

# Practical Tips on Making “Vector Voltmeter (VVM)” Phase Measurements using VNA Master (Option 15)

## Introduction

**VOR-DME.** RF cable matching is a critical, yet common measurement in the construction and maintenance of air navigation antenna systems like VHF Omnidirectional Range (VOR) antenna clusters and Instrument Landing Systems (ILS). Both of these systems are used at the nation’s airports and in travel corridors for airline routes. The VOR system (conventional) features a four-antenna “Alford Loop” antenna system that is topped by individual monitoring elements around a full 360 degrees. This allows aircraft to receive a signal in any direction from the station beacon (Figure 1a).

Using a different radiation technique, the Doppler VOR uses signal phase shifting to create its signal (Figure 1b). This angle-sensitive signal provides the azimuth angle from the beacon to the aircraft, and is displayed in the cockpit.

Distance from the beacon is determined by a co-located transponder-based system (Distance Measuring Equipment) using a pulsed-pair signal in the 1000 MHz band.



Figure 1a.



Figure 1b.

Figure 1. These two formats of VOR are recognized as the classical navigation beacons for airplane location. They are characterized by multiple radiation elements, which require precise phase measurements for signal cables on installation and maintenance.

**ILS.** The ILS navigation technique consists of two independent sub-systems. One provides lateral guidance in the 108 - 112 MHz band (Localizer), while the other provides vertical guidance in the 329 - 336 MHz band (Glideslope or GlidePath) to aircraft approaching a runway (Figure 2).

