# ATV900 DC Bus Sharing Technical Note 

06/2019

This document describes how to design applications using ATV900 series drives on a common DC bus

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When devices are used for applications with technical safety requirements, the relevant instructions must be followed.

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Failure to observe this information can result in injury or equipment damage.
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## Safety Information

Important Information
NOTICE
Read these instructions carefully, and look at the equipment to become familiar with the device before trying to install, operate, or maintain it. The following special messages may appear throughout this documentation or on the equipment to inform of potential hazards or to call attention to information that clarifies or simplifies a procedure.


The addition of this symbol to a Danger safety label indicates that an electrical hazard exists, which will result in personal injury if the instructions are not followed.

This is the safety alert symbol. It is used to alert you to potential personal injury hazards. Obey all safety messages that follow this symbol to avoid possible injury or death.

## A DANGER

DANGER indicates a hazardous situation which, if not avoided, will result in death or serious injury.

## A WARNING

WARNING indicates a hazardous situation which, if not avoided, could result in death or serious injury.

## A CAUTION

CAUTION indicates a hazardous situation which, if not avoided, could result in minor or moderate injury.

## NOTICE

NOTICE is used to address practices not related to physical injury.

## PLEASE NOTE

Electrical equipment should be installed, operated, serviced, and maintained only by qualified personnel. No responsibility is assumed by Schneider Electric for any consequences arising out of the use of this material.

A qualified person is one who has skills and knowledge related to the construction and operation of electrical equipment and its installation, and has received safety training to recognize and avoid the hazards involved.

## Qualification Of Personnel

Only appropriately trained persons who are familiar with and understand the contents of this manual and all other pertinent product documentation are authorized to work on and with this product. In addition, these persons must have received safety training to recognize and avoid hazards involved. These persons must have sufficient technical training, knowledge and experience and be able to foresee and detect potential hazards that may be caused by using the product, by changing the settings and by the mechanical, electrical and electronic equipment of the entire system in which the product is used. All persons working on and with the product must be fully familiar with all applicable standards, directives, and accident prevention regulations when performing such work.

## Intended Use

This product is a drive for three-phase synchronous, asynchronous motors and intended for industrial use according to this manual. The product may only be used in compliance with all applicable safety standard and local regulations and directives, the specified requirements and the technical data. The product must be installed outside the hazardous ATEX zone. Prior to using the product, you must perform a risk assessment in view of the planned application. Based on the results, the appropriate safety measures must be implemented. Since the product is used as a component in an entire system, you must ensure the safety of persons by means of the design of this entire system (for example, machine design). Any use other than the use explicitly permitted is prohibited and can result in hazards.

## Product Related Information

Read and understand these instructions before performing any procedure with this drive.

## 4 A DANGER

## HAZARD OF ELECTRIC SHOCK, EXPLOSION OR ARC FLASH

- Only appropriately trained persons who are familiar with and understand the contents of this manual and all other pertinent product documentation and who have received safety training to recognize and avoid hazards involved are authorized to work on and with this drive system. Installation, adjustment, repair and maintenance must be performed by qualified personnel.
- The system integrator is responsible for compliance with all local and national electrical code requirements as well as all other applicable regulations with respect to grounding of all equipment.
- Many components of the product, including the printed circuit boards, operate with mains voltage.
- Only use properly rated, electrically insulated tools and measuring equipment.
- Do not touch unshielded components or terminals with voltage present.
- Motors can generate voltage when the shaft is rotated. Prior to performing any type of work on the drive system, block the motor shaft to prevent rotation.
- AC voltage can couple voltage to unused conductors in the motor cable. Insulate both ends of unused conductors of the motor cable.
- Do not short across the DC bus terminals or the DC bus capacitors or the braking resistor terminals.
- Before performing work on the drive system:
- Disconnect all power, including external control power that may be present. Take into account that circuit breaker or main switch does not de-energize all circuits.
- Place a Do Not Turn On label on all power switches related to the drive system. - Lock all power switches in the open position.
- Wait 15 minutes to allow the DC bus capacitors to discharge.
- Follow the instructions given in the chapter "Verifying the Absence of Voltage" in the installation manual of the product.
- Before applying voltage to the drive system:
- Verify that the work has been completed and that the entire installation cannot cause hazards.
- If the mains input terminals and the motor output terminals have been grounded and shortcircuited, remove the ground and the short circuits on the mains input terminals and the motor output terminals.
- Verify proper grounding of all equipment.
- Verify that all protective equipment such as covers, doors, grids is installed and/or closed

Failure to follow these instructions will result in death or serious injury.
Damaged products or accessories may cause electric shock or unanticipated equipment operation.

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## 4 ! DANGER

## ELECTRIC SHOCK OR UNANTICIPATED EQUIPMENT OPERATION

Do not use damaged products or accessories.
Failure to follow these instructions will result in death or serious injury.
Contact your local Schneider Electric sales office if you detect any damage whatsoever.
This equipment has been designed to operate outside of any hazardous location. Only install this equipment in zones known to be free of hazardous atmosphere.

## $\therefore$ DANGER

## POTENTIAL FOR EXPLOSION

Install and use this equipment in non-hazardous locations only.
Failure to follow these instructions will result in death or serious injury.
Your application consists of a whole range of different interrelated mechanical, electrical, and electronic components, the drive being just one part of the application. The drive by itself is neither intended to nor capable of providing the entire functionality to meet all safety-related requirements that apply to your application. Depending on the application and the corresponding risk assessment to be conducted by you, a whole variety of additional equipment is required such as, but not limited to, external encoders, external brakes, external monitoring devices, guards, etc.

As a designer/manufacturer of machines, you must be familiar with and observe all standards that apply to your machine. You must conduct a risk assessment and determine the appropriate Performance Level (PL) and/or Safety Integrity Level (SIL) and design and build your machine in compliance with all applicable standards. In doing so, you must consider the interrelation of all components of the machine. In addition, you must provide instructions for use that enable the user of your machine to perform any type of work on and with the machine such as operation and maintenance in a safe manner.

The present document assumes that you are fully aware of all normative standards and requirements that apply to your application. Since the drive cannot provide all safety-related functionality for your entire application, you must ensure that the required Performance Level and/or Safety Integrity Level is reached by installing all necessary additional equipment.

## A WARNING

## INSUFFICIENT PERFORMANCE LEVEL/SAFETY INTEGRITY LEVEL AND/OR UNINTENDED EQUIPMENT OPERATION

- Conduct a risk assessment according to EN ISO 12100 and all other standards that apply to your application.
- Use redundant components and/or control paths for all critical control functions identified in your risk assessment.
- If moving loads can result in hazards, for example, slipping or falling loads, operate the drive in closed loop mode.
- Verify that the service life of all individual components used in your application is sufficient for the intended service life of your overall application.
- Perform extensive commissioning tests for all potential error situations to verify the effectiveness of the safety-related functions and monitoring functions implemented, for example, but not limited to, speed monitoring by means of encoders, short circuit monitoring for all connected equipment, correct operation of brakes and guards.
- Perform extensive commissioning tests for all potential error situations to verify that the load can be brought to a safe stop under all conditions
Failure to follow these instructions can result in death, serious injury, or equipment damage.
A specific application note NHA80973 is available on hoisting machines and can be downloaded on www.se.com.

Drive systems may perform unexpected movements because of incorrect wiring, incorrect settings, incorrect data or other errors.

## A WARNING

UNANTICIPATED EQUIPMENT OPERATION

- Carefully install the wiring in accordance with the EMC requirements.
- Do not operate the product with unknown or unsuitable settings or data.
- Perform a comprehensive commissioning test.

Failure to follow these instructions can result in death, serious injury, or equipment damage.

