathrm{~Hz} \end{aligned}$ |
| Regulation of RF Output Power | 3\% |
| Output Variation (Over 1 Frame) | 2\% |
| Sideband Response |  |
| $\begin{aligned} & -1.25 \mathrm{MHz} \text { and below } \\ & -0.75 \text { to }-0.5 \mathrm{MHz} \\ & -0.5 \text { to }+3.58 \mathrm{MHz} \\ & +3.58 \mathrm{MHz} \text { to }+4.18 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} & -20 \mathrm{~dB} \\ & +0.5 \mathrm{db},-2 \mathrm{~dB} \\ & \pm 0.5 \mathrm{~dB} \\ & +0.5,-1.0 \mathrm{~dB} \end{aligned}$ |
| Freq Response vs. Brightness | $\pm 0.5 \mathrm{~dB}$ |
| Visual Modulation Capability | 1\% |
| Differential Gain | 5\% |
| Incidental Phase Modulation | $\pm 3^{\circ}$ |
| Linearity (Low Frequency) | 5\% |


| Visual Performance (continued) |  |
| :--- | :--- |
| Differential Phase | $\pm 3^{\circ}$ |
| Signal-to-Noise Ratio | 55 dB |
| 2t K-Factor | $2 \%$ |
| Noise Factor (Translators) | 5 dB (Max) |
| w/Input Preamp | 3 dB (Max) |
| Input Dynamic Range (Translators) | -60 dB to |
|  | -15 dBm |
| w/Input Preamp | -75 dBm |
|  | to -30 dBm |
| Env. Delay (Transmitters) | Per FCC Standard |
| Video Input (Transmitters) | 75 ohms |
|  | (Loop through) |
| Harmonics | -60 dB or better |
| Intermodulation Products | -52 dB or better |
| Spurious (.3 MHz from channel edge) |  |
| 100W and lower | -50 dB or better |
| Greater than 100W | -60 dB or better |

## Aural Performance

| Frequency Deviation Capability | $\pm 75 \mathrm{kHz}$ |
| :--- | :--- |
| (Transmitters) |  |
| Distortion | $0.5 \%$ |
| FM Noise | -60 dB |
| AM Noise | -55 dB |
| Aural to Visual Separation | 4.5 MHz |
|  | $\pm 100 \mathrm{~Hz}$ |

Composite Audio Input (Multi-channel sound)
(Transmitters)
$\begin{array}{ll}\text { Input Level } & 1 \mathrm{~V} \text { peak, } \\ & \text { nominal }\end{array}$

| Input Impedance | nominal <br> 75 ohms, <br> unbalanced |
| :--- | :--- |
| Frequency Range |  |


| Frequency Range |  |
| :--- | :--- |
| $\pm 0.1 \mathrm{~dB}$ response | 50 Hz to 50 kHz |
| $\pm 0.5 \mathrm{~dB}$ response | 30 Hz to 120 kHz |



| Input | 600 ohms, |
| :--- | :--- |
| balanced |  |
| Freq Range ( $\pm 0.5 \mathrm{~dB}$ resp. $)$ | 30 Hz to 15 kHz |

Pre-emphasis $75 \mu \mathrm{~s}$
Subcarrier Input (Transmitters)
Input Level
nominal
75 ohms, unbalanced 20 kHz to 120 kHz