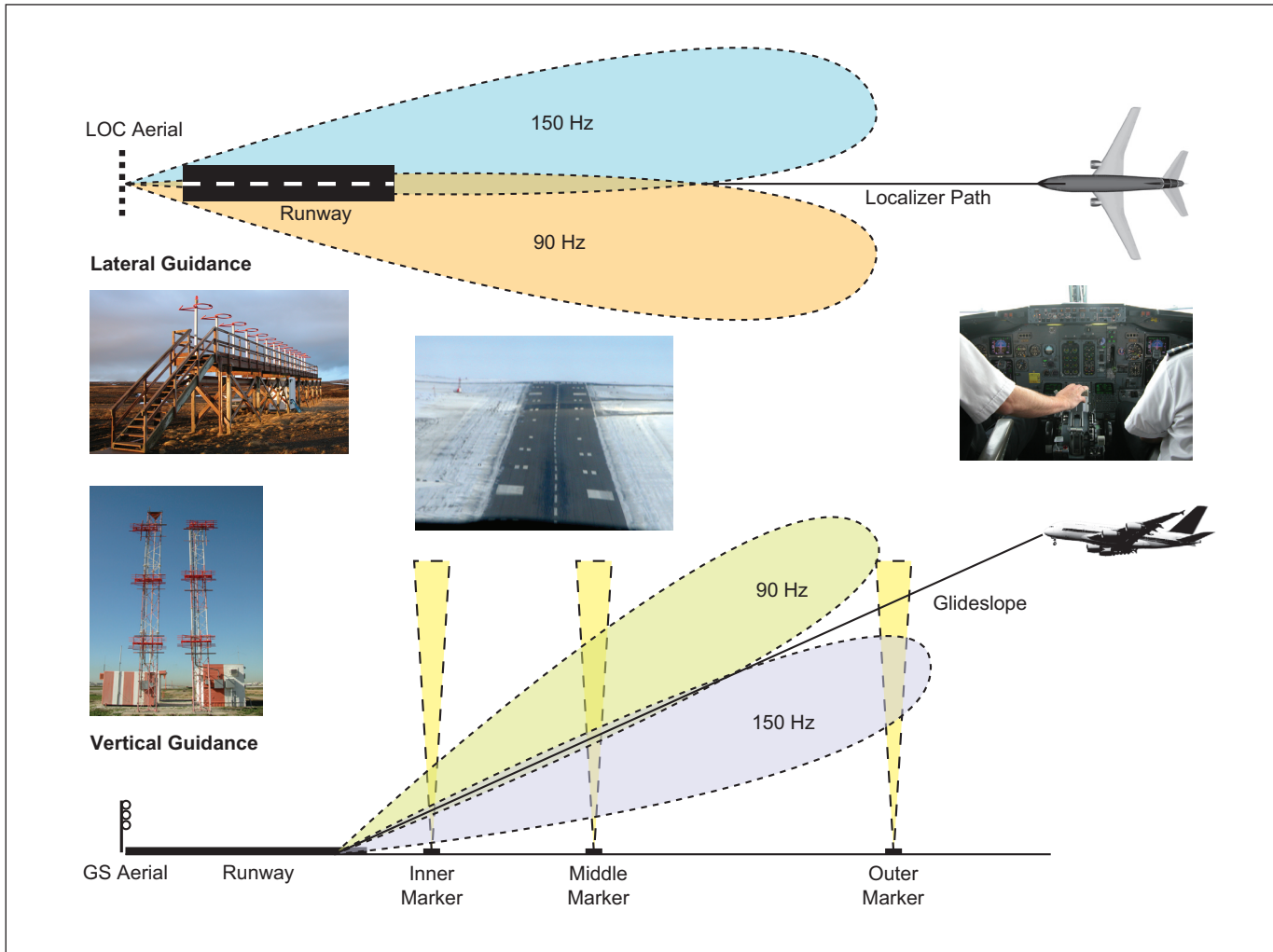


Figure 2. The ILS shown here is the close-in navigation aid which displays an aircraft's deviation from the proper glide path, both laterally and vertically. During approach, the pilot can optimize descent for landing using feedback from the ILS elements deployed toward the end of the runway.

In both applications, it is important for the antenna signal cables to have the same electrical, as well as mechanical length. At the core of these types of systems is a signal distribution center that protects critical interconnects while offering access for installation and maintenance activities (Figure 3). Measuring the cables' characteristics (e.g., phase length and insertion loss) is therefore essential to proper performance and the safety of the air-travel industry.

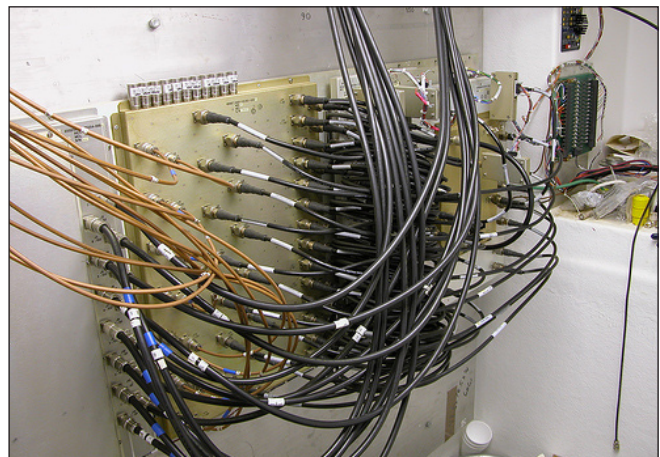


Figure 3. A maze of precise-length signal cables are required to feed the antenna elements with individual signals of the proper phase.

Traditionally, the technician or RF engineer would accomplish this task using a Vector Voltmeter (VVM) measurement system, but today these instruments are obsolete and their functionality has been replaced by the modern vector network analyzer (VNA). These powerful measurement tools not only measure raw vector (amplitude and phase) data, but also invoke sophisticated calibration/correction routines which are handled by internal software to enhance the resulting data for excellent accuracy. In addition, unlike the VVM that required an external signal generator, modern VNAs feature a built-in signal source, which lends convenience to remote field operations.

This application note focuses on cable-phase measurement procedures for applications requiring absolute phase shift at a particular frequency. It also treats the common measurement routines where many cables must be matched for identical phase shift versus frequency. Its objective is to present practical measurement tips and procedures that will help a technician or RF engineer conduct cable phase-characteristic measurements using the Anritsu VNA Master, Vector Voltmeter Option 15.

## **The Evolution of the VVM to Vector Network Analyzer**

The VVM is an instrument that was first introduced in the mid 1960s. It was designed with two basic functions in mind: to make RF circuit measurements utilizing a sampling probe containing a high-impedance probing function and to make coaxial network measurements working in 50-ohm transmission lines.

Those early commercial VVMs were based on what, at the time, was considered revolutionary new signal sampling technology. The idea was to drive a step-recovery diode with an RF local oscillator (LO), resulting in extremely narrow impulses of power at the LO frequency. According to mathematical theory, such impulses generate a wide frequency range of harmonics, almost flat with increasing frequency, to 1000 MHz and beyond. This concept was similar in principal to the technology employed in sampling oscilloscopes introduced in 1962, and quickly became the foundation of an innovative new future of RF and microwave instruments for measuring complex parameters.

While early attempts at network analysis with the VVM used a two probe/coax Tee arrangement on two opposing directional couplers and resulted in a reflectometer that worked from 10 MHz to 1 GHz, such functionality came at the price of considerable manual effort. The two RF voltages and the phase angle between the forward and reflected signals had to be recorded by hand, and the unknown impedance (Smith Chart) calculated and plotted laboriously. Despite this limitation, the VVM with its amplitude and phase-ratio measurements enabled a significant work increase over VHF bridges and other such slow and inaccurate equipment.

By the late 1960s, the VVM's network measurement ratio function was taken over by full-fledged microwave network analyzers that went far higher in frequency, to 12 GHz and above. In the decades since, the VVM has generally been used for the direct measurement of RF phase angles in transmission lines—probing RF voltages (A and B) in two channels, and displaying A, B, A/B, B/A, and the phase difference between them. Over time, circuit probing for RF amplifiers and other VHF analog circuits declined as integrated circuits and digital technology took over many analog and RF voltage functions. Later versions of VVMs were introduced with additional features, but even those instruments have now been retired. Today, the functional RF ratio measurements that were once the mainstay of the VVM are performed by modern VNAs.