## A WARNING

## LOSS OF CONTROL

- The designer of any control scheme must consider the potential failure modes of control paths and, for critical control functions, provide a means to achieve a safe state during and after a path failure. Examples of critical control functions are emergency stop, overtravel stop, power outage and restart.
- Separate or redundant control paths must be provided for critical control functions.
- System control paths may include communication links. Consideration must be given to the implications of unanticipated transmission delays or failures of the link.
- Observe all accident prevention regulations and local safety guidelines (1).
- Each implementation of the product must be individually and thoroughly tested for proper operation before being placed into service. Failure to follow these instructions can result in death, serious injury, or equipment damage.

Failure to follow these instructions can result in death, serious injury, or equipment damage.
(1) For USA: Additional information, refer to NEMA ICS 1.1 (latest edition), Safety Guidelines for the Application, Installation, and Maintenance of Solid State Control and to NEMA ICS 7.1 (latest edition), Safety Standards for Construction and Guide for Selection, Installation and Operation of AdjustableSpeed Drive Systems.

The temperature of the products described in this manual may exceed $80^{\circ} \mathrm{C}\left(176{ }^{\circ} \mathrm{F}\right)$ during operation.

## A WARNING

## HOT SURFACES

- Ensure that any contact with hot surfaces is avoided.
- Do not allow flammable or heat-sensitive parts in the immediate vicinity of hot surfaces.
- Verify that the product has sufficiently cooled down before handling it.
- Verify that the heat dissipation is sufficient by performing a test run under maximum load conditions.
Failure to follow these instructions can result in death, serious injury, or equipment damage.

Machines, controllers, and related equipment are usually integrated into networks. Unauthorized persons and malware may gain access to the machine as well as to other devices on the network/fieldbus of the machine and connected networks via insufficiently secure access to software and networks.

## A warning

## UNAUTHORIZED ACCESS TO THE MACHINE VIA SOFTWARE AND NETWORKS

- In your hazard and risk analysis, consider all hazards that result from access to and operation on the network/fieldbus and develop an appropriate cyber security concept.
- Verify that the hardware infrastructure and the software infrastructure into which the machine is integrated as well as all organizational measures and rules covering access to this infrastructure consider the results of the hazard and risk analysis and are implemented according to best practices and standards covering IT security and cyber security (such as: ISO/IEC 27000 series, Common
- Criteria for Information Technology Security Evaluation, ISO/ IEC 15408, IEC 62351, ISA/IEC 62443, NIST Cybersecurity Framework, Information Security Forum - Standard of Good Practice for Information Security).
- Verify the effectiveness of your IT security and cyber security systems using appropriate, proven methods.

Failure to follow these instructions can result in death, serious injury, or equipment damage.

## A WARNING

## LOSS OF CONTROL

- Perform a comprehensive commissioning test to verify that communication monitoring properly detects communication interruptions.

Failure to follow these instructions can result in death, serious injury, or equipment damage.

| NOTICE |
| :--- |
| DESTRUCTION DUE TO INCORRECT MAINS vOLTAGE |
| Before switching on and configuring the product, verify that it is approved for the mains voltage. |
| Failure to follow these instructions can result in equipment damage. |

## About the book

## Related document

Use your tablet or your PC to quickly access detailed and comprehensive information on all our products on www.schneider-electric.com.

The internet site provides the information you need for products and solutions

- The whole catalog for detailed characteristics and selection guides
- The CAD files to help design your installation, available in over 20 different file formats
- All software and firmware to maintain your installation up to date
- A large quantity of White Papers, Environment documents, Application solutions, Specifications... to gain a better understanding of our electrical systems and equipment or automation
- And finally all the User Guides related to your drive, listed below:

| Title of Documentation | Reference Number |
| :---: | :---: |
| ATV930, ATV950 Installation manual | NHA80932 (English), NHA80933 (French), <br> NHA80934 (German), NHA80935 (Spanish), <br> NHA80936 (Italian), NHA80937 (Chinese), <br> NHA80932PT (Portuguese), NHA80932TR (Turkish) |
| ATV900 Programming manual | NHA80757 (English), NHA80758 (French), <br> NHA80759 (German), NHA80760 (Spanish), <br> NHA80761 (Italian), NHA80762 (Chinese), <br> NHA80757PT (Portuguese), NHA80757TR (Turkish) |
| Altivar Regenerative Unit User manual | NVE88423 (English) |
| Altivar Regenerative Unit Sizing Tool | NVE94856 (English) |

You can download these technical publications and other technical information from our website at http://download.schneider-electric.com

## Terminology

The technical terms, terminology, and the corresponding descriptions in this manual normally use the terms or definitions in the relevant standards.

In the area of drive systems this includes, but is not limited to, terms such as error, error message, failure, fault, fault reset, protection, safe state, safety function, warning, warning message, and so on.
Among others, these standards include:

- IEC 61800 series: Adjustable speed electrical power drive systems
- IEC 61508 Ed. 2 series: Functional safety of electrical/electronic/programmable electronic safety-related
- EN 954-1 Safety of machinery - Safety related parts of control systems
- EN ISO 13849-1 \& 2 Safety of machinery - Safety related parts of control systems.
- IEC 61158 series: Industrial communication networks - Fieldbus specifications
- IEC 61784 series: Industrial communication networks - Profiles
- IEC 60204-1: Safety of machinery - Electrical equipment of machines - Part 1: General requirements

In addition, the term zone of operation is used in conjunction with the description of specific hazards, and is defined as it is for a hazard zone or danger zone in the EC Machinery Directive (2006/42/EC) and in ISO 12100-1.

Also see the glossary at the end of this manual.

## Preamble

The document defines the rules to be applied to link ATV900 drives range on a common DC bus. It also gives the limits of the DC bus connection.
The main target to use a common DC bus is to save energy, as the braking energy of one drive operating in generator mode can be re-used by another drive operating in motor mode instead of dissipating it in heat into a braking resistor. It means that the key point to decide to use a DC bus connection is to define the drives cycles. The DC bus connection has no sense if all drives are all operating in generator mode or in motor mode at the same time. The first step is to estimate the benefits to use a DC bus connection regarding the drives cycles.

Sharing the DC bus and adjusting the drive cycles to reduce the braking energy during normal operation could also lead to a reduction of the number of braking resistors to use in the application. In order to take advantages of using a common DC bus it is necessary to verify that energy is shared during cycles. The diagram below shows a cycle where energy can be saved when one drive is operating in motor mode and another one operating in braking mode.

When some drives linked on the DC bus are braking and the other drives linked on the DC bus cannot re-use the braking energy, excess energy must be either dissipated in a braking resistor or pushed back to the mains power supply using a regenerative unit. See section "Using a braking unit on a common DC bus"
It is also necessary to consider if some emergency operating modes like "fast stop" or "emergency stop" are required by the application, which will need the full power braking capability of all drives at the same time. This situation cannot lead to braking resistors reduction.


NOTE: If the use cases detailed in this technical note does not correspond to your application, or if you need more support, contact your Customer Care Center.

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## General instructions when using a common DC link

## Input voltage

Only drives having the same input voltage range can share the same DC bus. ATV9x0 drives have two mains voltage ranges:

- 200 / 240 V 3-phase for ATV9x0xxxM3x references,
- 400 / 480 V 3-phase for ATV9x0xxxN4x references.


## ATV9x0xxxM3x drives and ATV9x0xxxN4x drives must never share the same DC bus.

## Short circuit detection

The aim of this detection is to help to protect other drives from an internal DC short-circuit in one of the drives linked on the common DC link.
Usually, each drive has to be connected to the DC common link by 2 fuses selected in the semi-conductor protection class, which have the capability to clear a DC current.

## Disconnection from the DC bus.

To easily disconnect one drive from the DC bus while others are in operation, the drives can be wired to the DC bus through a DC voltage switch-disconnector as shown in the drawings of this document. This device provides switch-on and switch-off on the DC-bus and isolation from the DC-bus voltage when it is switched-off to allow the replacement of the fuses or of the drive.
The DC voltage switch-disconnector to be associated with the drives are listed in the section "SC switchdisconnector" at the end of this document

## Input phase loss

Input phase loss fault detection must be enabled on all the drive linked on the DC bus and fed by the AC main power supply. This is required to avoid that a low power drive to supply all the other though the DC bus link in case of mains power loss of high power drives.
When a drive is only fed by the DC bus link, the input phase loss fault must be disabled.