## General

| Model Number* | LU10Ax | LU100Ax | LU250Ax | LU500Ax | LU1000Ax | LU2000Ax | LU3000Ax | LU4000Ax | LU5000Ax | LU6000Ax |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Power Output (Watts) |  |  |  |  |  |  |  |  |  |  |
| Visual (Peak) | 10 | 100 | 250 | 500 | 1000 | 2000 | 3000 | 4000 | 5000 | 6000 |
| Aural (Avg.) | 1 | 10 | 25 | 50 | 100 | 200 | 300 | 400 | 500 | 600 |
| Output Connector Power Consumption (Watts) | $\begin{aligned} & N \\ & 250 \end{aligned}$ | $\begin{aligned} & N \\ & 675 \end{aligned}$ | $\begin{aligned} & 7 /{ }^{7} \text { EIA } \\ & 1100 \end{aligned}$ | $\begin{aligned} & 7 / 8^{\prime \prime} \text { EIA } \\ & 1900 \end{aligned}$ | $\begin{aligned} & 7 / 8 "^{" E I A} \\ & 3500 \end{aligned}$ | $\begin{aligned} & 7 / 8{ }^{" E I A} \\ & 6700 \end{aligned}$ | $\begin{aligned} & 31 / 8 " \text { EIA } \\ & 10,250 \end{aligned}$ | $\begin{aligned} & 31 /{ }^{2 n} \mathrm{EIA} \\ & 13,500 \end{aligned}$ | $\begin{aligned} & 31 / 8 " \text { EIA } \\ & 16,700 \end{aligned}$ | $\begin{aligned} & 31 / 8_{8} \text { EIA } \\ & 19,900 \end{aligned}$ |
| Input Power |  |  |  |  |  |  |  |  |  |  |
| Line Voltage (Volts) | $117 / 230 \pm 10 \%$ |  | $230 \pm 10 \%$ |  |  |  |  |  |  |  |
| Power Requirements | Single Phase, 50 or 60 Hz |  |  |  |  |  |  |  |  |  |
| Size ( $H \times W \times D$ ) | $8.75 " \times 19^{\prime \prime} \times 23^{\prime \prime}$ <br> (Chassis Only) |  | $55^{\prime \prime} \times 22$ " $\times 34$ " |  |  |  | $76 " \times 22$ " 34 " | $76 " \times 44$ " $\times 34$ " |  |  |
| Weight (lbs.) | 45 | 45 | 340 | 360 | 400 | 550 | 700 | 1030 | 1180 | 1330 |
| Operational Temperature Range | 0 to $+50^{\circ}$, derate $2^{\circ} \mathrm{C} / 1000 \mathrm{ft}$. |  |  |  |  |  |  |  |  |  |
| Maximum Altitude ${ }^{3}$ | 8500 feet ( 2600 m ) AMSL |  |  |  |  |  |  |  |  |  |
| Operational Humidity Range | 0\% to 95\% non-condensing |  |  |  |  |  |  |  |  |  |
| RF Load Impedance | $50 \Omega$ |  |  |  |  |  |  |  |  |  |

* For transmitters use "T" suffix, translators use "L" suffix (ex. LU100AT-100W Transmitter)

Specifications published here are current as of the date of publication of this document. Because we are continuously improving our products, Axcera reserves the right to change specifications without prior notice. At any time, you may verify product specifications by contacting our office. Axcera views it's patent portfolio as an important corporate asset and vigorously enforces its patents. Products or features contained herein may be covered by one or more U.S. or foreign patents.

## APPENDIX B

DRAWINGS AND PARTS LISTS
Innovator LX Series Analog System
LX Series 10W to 100W System Block Diagram ..... 1302139
Chassis Assembly, 110 VAC Exciter, LX Series Interconnect ..... 1303108
OR Chassis Assembly, 220 VAC Exciter, LX Series
Interconnect ..... 1303108
Backplane Board, LX Series
Schematic ..... 1301995
Modulator Assembly, M/ N - 1301929 (Not present in Translator Systems)
Assembly consists of:
Analog Modulator Board, System M/N Schematic ..... 1301798
IF Processor Assembly - 1301938Assembly consists of:
IF Processor Board
Schematic ..... 1301983
Upconverter Assembly, Analog - 1302060
Interconnect ..... 1302060
Assembly consists of:
Front Panel LED Display Board
Schematic ..... 1303035
UHF Filter
Schematic ..... 1007-3101
UHF Generator Board
Schematic ..... 1585-3265
L.O./Upconverter Board Schematic ..... 1302134
Control/ Power Supply Assembly - 1301936 , 110 VAC Interconnect ..... 1302062
OR Control/ Power Supply Assembly - 1303229, 220 VAC Interconnect ..... 1302062
Assembly consists of:
Control Board
Schematic ..... 1302023
Power Protection Board
Schematic ..... 1302839
Switch Board
Schematic ..... 1527-3406
Power Amplifier Assembly - 1301923
Interconnect ..... 1302061
OR Driver Amplifier Assembly, (Used in High Power Systems)
Interconnect ..... 1303452
Assembly consists of:
Coupler Board Assembly Schematic ..... 1303152
Amplifier Control Board Schematic ..... 1301964
1 Watt Module AssemblyContains a 1 Watt UHF Amplifier Board (1302761).
1 Watt UHF Amplifier Board Schematic ..... 1302762
TFS 40W UHF Module, TestedMade from a TFS 40W UHF Module, Stork (51-5379-308-00).
TFS 40W UHF Module, Stork
Schematic. ..... 51-5379-308-00 WSP
RF Module Pallet, PhilipsMade from a RF Module Pallet w/o Transistors (1152336).
RF Module Pallet w/o Transistors Schematic 51-5379-309-00 WSP


[^0]:    U23 and U24 are low drop out +5 VDC, voltage regulators with a tolerance greater