## Making Phase Cable Measurements in the Field

When equipped with the Vector Voltmeter Option 15, the Anritsu VNA Master is a convenient and accurate vector network analyzer for measuring absolute insertion-phase characteristics or comparing phase match between multiple RF cables. It is an especially useful tool in field test configurations, where access to AC power is typically limited. The VNA Master's Vector Voltmeter mode effectively replaces the functional ratio measurements of now obsolete vector voltmeters and the signal generator. However, it cannot be used to measure RF voltages, which of course, are not needed for determining phase shift.

When configured with VVM Option 15, the VNA Master provides detailed software routines and data displays for making phase-cable measurements. It contains its own built-in vector insertion loss and phase receiver, a wideband signal source and directional bridges/couplers—all configured internally—for conducting both 1-port and 2-port measurements at selected CW frequencies (Figures 4 and 5). Unlike VVMs with their 1000-MHz limit, the VNA Master with Option 15 measures cable characteristics to 4 GHz, 6 GHz, or 20 GHz (depending on model), making it a suitable replacement for the most used VVM ratio function—measuring component parameters.

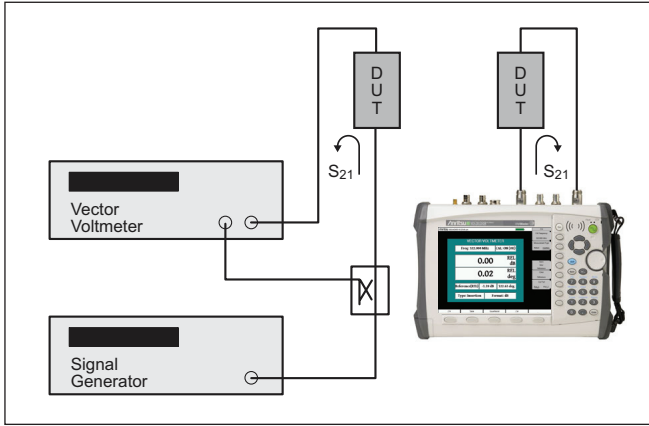


Figure 4. The biggest advantage of the VNA Master (on right) is that it self-contains the test signal source and directional devices to detect forward and reverse power. It requires no other external accessories so it is a much more convenient tool for field operation, especially considering that it is battery-powered for less reliance on AC power in remote environments.

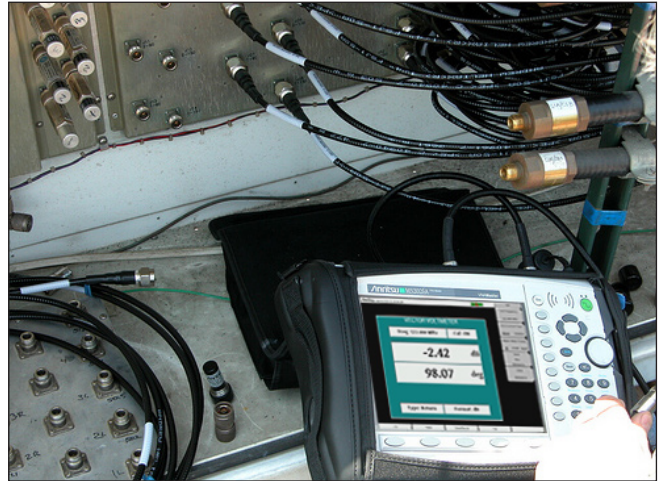


Figure 5. Compare this VNA Master footprint with previous VVM systems. As shown here, the portable size enables close-up access to help streamline installation and maintenance tasks for field personnel.

With the VNA Master, cable-phase measurements can be obtained by two different techniques, both based on the concept of scattering parameters. In any cable or component, there are four numerical quantities which describe the “transfer function” versus frequency (Figure 6). These are the four scattering parameters:  $S_{11}$ ,  $S_{22}$ ,  $S_{12}$ , and  $S_{21}$ .  $S_{11}$  is the reflection signal at port 1, and can come from a bad input connector or discontinuities along the cable, a pinched or knotted region, or a short or open load on the far end.  $S_{22}$  is likewise, the vector reflection from a signal input at port 2.  $S_{21}$  is the transmission characteristic for a signal entering port 1 and exiting at port 2.  $S_{12}$  is the transmission characteristic for a signal entering port 2 and exiting at port 1. Each of these four scattering parameters is a vector number and varies with frequency across the useful spectrum of the component or cable.