## Ground fault detection

ATV900 ground fault detection does not need to be disabled.

## EMC

When a common DC bus is used, conducted and radiated disturbances level cannot be at the same level as a drive alone. The application of the wiring recommendations of this document helps to minimize the increase of disturbances levels.

## Group definition for drives association

All ATV900 ratings have an integrated DC choke to reduce the input current harmonics, which will also work as input currents balancing between drives linked on the same DC bus.
Drives are grouped according to the following table, depending on the characteristics of the input stage

- Input diodes or thyristors rectifier $\mathrm{I}^{2} \mathrm{t}$
- Mains input voltage range 200 / 240 V or 400 / 480 V

Refer to the ATV900 installation manual for terminal location

| Groups | Drives references | Input stage |
| :---: | :---: | :---: |
| A1 | ATV9x0U07N4x ... ATV9x0D22N4x | 400 V 3-phase, diodes, relay and charge resistor |
| A2 | ATV9x0D30N4x ... ATV9x0C31N4x | 400 V 3 -phase, SCRs/diodes and soft-charge control |
| B1 | ATV9x0U07M3x ... ATV9x0D11M3x | 200 V 3 -phase, diodes, relay and charge resistor |
| B2 | ATV9x0D15M3x ... ATV9x0D45M3x | 200 V 3 -phase, SCRs/diodes and soft-charge control |

## Wiring

All ATV9x0 drives are $380 \sim 480 \mathrm{~V}$ or $200 \sim 240 \mathrm{~V}$, 3-phase AC input voltage. When the drives share the same DC bus and are supplied at the same time by the mains on L1, L2 and L3 terminals, it must be by the same power lines after the same mains transformer.
In order to limit the over-voltages on the common DC bus while drives are operating, the following cabling rules must be respected:

- The total cable length between PA/+ and PC/- connections of one drive to PA/+ and PC/- connections of another drive must be less than $2 \mathbf{m}$.
- The ground wire included in the DC bus is optional. It is not a protective ground conductor (PE); it just helps to reduce the conducted and radiated emissions.
- The distance between +DC and -DC wires must not exceed $5 \mathbf{~ c m}$ except close to the junctions' terminals, the switch-disconnector, the fuses holders or the drives PA/+ and PC/- to allow cabling. This is to avoid over-voltage on the DC link while the drives are operating.
To meet this requirement, it is possible to use one of the following solutions:
Independent cables with cable clamps,
Two or three-wires sheathed cable,
Or 2-wires shielded cable where the shield is grounded.


## Drives supplied by the AC mains

To protect the drives' input rectifiers in case of short-circuit on the DC bus link, semi-conductor protection class fuses must be selected from the table at the end of this document. The location of fuses depends on the type of drives used on the DC bus link.
All the drives sharing a common DC bus link must be switched-on at the same time to the mains power supply. If there is a delay between different switch-on, high power drive must be switched on before low power drives. This is to avoid low power drives to charge all the capacitors of the drives wired on the common DC bus.
When drives are fed by the AC mains, all the input rectifiers of the drives linked on the common DC bus are operating. To balance the input currents between drives, the rules described in this section must be applied.
All ATV900 drives have DC terminals similar to the input lines and motor output terminals. Same cables as those used for mains input lines can be used for DC bus connections.
The drive terminals cannot withstand the total DC-bus current and therefore cannot be used for chaining. Wiring blocks must be used to build the DC bus link and to wire each drive with only one wire for the PA/+ connection and one wire for the PC/- connection.
The wiring blocks can be selected in the Schneider-Electric catalog in the LINERGY product range as shown in the last section (Wiring options) of this document.
In order to limit the over-voltages on the common DC bus while drives are operating, the wiring recommendations listed at the beginning of this document must be applied.

The generic wiring diagram of this configuration is shown in the drawing below:


For U (mains) $=400 / 480 \mathrm{~V}$, drives $1 \ldots \mathrm{n}$ must belong to groups A 1 or A 2
For U (mains) $=200 / 240 \mathrm{~V}$, drives $1 \ldots \mathrm{n}$ must belong to groups B1 or B2

## Drives supplied by the DC terminals

In this configuration, the drives are not supplied by the mains power supply, but only through the PA/+ terminal and the PC/- inputs. The DC source can be one of the following:

- A drive which a part of the power is provided to other drives through the DC bus,
- A dedicated DC power source device to provide DC voltage.


## Drives supplied by the DC outputs of another drive

ATV900 can supply in a correct way a motor of minimum one third of the drive rated power. It means that the maximum power available to supply a DC bus is two third of the drive's power rating.
The drive which supplies the common DC bus of other drives must always use the input line choke listed in the section "Line chokes" at the end of this document, in order to limit the RMS input current due to increased capacitors value on the DC bus.

The generic cabling circuit is shown on the drawings below.


For U (mains) $=400 / 480 \mathrm{~V}$, drives $1 \ldots$ n must belong to groups A 1 or A 2
For U (mains) $=200 / 240 \mathrm{~V}$, drives $1 \ldots$ n must belong to groups B1 or B2

In addition to the general instructions listed at the beginning of this document, the following rules must be respected:

- The power rating of drive 1 is always the highest power rating of the full system. It must be used at least at one third of its rated power (for example a 90 kW drive must be used at least with a 30 kW motor, which leaves 60 kW to supply drives 2 to n )
- An additional input line choke selected from the list of the section "Line chokes" at the end of this document, is needed only if the total power of drives 2 to n is greater than $25 \%$ of the rated power of drive 1, because of the increase of the total DC capacitor value.
- Drives 2 to n are sorted by power rating: from the highest for drive 2 to the lowest for drive n , to get the highest wiring impedance on the lowest drive power rating.
- If drives 2 to drives $n$ belong to groups A1 or B1, the internal soft-charge circuits of these drives will limit the capacitor charge current during switch-on of drive 1.
Drives 2 to n belonging to group A2 or B2, must use the additional external soft-charge circuit as described in the section at the end of this document, because there is no DC capacitors charge limitation when they are supplied by the DC bus.
- DC fuses on each drive (drive 1 to drive $n$ ) have to be defined according to the "Fuses table" section at the end of this document.


## Drive supplied by a DC power supply

The DC power supply replaces the drive which shared a part of its power with the common DC bus in the configuration of the previous section. The output power rating of the DC source must be greater or equal to the sum of all drives' power rating linked on the common DC bus. It has also to provide the transient overload required by the drives in the application.
The DC source output protection fuses have to be selected according to the DC source user's manual. If these data are not provided, the same semiconductors protection class fuses defined for the drive of the same power rating can be used.
The DC source must guarantee a maximum of 3\% DC voltage drop and 5\% DC voltage ripple at rated load.
If the DC source is a simple diodes or non-reversible SCR/diodes rectifier, input line chokes or DC output choke might have to be added to reduce the input line RMS current.
If the DC source is an active front-end which performs also input harmonic current mitigation with or without regenerative braking capabilities, no additional parts are needed except those needed by the active DC source itself.

In addition to the generic instructions defined at the beginning of this document, the following additional requirements must be applied in this case:

- Drives 2 to n are sorted by power rating: from the highest for drive 2 to the lowest for drive n , to get the highest wiring impedance on the lowest drive power rating.
- If drives 2 to drives $n$ belong to groups A1 or B1, the internal soft-charge circuits of these drives will limit the capacitor charge current during switch-on of drive 1.
Drives $\mathbf{2}$ to $\mathbf{n}$ belonging to group A2 or B2, must use the additional external soft-charge circuit as described in the section at the end of this document, because there is no DC capacitors charge limitation when they are supplied by the DC bus.
- DC fuses on each drive (drive 1 to drive $n$ ) have to be defined according to the "Fuses table" section at the end of this document.