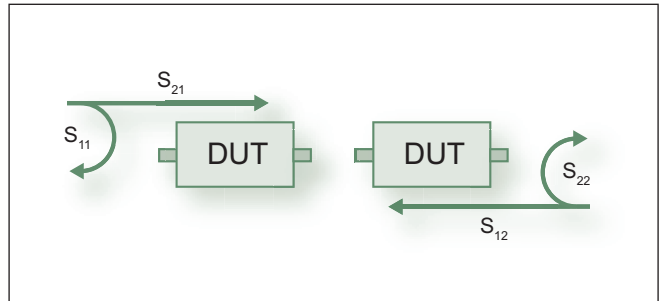


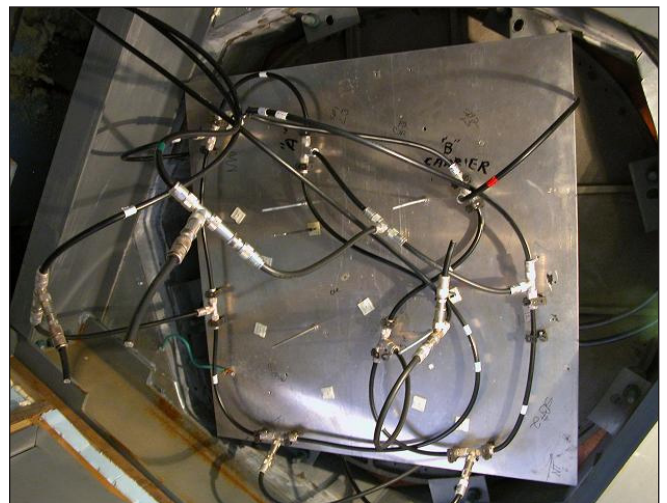
Figure 6. In this diagram, the four scattering parameters for a 2-port component or cable are defined. Each is a vector quantity and varies with frequency. On the left, the forward transmission from port 1 measures  $S_{11}$  and  $S_{21}$ . On the right, the reverse transmission from port 2 measures  $S_{22}$  and  $S_{12}$ . Each of these four S-parameters has both magnitude and phase terms that can be displayed in a variety of popular trace formats.

The two techniques used by the VNA Master to obtain cable-phase measurements are:

1. Insertion technique. This technique utilizes the VNA Master's 2-port setup to make cable-phase measurements and is generally considered the preferred technique. It characterizes the insertion phase delay of a signal by measuring  $S_{21}$  through the cable. This allows the operator to determine the phase shift of the component or cable from input connector to output connector. Measured  $S_{21}$  data is displayed as insertion loss in dB, while insertion phase is displayed in degrees.
2. Reflection technique. This technique measures the  $S_{11}$  reflected signal on a component or cable, and is dependent on the far end of the cable being deliberately mismatched—either shorted or left as an open circuit. With the mismatch, virtually 100 percent of the input signal is reflected and as a result, the phase delay of the measured reflected signal is equal to twice the one-way phase of the cable. Likewise, the cable measured return loss is twice the one-way loss.

The reflection technique is especially useful for situations where the operator must manually create multiple phase-matched cables using the “measure-and-snip” operation. This operation requires the engineer or technician to carefully snip small amounts of cable with a diagonal cutter, perhaps 1/8th inch at a time, and re-measure the effect on the 2-way phase.

As an example, in one specific VOR system program, a special and detailed instruction set describes the step-by-step procedures needed to create phase-matched cables, either with standard RG-214 coax cable or with 1/4 inch Andrew Heliax® (solid outside conductor) coaxial transmission line. The conditions are strict since matching is needed for the cable-phase measurements to within +/-0.2 degrees at the VOR system frequencies in the 108 to 118-MHz range. For reference, at 108 MHz, 1.0 inches of the RG-214 coaxial cable equals 4.99 degrees, varying with frequency, of course, and going to 5.45 degrees at 118 MHz (Figure 7).



*Figure 7. Typical cabling installation in a VOR system is shown here. The system uses RG-214/U type coax and signal splitter/combiner components. Critical phase-matching requirements ensure the overall system operates correctly as a navigational aid for aircraft.*

## Two-Port VVM Measurements

With the VNA Master, Option 15, operators can make cable-phase measurements using the insertion technique previously described. Prior to conducting a 2-port measurement (S21) in VVM mode, the VNA Master must be calibrated (Figure 8). To begin, select a continuous wave (CW) frequency and choose 2-port calibration. When making a 2-port connection to the device under test (DUT), select the insertion measurement type and then perform a 2-port calibration. For specific details on the 2-port calibration procedure, refer to the *VNA Master User Guide*.

The process of calibration establishes a reference plane for subsequent measurements by using open, short, load, and through standards (also known as SOLT calibration, Figure 9). The standard process involves connecting these calibration components as prompted by the VNA Master. After calibration, the VNA Master is ready to conduct phase-matching measurements.

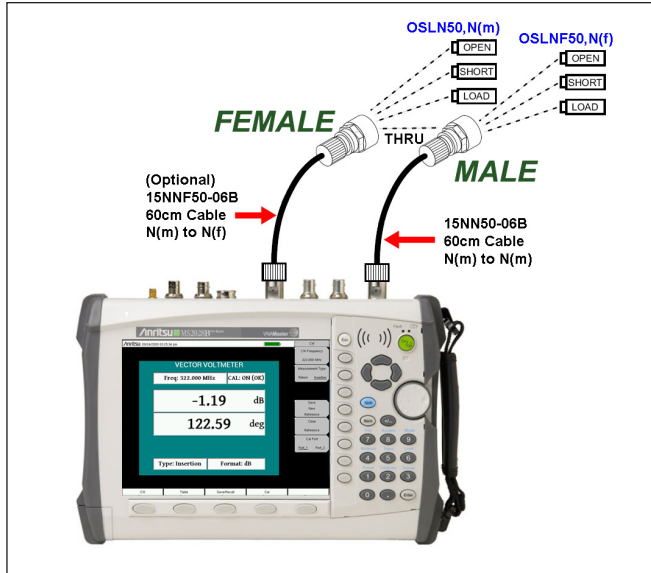


Figure 8. VNA Master's calibration procedures provide the zero-phase reference for later insertion-phase measurements. The calibration algorithm requires a through connection so it is important to set up a male-female interconnect scheme to ensure a precise zero-phase reference.



Figure 9. Convenient calibration artifacts (e.g., N and K) are available for the VNA Master Option 15, to provide the open, short and load standards for the calibration procedure.

## Phase Matching Cables

In preparation for installation, the time-consuming cable fabrication process is performed (Figure 10). When fabricating cables with precise phase requirements, system users will likely have their own recommended procedures. For federal antenna installations, for example, there are detailed instructions for the fabrication and measurement procedures. Nevertheless, a good general procedure is as follows:

1. Connectorize the first (reference) cable on both ends.
2. Make an insertion phase measurement and store the data.
3. Cut a second cable to length, being careful not to cut shorter than the reference cable, and connectorize it on both ends.
4. Measure the second connectorized cable and compare it to the first (reference) cable.



Figure 10. This system installation is configured with solid outer conductor cables. Maintenance activities are usually scheduled to avoid peak operational periods.

From the difference observed, it is possible to “guesstimate” how much the second cable needs to be trimmed, but the remove/trim operation is often not that precise. In order to trim, one of the second cable’s connectors is removed and the center conductor is trimmed. The connector is then re-connected on the second cable for another measured comparison with the first cable. While it may be difficult to trim the cable correctly the first time, experienced users often achieve success in the first two or three tries.

The measure-and-cut practices vary with frequency. Lower frequencies (VHF) will likely be in the 1/16th- to 1/8th-inch range for final iterations. At 1 GHz and above, the re-connecting might only involve unsoldering the center conductor, moving it 1/32th inch or less, and just letting the solder cool. For example, at 118.5 MHz, 1.0 inch of 1/4th inch Andrew Heliax with a  $V_p = 0.84$ , equals approximately 4.28 degrees, while at 332.3 MHz, it equals 12.05 degrees. Often times, those last few tenths of a degree involved with getting the cable trimmed “just right” can become very frustrating. With careful and clever attention to detail and data, users can establish their own learning curve.

Once the 2-port measurements have been made, measured data appears in a display window similar to that shown in Figure 11.

### Relative Phase Measurements

A key advantage of the VNA Master’s computational power is that it can store a measurement from a master cable or component—what some refer to as “gold standards”—and make further measurements on other similar cables to determine the consistency of the cables to one another. Measurement results can be displayed using VNA Master’s CW display. More information on this procedure is detailed in the *VNA Master Option 15 User Guide*.

As an example, consider Figure 12. Here, the VNA Master Vector Voltmeter mode saves the current cable measurement in a new reference window and converts the main measurement window to display the **difference** between the current measurement and saved reference. Saving a reference normalizes the results to the current measurement. When **relative** measurements for the second unit are displayed, REL is indicated in the main measurement window. Note that the original reference measurement is also displayed on the bottom of the screen.

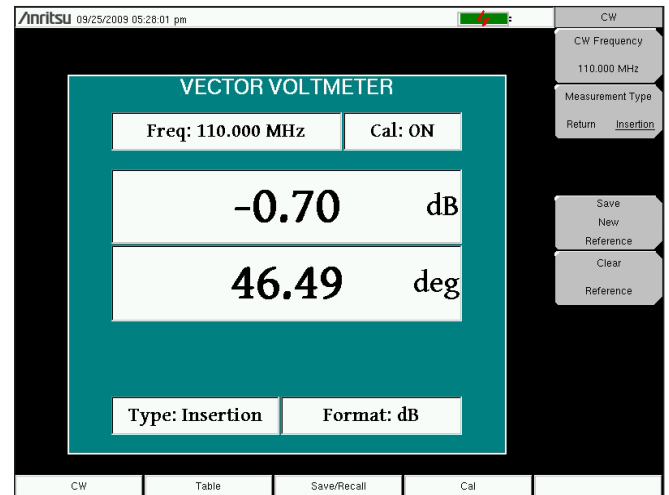


Figure 11. The VNA Master’s VVM display shows the insertion signal loss (-0.70 dB) and phase shift (46.49 deg) for the test frequency of 110 MHz. These quantities are derived from the VNA Master’s measurement of  $S_{21}$ .