For U (mains) $=400 / 480 \mathrm{~V}$, drives $2 \ldots$ n must belong to groups A1 or A2
For U (mains) $=200 / 240 \mathrm{~V}$, drives $2 \ldots$ n must belong to groups B1 or B2

## Using a braking unit on a common DC bus.

When some drives sharing a common DC-bus are braking and if the other drives linked on the same DC-bus are not able to use all this braking energy, the drives' DC bus capacitors will store this energy. This will lead to an increase of the DC bus voltage. To avoid any over-braking error on the drives (error code: ObF) a braking unit can be used. The same solutions as for a single drive can be used:

- braking resistor,
- or regenerative braking unit.

The full knowledge of the application cycles, or the situations which can happen during all drives' operations is necessary to define what are the peak and average power, the braking time and the duty cycle.

## Braking resistor.

In any of the above described DC-bus sharing configuration, a braking resistor can be used on each drive linked to the DC-bus, when this feature in included. The braking IGBT integrated in the drives is activated when the DC bus voltage reaches a defined level. Since the DC-bus voltage is common, any braking IGBT of any drive on the DC-bus will operate to discharge the DC-bus through the externally connected resistor.
On each drive equipped with a braking resistor, the parameter "brC" must be set to "yes" to enable operation of the braking IGBT. This will set parameter "brA" to "no" on these drives.
Parameter "brA" can be set in different ways on the other drives sharing the common DC-bus:

- "brA" set to "no" to get the braking performances on drives to follow the deceleration ramp.
- "brA" set to "yes" for drives for which it is not necessary to follow the deceleration ramp.

The calculation of the braking resistor is made in the same way as for a single drive, but the total braking power on the DC bus must be considered. This includes the maximum steady state braking power and the deceleration power of all the drive which have the "brA" parameter set to "no".
This will give the peak power $P_{\text {peak }}$, the total braking time, the average power $P_{\text {avg }}$ and the duty cycle.

## Using only one braking resistor

The simplest solution is to use only one braking resistor wired on one of the drives sharing the DC bus. This is possible if the calculated peak braking power $P_{\text {peak }}$ and the average braking power $P_{\text {avg }}$ are lower than the capabilities of one of the drives sharing the DC bus. The decision process is the following:

## 1.Select the drive to be equipped by a braking resistor

The peak braking power $P_{\text {peak }}$ of the system must be dissipated in the braking resistor. To do it, the maximum resistor value $R_{\text {max }}$ is calculated by

$$
R_{\max }=\frac{\left(U_{\text {brake }}\right)^{2}}{P_{\text {peak }}}
$$

where $U_{\text {brake }}$ is the DC bus voltage when the braking IGBT is in use. On ATV900, $U_{\text {brake }}=780 \mathrm{~V}$.

The drive selected must accept a minimum braking resistor value $R_{\min }$ lower than $R_{\max }$ in order to be able to select a resistor value $R$ defined by

$$
R_{\min } \leq R \leq R_{\max }
$$

The highest power rating drive sharing the DC bus equipped with a braking IGBT can be used to drive the braking resistor even if it is not this drive which will brake during the application cycle. Even in "ready" state, ATV900 can activate the braking IGBT if the "brC" parameter is set to "yes" and the "brA" parameter set to "no".
If no drive on the DC bus has $R_{\min }$ specification verifying $R_{\min } \leq R_{\max }$, it is not possible to use only one braking resistor in the system.

In this case the section "Using more than one braking resistor" later in this document must be considered.

## 2. Define the braking resistor rated power

The braking torque characteristic and the duty cycle of the application allow to calculate the average braking power $P_{\text {avg }}$. The rated power of the braking resistor $R$ must be greater or equal to this average braking power. The overload factor of the braking resistor must allow to withstand the peak power $P_{\text {peak }}$. The typical braking cycles defined in the ATV900 catalog can help to select a braking resistor.

## Using more than one braking resistor

If there is no drive sharing the DC bus having a $R_{\min }$ specification which meet the condition $R_{\min } \leq R_{\max }$, it means that the peak braking power has to be shared by two or more drives depending on the application.

## 1. Define number and values of braking resistors

The simplest way is to start with the highest power rating drive sharing the $D C$ bus and to define the peak power $P_{\text {peak(R1) }}$ that it will be able to dissipate:

$$
P_{\text {peak }(R 1)}=\frac{\left(U_{\text {brake }}\right)^{2}}{R_{1}}
$$

with $R_{1} \geq R_{\min (1)}$ where $R_{\min (1)}$ is the minimum braking resistor of drive 1 .

This has to be continued with the next highest drives' power ratings to define $R_{2} \geq R_{\min (2)}, \ldots R_{n} \geq R_{\min (n)}$ with $R_{2} \geq R_{\min (2)}$ where $R_{\min (2)}$ is the minimum braking resistor of drive $2, \ldots$ and $R_{n} \geq R_{\min (n)}$ where $R_{\min (n)}$ is the minimum braking resistor of drive n and to calculate

$$
P_{\text {peak }(R 2)}=\frac{\left(U_{\text {brake }}\right)^{2}}{R_{2}}, \ldots \quad P_{\text {peak }(R n)}=\frac{\left(U_{\text {brake }}\right)^{2}}{R_{n}}
$$

until we get

$$
P_{\text {peak }(R 1)}+P_{\text {peak }(R 2)}+\cdots+P_{\text {peak }(R n)} \geq P_{\text {peak }}
$$

## 2. Define braking resistors rated power

The braking torque characteristic and the duty cycle of the application allow to calculate the total average braking power $P_{\text {avg }}$, which must be shared between all the braking resistors. The rated power of each resistor $P_{\text {avg(Ri) }}$ will be defined with the same ratio to the average braking power as the ratio of the peak power of each resistor to the total peak power.
The peak power of resistor $i$ is

$$
P_{\text {peak }(R i)}=\frac{\left(U_{\text {brake }}\right)^{2}}{R_{i}}
$$

The total peak power for all the resistors is

$$
P_{\text {peak }}=P_{\text {peak }(R 1)}+P_{\text {peak }(R 2)}+\cdots+P_{\text {peak }(R n)}=\left(U_{\text {brake }}\right)^{2} \cdot\left(\frac{1}{R_{1}}+\frac{1}{R_{2}}+\cdots+\frac{1}{R_{n}}\right)
$$

The ratio $k\left(R_{i}\right)$ of the peak power of resistor $i$ to the total peak power is

$$
k\left(R_{i}\right)=\frac{P_{\text {peak }(R i)}}{P_{\text {peak }}}=\frac{\frac{1}{R_{i}}}{\frac{1}{R_{1}}+\frac{1}{R_{2}}+\cdots+\frac{1}{R_{n}}}
$$

The average power of resistor $i$ can be calculated by

$$
P_{\operatorname{avg}(R i)}=k\left(R_{i}\right) \cdot P_{a v g}
$$

## Example 1: one braking resistor

Let consider the following system of 3 drives sharing the same DC bus:
ATV9x0D15N4 + ATV9x0U75N4 + ATV9x0U40N4
The application is defined by the following

- ATV9x0D15N4 never brakes; it can be running or in "ready" state
- ATV9x0U75N4 and ATV9x0U40N4 are making cycles and can brake both at rated torque at the same time to decelerate their loads from rated speed down to 0 during 3 s every 40 s .

When ATV9x0D15N4 is operating at least at $80 \%$ of its rated torque the braking energy of the two other drives is reused by ATV9x0D15N4.
When ATV9x0D15N4 is in "ready", the braking energy of ATV9x0U75N4 and ATV9x0U40N4 must be dissipated in a braking resistor.