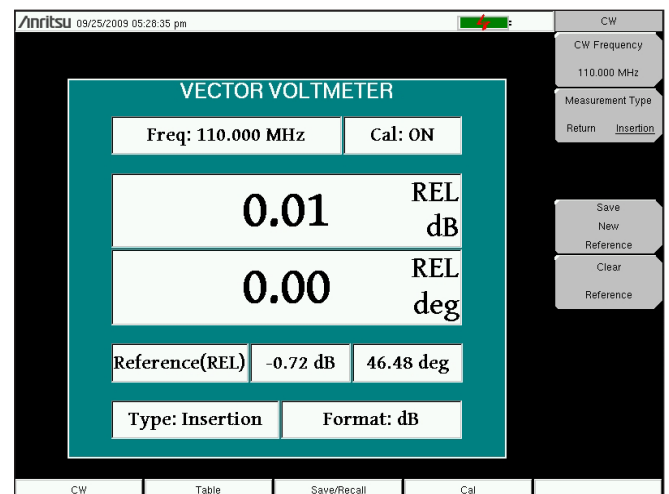


Figure 12. Comparing cable parameters on phase and insertion loss is easy, as shown on this VVM display, with the relative differences in the middle and the original parameter values (gold standard unit) in the lower portion of the screen. The two cables are more phase matched as the relative difference between them becomes smaller.

## One-Port VVM Measurements

With the VNA Master, Option 15, operators can also make cable-phase measurements using a reflection technique. These 1-port measurements are most convenient in cases where “measure-and-snip” operations must be performed to create cables of exactly the right phase length for a prescribed frequency. One-port measurements are possible because the open end of the cable under test forms an almost 100 percent reflection at VHF frequencies. In the standard view, the display will show twice the one-way phase of the cable (likewise, the cable attenuation is twice the one-way loss), but this can be a convenient approach when access to both ends of the cable is not possible. In the relative view, the display will show the proper differences between the two cables. Attention is needed when fabricating cables since the trimming effects are more pronounced given the round-trip aspect of this setup.

Similarly, calibration is required prior to making any 1-port measurements. The 1-port calibration procedure uses simple Open, Short and Load standard artifacts as shown in Figure 13 to establish the zero-phase reference. For specific details on the 1-port calibration procedure, refer to the *VNA Master Option 15 User Guide*.

When using the 1-port technique to measure a cable's phase length, it must be assumed that the raw end of the cable reflects back all the power. An open coaxial cable end will reflect most of the power back, but it sometimes can function as a non-efficient antenna at microwave frequencies, leaking a small amount of power and therefore not achieving 100 percent reflection—a condition dependent on frequency. For VHF frequencies in the 100- to 500-MHz range, for example, an open end has almost perfect reflection.

The VNA Master Option 15 is capable of measurements up to 4 GHz, 6 GHz, or 20 GHz (depending on model). At these higher microwave ranges, users are advised to prepare the cable center conductor and braided shield to be electrically shorted, such as by soldering the two together to ensure a good short. This extra soldering step complicates the “measure-and-snip” technique since once the required phase is obtained by multiple snips, the final addition of the real connector starts with a slightly damaged cable end. Yet, with a little experience, the user will find the effect of those last several 1/16th inch snips can be understood as the process goes on.