To simplify the calculation, we consider 0.9 as the motors efficiency and 0.95 as the drives efficiency. The total peak power of the system is the sum of the peak power of both drives:

$$
P_{\text {peak }}=(7.5 \times 0.9 \times 0.95)+(4.0 \times 0.9 \times 0.95)=6.41+3.42=9.83 \mathrm{~kW}
$$

The maximum resistor $R_{\max }$ to get this peak power is

$$
R_{\max }=\frac{780^{2}}{9.83 \times 10^{3}}=61.9 \Omega
$$

The minimum braking resistor value of ATV900HD15N4 is given in ATV900 installation manual

$$
R_{\min }=16 \Omega
$$

The condition $R_{\min } \leq R_{\max }$ is met. It is possible to select a resistor value between $16 \Omega$ and $61.9 \Omega$
The two drives are braking by doing a deceleration at constant torque, it means that the power is decreasing linearly with speed during 3 s and then there is no braking power during 40 s . The average power during one cycle can be calculated by

$$
P_{\text {avg }}=\frac{1}{3+40} \times\left(\frac{9.83 \mathrm{~kW}}{2} \times 3+0 \times 40\right)=228.7 \mathrm{~W}
$$

The reference VW3A7732, $28 \Omega, 300 \mathrm{~W}$ wired on the ATV9x0D15N4 meets the requirements of this application.

## Example 2: two braking resistors

Let consider the following system of 7 drives sharing the same DC bus:
ATV9x0U75N4 + ATV9x0U55N4 + $5 \times$ ATV9x0U22N4
The application is defined by the following

- All drives are making acceleration and deceleration cycles.
- The sequences of the drives are synchronized in a way that there are always drives running using enough power when another one is braking. In this case the DC bus sharing is operating.
- Every 75 s all the drives have to stop at the same time, with a braking torque equal to 1.3 times the rated torque of the motor, during 2 s to decrease the speed from rates speed down to 0 .

The DC bus sharing does not work to achieve the full braking sequence every 75 s . This braking energy has to be dissipated in braking resistors. Instead of using one braking resistor per drive, it is possible to use less than 7 pieces in this application.
To simplify the calculation, we consider 0.9 as the motors efficiency and 0.95 as the drives efficiency. The total peak power of the system is the sum of the peak power of all drives:
$P_{\text {peak }}=(1.3 \times 7.5 \times 0.9 \times 0.95)+(1.3 \times 5.5 \times 0.9 \times 0.95)+5 \times(1.3 \times 2.2 \times 0.9 \times 0.95)=26.7 \mathrm{~kW}$
$P_{\text {avg }}=\frac{1}{2+75} \times\left(\frac{26.7 \mathrm{~kW}}{2} \times 2+0 \times 75\right)=346.8 \mathrm{~W}$

The highest drive power rating is ATV9x0U75N4. The minimum braking resistor value is $R_{\min (1)}=28 \Omega$.
This value exists in the ATV900 catalog, $R_{1}=28 \Omega$ can be selected.
With this value $P_{\text {peak }(R 1)}=\frac{780^{2}}{28}=21.7 \mathrm{~kW}$ which is not enough compared to 26.7 kW

The next highest drive power rating is ATV9x0U55N4. The minimum braking resistor value is $R_{\min (2)}=31 \Omega$. This value does not exist in the ATV900 catalog, the next higher value is $R_{2}=60 \Omega$
With this value $P_{\text {peak }(R 2)}=\frac{780^{2}}{60}=10.1 \mathrm{~kW}$.
Now $P_{\text {peak }(R 1)}+P_{\text {peak }(R 2)}=21.7+10.1=31.8 \mathrm{~kW}$ is greater than 26.7 kW
The application will use

- $R_{1}=28 \Omega$ braking resistor associated with the ATV9x0U75N4
- $R_{2}=60 \Omega$ braking resistor associated with the ATV0x0U55N4

The total average power of the application is shared between R1 and R2 by the following factors:

$$
\begin{aligned}
& k\left(R_{1}\right)=\frac{\frac{1}{28}}{\frac{1}{28}+\frac{1}{60}}=0.68 \Rightarrow P_{\operatorname{avg}(R 1)}=0.682 \cdot 346.8=236.4 \mathrm{~W} \\
& k\left(R_{2}\right)=\frac{\frac{1}{60}}{\frac{1}{28}+\frac{1}{60}}=0.32 \Rightarrow P_{\operatorname{avg}(R 2)}=0.318 \cdot 346.8=110.3 \mathrm{~W}
\end{aligned}
$$

The selected resistance from the catalog are:
VW3A7732, $28 \Omega, 300 \mathrm{~W}$
VW3A7731, $60 \Omega, 160 \mathrm{~W}$

## Regenerative braking unit.

In any of the above described DC-bus sharing configuration using $400 / 480 \mathrm{~V}$ drives, the regenerative units ATVRU75N4 and/or ATVRD15N4 can be used on the DC-bus. These regenerative braking units are autonomous devices, that compare the input mains voltage level with the DC-bus voltage, and start to push-back power to the mains when the difference is greater than a fixed threshold.
The rated power of ATVRU75N4 is 6.8 kW continuous, with 10.2 kW transient overload during 60s.
The rated power of ATVRD15N4 is 13.5 kW continuous, with 20.3 kW transient overload during 60 s .
These units can be associated in parallel, up to 3 units of any of the two power ratings, to cover up to 45 kW . When the average braking power is high, these units have an advantage compared to braking resistors:

- regen units can be integrated in the cabinet because the size is smaller than hoisting type resistors,
- the heat dissipation is very low, because their efficiency is better than $95 \%$,
- depending on the braking power and the cycle, the return on investment by energy saving can be fast.

If we consider the same system as in example 2 in previous section, but with a more severe cycle: the machine has to stop every 20 s . In this case the peak power is the same as in the previous cycle, but the average power becomes:

$$
P_{a v g}=\frac{1}{2+20} \times\left(\frac{26.7 \mathrm{~kW}}{2} \times 2+0 \times 20\right)=1213.6 \mathrm{~W}
$$

This leads to select braking resistors of same value but with higher average power:
VW3A7742, $28 \Omega, 1100 \mathrm{~W} \quad 570 \mathrm{~mm} \times 190 \mathrm{~mm} \times 180 \mathrm{~mm}$
VW3A7741, $60 \Omega, 500 \mathrm{~W} \quad 465 \mathrm{~mm} \times 175 \mathrm{~mm} \times 100 \mathrm{~mm}$

To compare with power regenerative units, the peak power of 26.7 kW is achieved by using

| 1x ATVRD15N4 | $399 \mathrm{~mm} \times 235 \mathrm{~mm} \times 105 \mathrm{~mm}$ |
| :--- | :--- |
| $+1 \times$ ATVRU75N4 | $337 \mathrm{~mm} \times 175 \mathrm{~mm} \times 80 \mathrm{~mm}$ |

The two units are wired in parallel, which gives a total of 30.5 kW transient power, more than enough average power, with smaller overall dimensions.
Taking into account a global efficiency of the two regen units of $95 \%$ and assuming 8 hours per days, 220 days per year of the system operation, the total energy saved per year is:

$$
E_{\text {saved }}=1213.6 \times 0.95 \times 8 \times 220=2029.3 \mathrm{kWh}
$$

Depending on the local energy cost and the buying price difference between the two resistors and the two regen units it is easy to calculate the return on investment of the regen solution.

## Fuses table

The fuses to be used with the drives sharing a common DC bus must be selected in the semiconductors protection class. The following table give for each drive the rating of the fuse as it is given in the fuses' suppliers catalog. It takes in to account the following parameters:

- The current rating of the fuse is given at $30^{\circ} \mathrm{C}$, the value listed in this table takes into account the derating to be applied on the fuse to operate in the $50^{\circ} \mathrm{C}$ drive's environment,
- The current rating of the fuse takes also into account the drives overload (1.5 rated current during 60 s ) and the thermal cycling when the drive is running or stopped.

To protect the input rectifiers of the drives two fuses must be used: one fuse on the +DC line and one fuse on the -DC line.