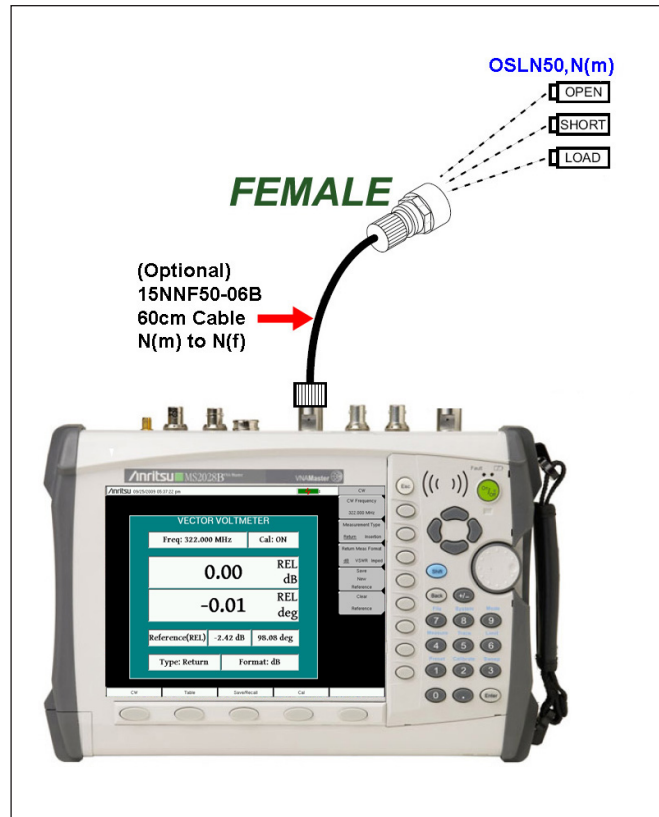


Figure 13. The 1-port VVM measurement procedures are preferred for cable measurements when access to both ends of the cable are limited. In this case, the absolute attenuation and phase are twice the one-way trips on the cable. Prior to making these measurements, the VNA Master must be calibrated for 1-port measurements using the setup pictured here.



## Measurement/Cable-Snipping Tips

While interactively measuring and snipping cables for matched phase is a tedious job, made faster only by experience, a number of tips can help with this task. Two such tips are:

- Tip 1. At any one frequency, cut the cable to be prepared several inches longer than the final length. Solder the raw end, creating a good short and take a measurement. Next, cut off exactly one inch of cable, solder it identically again and take another measurement. Note the change in phase from the removal of the one inch segment and calculate the amount of phase difference for, say, 1/8th inch. When the snip procedure gets near to the final desired value of measured phase, the user will now have a predicted mental picture of how much to snip.
- Tip 2. The procedure in Tip 1 can also be run by the operator. Using the 1-port method, make a shorted-end phase measurement and note the value. Attach the final cable connector at that length using the normal connector attaching process. Next, make a 2-port connector-to-connector insertion phase measurement, as described above, and record the difference in phase. This correction value can be utilized in later steps when converting from the raw end measurements to the final connectorized configuration.

## Displaying Measured Data

The VNA Master Option 15 display includes a convenient table for comparing multiple cables. With this feature, the user can save the first cable measurement as a reference, view the differences between the reference cable and other cables, and then output a final report showing both absolute and relative values of all cables. As an example, Figure 14 shows a display table with measured values of phase and attenuation for each cable. Their relative phase and amplitude, with respect to a chosen “golden standard cable,” is shown in the top box as the REL standard.

Freq: 322.000 MHz		CAL: ON (OK)		
Reference(REL)		-1.19 dB      122.63 deg		
Cable	Amp	REL Amp	Phase	REL Phase
1	-1.75 dB	-0.56 dB	-161.14 deg	76.23 deg
2	0.00 dB	0.00 dB	0.00 deg	0.00 deg
3	0.00 dB	0.00 dB	0.00 deg	0.00 deg
4	0.00 dB	0.00 dB	0.00 deg	0.00 deg
5	0.00 dB	0.00 dB	0.00 deg	0.00 deg
6	0.00 dB	0.00 dB	0.00 deg	0.00 deg
7	0.00 dB	0.00 dB	0.00 deg	0.00 deg
8	0.00 dB	0.00 dB	0.00 deg	0.00 deg
9	0.00 dB	0.00 dB	0.00 deg	0.00 deg
10	0.00 dB	0.00 dB	0.00 deg	0.00 deg
11	0.00 dB	0.00 dB	0.00 deg	0.00 deg
12	0.00 dB	0.00 dB	0.00 deg	0.00 deg

Type: Insertion      Format: dB

Figure 14. Powerful software routines not only provide measurement corrections and sequence-prompt instructions, but display results for multiple cables as shown in this screen capture. On the right is a typical soft key “Measurement Menu” cluster, showing the operator choices as the measurement progresses.

## Measurement Uncertainty

The phase measurement accuracy of a typical VNA Master is acquired from the published uncertainties curves. A typical uncertainty curve is shown in Figure 15 (please refer to the technical data sheet for model-specific uncertainty curves). In this example, the legend shows the uncertainties for three bands: 5 kHz to 3 GHz, 3 to 6 GHz, and 6 to 20 GHz. Select the band and then the  $S_{21}$  level to extract the uncertainty in degrees.