## IEC fuses table

| Drives 400 / 480 V |  | Semi-conductor protection class fuses ratings of MERSEN |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| reference | Power (kW) | Current rating (A) | IEC <br> DC voltage (V) | Reference | Fuse support for 2 fuses in DC lines |
| ATV9x0U07N4x | 0.75 | 6 | $700{ }^{(1)}$ | FR10GR69V6 | 2 US U 101 IHEL |
| ATV9x0U15N4x | 1.5 | 8 | $700{ }^{(1)}$ | FR10GR69V8 | 2 XS 101 HEL |
| ATV9x0U22N4x | 2.2 | 12.5 | $700{ }^{(1)}$ | FR10GR69V12.5 | $2 \times$ US101IHEL |
| ATV9x0U30N4x | 3.0 | 16 | $700{ }^{(1)}$ | FR10GR69V16 | $2 \mathrm{XSS1011HEL}$ |
| ATV9x0U40N4x | 4.0 | 20 | $700{ }^{(1)}$ | FR10GR69V20 | $2 \times$ US101IHEL |
| ATV9x0U55N4x | 5.5 | 25 | $700{ }^{(1)}$ | FR10GR69V25 | 2 US 101 HEL |
| ATV9x0U75N4x | 7.5 | 32 | $700{ }^{(1)}$ | FR10GR69V32 | $2 \times$ US101IHEL |
| ATV9x0D11N4x | 11 | 50 | 1000 | FR27GB80V50T | PS272PREBS |
| ATV9x0D15N4x | 15 | 63 | 1000 | FR27GB80V63T | PS272PREBS |
| ATV9x0D18N4x | 18.5 | 63 | 1000 | FR27GB80V63T | PS272PREBS |
| ATV9x0D22N4x | 22 | 80 | 1000 | FR27GB80V80T | PS272PREBS |
| ATV9x0D30N4x | 30 | 100 | 1000 | FR27GB80V100T | PS272PREBS |
| ATV9x0D37N4x | 37 | 125 | $750{ }^{(1)}$ | NH1GS69V125PV | 2x HPBB11PPR |
| ATV9x0D45N4x | 45 | 160 | $750{ }^{(1)}$ | NH1GS69V160PV | 2x HPBB11PPR |
| ATV9x0D55N4x | 55 | 200 | $750{ }^{(1)}$ | NH1GS69V200PV | 2x HPBB11PPR |
| ATV9x0D75N4x | 75 | 250 | $750{ }^{(1)}$ | NH1GS69V250PV | 2x HPBB11PPR |
| ATV9x0D90N4x | 90 | 315 | $750{ }^{(1)}$ | NH2GS69V315PV | 2x HPBB21PPR |
| ATV9x0C11N4x | 110 | 400 | $700{ }^{(1)}$ | PC32UD69V400A | 2x SIDN80630A |
| ATV9x0C13N4x | 132 | 450 | $700{ }^{(1)}$ | PC32UD69V450A | 2x SIDN80630A |
| ATV9x0C16N4x | 160 | 500 | $700{ }^{(1)}$ | PC32UD69V500A | $2 \mathrm{SIDN80630A}$ |
| ATV9x0C22N4x | 220 | (3) | (3) | (3) | (3) |
| ATV9x0C25N4x | 250 | (3) | (3) | (3) | (3) |
| ATV9x0C31N4x | 315 | (3) | (3) | (3) | (3) |


| Drives 200 / 240 V | Semi-conductor protection class fuses ratings of MERSEN |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| reference | Power <br> (kW) | Current <br> rating (A) | IEC <br> DC voltage (V) | Reference | Fuse support <br> for 2 fuses in DC lines |
| ATV9x0U07M3x | 0.75 | 8 | 700 | FR10GR69V8 | US102I |
| ATV9x0U15M3x | 1.5 | 16 | 700 | FR10GR69V16 | US102I |
| ATV9x0U22M3x | 2.2 | 20 | 700 | FR10GR69V20 | US102I |
| ATV9x0U30M3x | 3.0 | 25 | 700 | FR10GR69V25 | US102I |
| ATV9x0U40M3x | 4.0 | 40 | 900 | FR14GR69V40 | US142I |
| ATV9x0U55M3x | 5.5 | 50 | 900 | FR14GR69V50 | US142I |
| ATV9x0U75M3x | 7.5 | 63 | 900 | FR22GR69V63 | US222I |
| ATV9x0D11M3x | 11 | 80 | 900 | FR22GR69V80 | US222I |
| ATV9x0D15M3x | 15 | 100 | 900 | FR22GR69V100 | US222I |
| ATV9x0D18M3x | 18.5 | 125 | 750 | NH00GS69V125PV | BB002EPBR |
| ATV9x0D22M3x | 22 | 160 | 750 | NH1GS69V160PV | BB12PPR |
| ATV9x0D30M3x | 30 | 200 | 750 | NH1GS69V200PV | BB12PPR |
| ATV9x0D37M3x | 37 | 250 | 750 | NH1GS69V250PV | BB12PPR |
| ATV9x0D45M3x | 45 | 315 | 750 | NH2GS69V315PV | BB22PPR |
| ATV9x0D55M3x | 55 | 400 | 750 | NH2UD69V400PV | BB22PPR |
| ATV9x0D75M3x | 75 | 500 | 750 | NH2UD69V500PV | BB22PPR |

## UL fuses table

| Drives 400 / 480 V |  | Semi-conductor protection class fuses ratings of MERSEN |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| reference | Power (kW) | Current <br> rating (A) | UL DC voltage (V) | Reference | Fuse support for 2 fuses in DC lines |
| ATV9x0U07N4x | 0.75 | 6 | 1000 | DCT6-2 | 2 XS 101 IHEL |
| ATV9x0U15N4x | 1.5 | 8 | 1000 | DCT8-2 | 2 US 101 HHEL |
| ATV9x0U22N4x | 2.2 | 12 | 1000 | DCT12-2 | 2 X US101IHEL |
| ATV9x0U30N4x | 3.0 | 15 | 1000 | DCT15-2 | 2 XS 101 HEL |
| ATV9x0U40N4x | 4.0 | 20 | 1000 | DCT20-2 | 2 XS 101 HEL |
| ATV9x0U55N4x | 5.5 | 25 | 1000 | DCT25-2 | 2 XS 101 HEL |
| ATV9x0U75N4x | 7.5 | 30 | 1000 | DCT30-2 | 2 XS U101IHEL |
| ATV9x0D11N4x | 11 | 50 | $950{ }^{(1)}$ | HSJ50 | PS272PREBS |
| ATV9x0D15N4x | 15 | 60 | $950{ }^{(1)}$ | HSJ60 | PS272PREBS |
| ATV9x0D18N4x | 18.5 | 60 | $950{ }^{(1)}$ | HSJ60 | PS272PREBS |
| ATV9x0D22N4x | 22 | 110 | $950{ }^{(1)}$ | HSJ110 ${ }^{(2)}$ | 2x 62001HPJ |
| ATV9x0D30N4x | 30 | 110 | $950{ }^{(1)}$ | HSJ110 ${ }^{(2)}$ | 2 6 62001HPJ |
| ATV9x0D37N4x | 37 | 125 | $950{ }^{(1)}$ | HSJ125 | 2 6 62001 HPJ |
| ATV9x0D45N4x | 45 | 150 | $950{ }^{(1)}$ | HSJ150 | 2 x 62001 HPJ |
| ATV9x0D55N4x | 45 | 200 | $950{ }^{(1)}$ | HSJ200 | 2 x 62001 HPJ |
| ATV9x0D75N4x | 55 | 250 | $950{ }^{(1)}$ | HSJ250 | 2 6 4031 HPJ |
| ATV9x0D90N4x | 75 | 350 | $950{ }^{(1)}$ | HSJ350 | 2 6 4031 HPJ |
| ATV9x0C11N4x | 110 | 400 | $950{ }^{(1)}$ | HSJ400 | $2 \times 64031 \mathrm{HPJ}$ |
| ATV9x0C13N4x | 132 | 450 | $950{ }^{(1)}$ | HSJ450 | $2 \times 6631 \mathrm{HPJ}$ |
| ATV9x0C16N4x | 160 | 500 | $950{ }^{(1)}$ | HSJ500 | $2 \times 6631 \mathrm{HPJ}$ |
| ATV9x0C22N4x | 220 | (3) | (3) | (3) | (3) |
| ATV9x0C25N4x | 250 | (3) | (3) | (3) | (3) |
| ATV9x0C31N4x | 315 | (3) | (3) | (3) | (3) |


| Drives 200 / 240 V |  | Semi-conductor protection class fuses ratings of MERSEN |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| reference | Power (kW) | Current rating (A) | $\begin{gathered} \text { IEC } \\ \text { DC voltage (V) } \end{gathered}$ | Reference | Fuse support for 2 fuses in DC lines |
| ATV9x0U07M3x | 0.75 | 8 | 500 | FR10GR69V8 | US102I |
| ATV9x0U15M3x | 1.5 | 16 | 500 | FR10GR69V16 | US102I |
| ATV9x0U22M3x | 2.2 | 20 | 500 | FR10GR69V20 | US102I |
| ATV9x0U30M3x | 3.0 | 25 | 500 | FR10GR69V25 | US102I |
| ATV9x0U40M3x | 4.0 | 40 | 500 | FR14GR69V40 | US142I |
| ATV9x0U55M3x | 5.5 | 50 | 500 | FR14GR69V50 | US1421 |
| ATV9x0U75M3x | 7.5 | 63 | 500 | FR22GR69V63 | US222I |
| ATV9x0D11M3x | 11 | 80 | 500 | FR22GR69V80 | US222I |
| ATV9x0D15M3 | 15 | 100 | 500 | FR22GR69V100 | US222I |
| ATV9x0D18M3x | 18.5 | 125 | 500 | HSJ125 | 2 6 62001 HPJ |
| ATV9x0D22M3x | 22 | 160 | 750 | HSJ150 | 2x 62001HPJ |
| ATV9x0D30M3x | 30 | 200 | 750 | HSJ200 | 2x 62001HPJ |
| ATV9x0D37M3x | 37 | 250 | 750 | HSJ250 | 2 6 64031 HPJ |
| ATV9x0D45M3x | 45 | 315 | 750 | HSJ350 | $2 \mathrm{64031HPJ}$ |
| ATV9x0D55M3x | 55 | 400 | 750 | HSJ400 | 2 6 64031 HPJ |
| ATV9x0D75M3x | 75 | 500 | 750 | HSJ500 | $2 \mathrm{6631HPJ}$ |

(1) with two fuses: one in +DC and one in -DC
(2)
fuse holder for fuses ratings HSJ80 and HSJ100 is not UL certified up to 600 V , therefore, rating 110 A is used.
(3) waiting for MERSEN proposal

## DC switch-disconnector.

To disconnect one drive from the DC bus while other drives remain in operation, each drive can be equipped by a DC switch-disconnector selected in the following table. It takes into account:

- the derating to apply to these devices to operate at $50^{\circ} \mathrm{C}$ ambient temperature,
- the operation overload on the drives.

These devices use $2 \times 2$ poles in series and must be installed as described in the devices instruction sheet for use at 800 V DC voltage.

| Drives 380 / 480 V |  | DC switch-disconnector |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| reference | Power <br> (kW) | Short name | Reference | DC voltage @ $50^{\circ} \mathrm{C}$ (V) | Rated current $@ 50^{\circ} \mathrm{C}$ <br> (A) |
| ATV9x0U07N4x | 0.75 | C60NA-DC | A9N61690 | 800 | 30 |
| ATV9x0U15N4x | 1.5 |  |  |  |  |
| ATV9x0U22N4x | 2.2 |  |  |  |  |
| ATV9x0U30N4x | 3.0 |  |  |  |  |
| ATV9x0U40N4x | 4.0 |  |  |  |  |
| ATV9x0U55N4x | 5.5 |  |  |  |  |
| ATV9x0U75N4x | 7.5 |  |  |  |  |
| ATV9x0D11N4x | 11 |  |  |  |  |
| ATV9x0D15N4x | 15 |  |  |  |  |
| ATV9x0D18N4x | 18.5 | C120NA-DC | A9N61701 | 1000 | 96 |
| ATV9x0D22N4x | 22 |  |  |  |  |
| ATV9x0D30N4x | 30 |  |  |  |  |
| ATV9x0D37N4x | 37 |  |  |  |  |
| ATV9x0D45N4x | 45 |  |  |  |  |
| ATV9x0D55N4x | 55 | NSX160 NA DC PV 4P | LV438160 | 1000 | 160 |
| ATV9x0D75N4x | 75 |  |  |  |  |
| ATV9x0D90N4x | 90 | NSX200 NA DC PV 4P | LV438250 | 1000 | 190 |
| ATV9x0C11N4x | 110 | NSX400 NA DC PV 4P | LV438300 | 1000 | 400 |
| ATV9x0C13N4x | 132 |  |  |  |  |
| ATV9x0C16N4x | 160 |  |  |  |  |
| ATV9x0C22N4x | 220 | NSX500 NA DC PV 4P | LV438500 | 1000 | 490 |
| ATV9x0C25N4x | 250 | NSX630b NA DC PV 4P |  | 1000 | 630 |
| ATV9x0C31N4x | 315 | NSX800 NA DC PV 4P |  | 1000 | 800 |


| Drives 200 / 240 V |  | DC switch-disconnector |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| reference | Power <br> (kW) | Short name | Reference | DC voltage $@ 50^{\circ} \mathrm{C}$ (V) | Rated current $@ 50^{\circ} \mathrm{C}$ <br> (A) |
| ATV9x0U07M3x | 0.75 | C60NA-DC | A9N61690 | 800 | 30 |
| ATV9x0U15M3x | 1.5 |  |  |  |  |
| ATV9x0U22M3x | 2.2 |  |  |  |  |
| ATV9x0U30M3x | 3.0 |  |  |  |  |
| ATV9x0U40M3x | 4.0 |  |  |  |  |
| ATV9x0U55M3x | 5.5 |  |  |  |  |
| ATV9x0U75M3x | 7.5 |  |  |  |  |
| ATV9x0D11M3x | 11 | C120NA-DC | A9N61701 | 1000 | 96 |
| ATV9x0D15M3x | 15 |  |  |  |  |
| ATV9x0D18M3x | 18.5 |  |  |  |  |
| ATV9x0D22M3x | 22 |  |  |  |  |
| ATV9x0D30M3x | 30 | NSX160 NA DC PV 4P | LV438160 | 1000 | 160 |
| ATV9x0D37M3x | 37 |  |  |  |  |
| ATV9x0D45N4x | 45 | NSX200 NA DC PV 4P | LV438250 | 1000 | 190 |
| ATV9x0D55M3x | 55 | NSX400 NA DC PV 4P | LV438300 | 1000 | 400 |
| ATV9x0D75M3x | 75 |  |  |  |  |

## Line chokes

Additional line chokes are required in some configuration (see section "Drives fed by DC terminals").