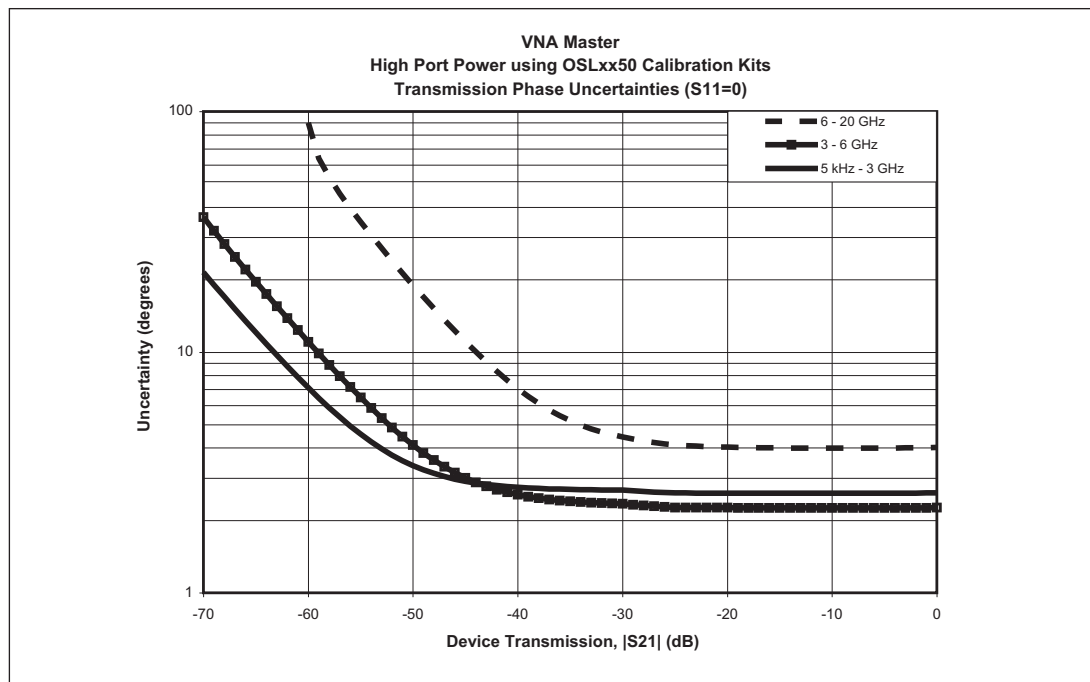


Figure 15. Phase measurement uncertainty for three different frequency ranges for the VNA Master are pictured in this graphic. Note that as the  $S_{21}$  insertion loss increases to 70 dB, the uncertainty increases, caused by trying to get phase information out of a much lower test signal.

The uncertainty graphs in Figure 15 provide measurement uncertainty at 23° C, after vector correction, for the standard N-type connector. Errors are worst-case contributions of residual directivity, source match, frequency response, network analyzer dynamic range, and connector repeatability. For 2-port measurements, transmission tracking, crosstalk and physical load match termination were added. Note that OSLN50 and OSLNF50 calibration components were used for these measurements.

The specification graph shows that **absolute** phase uncertainty in the low VHF ranges (bottom plot) and in the 0- to -40-dB insertion loss range is quite good at approximately  $\pm 2$ -3 degrees. In many phased-antenna applications, the main point of interest is a comparison of phase **differences** among the cables under test. Here, uncertainty in phase differences is expected to be much better than this absolute uncertainty specification since many of the test conditions are identical as one cable is replaced by another.

Finally, although the applications described thus far have dealt mostly with VHF systems and their requirements for phase-matched cables in phase-sensitive antenna systems, the VNA Master easily measures accurate phase characteristics all the way up to 6 and 20 GHz, depending on the model. In such cabling, 1 degree of phase shift is a **very** short length of cable. Consequently, all measurements are exceedingly critical for careful procedures. Even connector repeatability and technique come into play. Even so, as can be seen from Figure 15, for values of insertion loss less than 30 dB, absolute phase uncertainties of about  $\pm 4$  degrees are possible above 6 GHz. Cable matching, however, is much more problematic. Recall, for example, that at 6 GHz, a wavelength is 5 cm (in air) meaning that even 1 mm (1/25th inch) equals 7.2 degrees. With 1/4th inch Andrew Heliax,  $V_p = 0.84$ , 1 mm would equal 8.6 degrees.

## **Summary**

With the demise of the traditional VVM, the Anritsu VNA Master's Vector Voltmeter Option 15 offers a convenient and accurate alternative for a number of critical industry measurements. It is especially well suited for phase matching cables in multi-antenna applications, and for remote component and cable characterization of navigation beacons or wireless base stations. For these applications, the battery-operated VNA Master offers the ideal means of easily measuring and displaying phase and attenuation data for station cabling.

## **Acknowledgements**

Anritsu is indebted to, and appreciates the kind assistance of, the FAA engineering staff in reviewing this application note for procedures and accuracy. Mr. Art Chase of FAA Nav-Aids in the Fairbanks Alaska Technical Service Office was especially helpful in furnishing testing methodologies and advice for this crucial, but tedious cable creation task. Mr. Chase also furnished several operational photographs which provide an environmental snapshot of the field conditions for the task. Any errors are fully assumed by Anritsu.

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