| Drives 400 V / 480 V |  |  | External lines chokes |  | Integrated DC chokes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Power rating <br> kW | Catalog <br> reference | Group | Inductance <br> mH | Reference | Inductance |
| 0.75 | ATV9x0U07N4(x) | A1 | - | - | 21.6 |
| 1.5 | ATV9x0U15N4(x) | A1 | 10.0 | VW3A4551 | 11.5 |
| 2.2 | ATV9x0U22N4(x) | A1 | 4.0 | VW3A4552 | 8.10 |
| 3 | ATV9x0U30N4(x) | A1 | 4.0 | VW3A4552 | 5.80 |
| 4 | ATV9x0U40N4(x) | A1 | 4.0 | VW3A4552 | 4.55 |
| 5.5 | ATV9x0U55N4(x) | A1 | 2.0 | VW3A4553 | 3.40 |
| 7.5 | ATV9x0U75N4(x) | A1 | 2.0 | VW3A4553 | 2.90 |
| 11 | ATV9x0D11N4(x) | A1 | 1.0 | VW3A4554 | 2.25 |
| 15 | ATV9x0D15N4(x) | A1 | 1.0 | VW3A4554 | 1.52 |
| 18.5 | ATV9x0D18N4(x) | A1 | 0.50 | VW3A4555 | 1.18 |
| 22 | ATV9x0D22N4(x) | A1 | 0.50 | VW3A4555 | 1.00 |
| 30 | ATV9x0D30N4(x) | A2 | 0.50 | VW3A4555 | 0.760 |
| 37 | ATV9x0D37N4(x) | A2 | 0.30 | VW3A4556 | 0.585 |
| 45 | ATV9x0D45N4(x) | A2 | 0.30 | VW3A4556 | 0.490 |
| 55 | ATV9x0D55N4(x) | A2 | 0.30 | VW3A4556 | 0.365 |
| 75 | ATV9x0D75N4(x) | A2 | 0.30 | VW3A4556 | 0.310 |
| 90 | ATV9x0D90N4(x) | A2 | 0.155 | VW3A4558 | 0.226 |
| 110 | ATV9x0C11N4(x) | A2 | 0.120 | VW3A4559 | 0.160 |
| 132 | ATV9x0C13N4(x) | A2 | 0.098 | VW3A4560 | 0.160 |
| 160 | ATV9x0C16N4(x) | A2 | 0.066 | VW3A4561 | 0.160 |
| 220 | ATV9x0C22N4(x) | A2 | 0.049 | VW3A4562 | 0.105 |
| 250 | ATV9x0C25N4(x) | A2 | 0.049 | VW3A4562 | 0.095 |
| 315 | ATV9x0C31N4(x) | A2 | 0.038 | VW3A4564 | 0.069 |


| Drives 200 V / 240 V 3-phase |  |  | External lines chokes |  | Integrated DC chokes |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Power rating |  |  |  |  |  |
| kW | Catalog <br> reference | Group | Inductance <br> mH | Reference | Inductance |
| 0.75 | ATV9x0U07M3(x) | A1 | - | - | 6.45 |
| 1.5 | ATV9x0U15M3(x) | A1 | 4.0 | VW3A4552 | 3.5 |
| 2.2 | ATV9x0U22M3(x) | A1 | 4.0 | VW3A4552 | 2.55 |
| 3 | ATV9x0U30M3(x) | A1 | 2.0 | VW3A4553 | 1.85 |
| 4 | ATV9x0U40M3(x) | A1 | 2.0 | VW3A4553 | 1.47 |
| 5.5 | ATV9x0U55M3(x) | A1 | 1.0 | VW3A4554 | 1.27 |
| 7.5 | ATV9x0U75M3(x) | A1 | 1.0 | VW3A4554 | 1.52 |
| 11 | ATV9x0D11M3(x) | A1 | 0.50 | VW3A4555 | 1.0 |
| 15 | ATV9x0D15M3(x) | A1 | 0.50 | VW3A4555 | 0.52 |
| 18.5 | ATV9x0D18M3(x) | A1 | 0.50 | VW3A4555 | 0.52 |
| 22 | ATV9x0D22M3(x) | A1 | 0.30 | VW3A4556 | 0.52 |
| 30 | ATV9x0D30M3(x) | A2 | 0.30 | VW3A4556 | 0.265 |
| 37 | ATV9x0D37M3(x) | A2 | 0.155 | VW3A4558 | 0.226 |
| 45 | ATV9x0D45M3(x) | A2 | 0.155 | VW3A4558 | 0.226 |
| 55 | ATV9x0D55M3(x) | A2 | 0.155 | VW3A4558 | 0.160 |
| 75 | ATV9x0D75M3(x) | A2 | 0.150 | VW3A4557 | 0.160 |
|  |  |  |  |  |  |

## External soft-charge circuit for drives of groups x2

The soft-charge circuit of the internal main capacitors is not operating on these drives when they are supplied by the DC terminals. Drives of group A2 and B2 sharing the DC bus with other drives must always use the additional external soft-charge circuit described below:


## ATV9x0 settings

The drive's internal function to perform the soft-charge function must be used in the following way:

The parameter "dCo" (DC charging assign.) must be configured. The factory setting of this parameter is "no". It must be set to one of the possible options depending on the drive features to drive the contactor KM1:

- "r2...r3" if one of the internal relays is used,
- "r4...r6" if the relay output option module is used,
- "dol1...dol2" if the I/O extension module is used, in this case verify the maximum voltage and current data of the I/Os and the characteristics of the contactor coil.

The parameter "dCt" (DC bus charge time) must be set to the value listed in the table below.

For more details, see ATV9x0 programming manual in section "DC bus supply".

## Contactor KM1

A standard 3-poles AC contactor sized according AC-1 specification can be used. The peak current in the contacts occurs when the contactor is switched on at the end of the charge. The time to charge is defined to be greater than 7 time the time constant, which leads to a remaining voltage difference less than 1 V .
The control voltage of the coil must be within 12 Vdc to 48 Vdc and up to 250 Vac in order to be driven by one of the drives' relay outputs.

The 3 poles are wired in parallel to flow the DC current as shown on the schematics above. In this configuration, the total current is 2.25 times the rated current of the contactor defined for AC-1 coordination.
The length of the wire going through the contactor is integrated in the maximum length between two drives and therefore must be as short as possible. The +DC wire and the -DC wire must be kept parallel as much as possible to get a low leakage inductance in order to avoid overvoltage on the DC bus during operation.

## Resistor R

The charge resistor $R$ is selected in the standard braking resistors listed in ATV9x0 catalog. The reference depends on the drive rating as shown in the table below.
There are no constraints on the length of the wires from the resistor's terminals to the contactor (shown in black on the drawing above).

| Drive reference $400 / 480 \mathrm{~V}$ | Resistor R |  | ATV9x0 parameter | Contactor KM1 according to AC-1 coordination |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Value ( $\Omega$ ) | Ref. | Value (s) | Ref. | Rated current (A) | Current (3 poles in //) (A) |
| ATV9x0D30N4 | 28 | VW3A7732 | 0.5 | LC1D25•• | 40 | 90 |
| ATV9x0D37N4 | 28 | VW3A7732 | 0.5 | LC1D32•• | 50 | 112 |
| ATV9x0D45N4 | 28 | VW3A7732 | 0.6 | LC1D40•• | 60 | 135 |
| ATV9x0D55N4 | 16 | VW3A7733 | 0.6 | LC1D65•• | 90 | 180 |
| ATV9x0D75N4 | 16 | VW3A7733 | 0.6 | LC1D80•• | 125 | 281 |
| ATV9x0D90N4 | 16 | VW3A7733 | 0.8 | LC1D80•• | 125 | 281 |
| ATV9x0C11N4 | 16 | VW3A7733 | 1.1 | LC1D115•• | 200 | 450 |
| ATV9x0C13N4 | 16 | VW3A7733 | 1.1 | LC1D115•• | 200 | 450 |
| ATV9x0C16N4 | 16 | VW3A7733 | 1.1 | LC1D115•• | 200 | 450 |
| ATV9x0C22N4 | 10 | VW3A7734 | 1.0 | LC1F150•• | 250 | 562 |
| ATV9x0C25N4 | 10 | VW3A7734 | 1.0 | LC1F225•• | 315 | 709 |
| ATV9x0C31N4 | 8 | VW3A7735 | 1.2 | LC1F330•• | 400 | 900 |


| Drive reference <br> $200 / 240 ~ V$ | Resistor R |  |  | ATV9x0 <br> parameter <br> "dCt" | Contactor KM1 according to AC-1 coordination |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Value ( $\Omega$ ) | Ref. | Value (s) | Ref. | Rated current (A) | Current (3 poles in //) (A) |
| ATV9x0D15M3 | 28 | VW3A7732 | 0.8 | LC1D25•• | 40 | 90 |
| ATV9x0D18M3 | 28 | VW3A7732 | 1.0 | LC1D32•• | 50 | 112 |
| ATV9x0D22M3 | 28 | VW3A7732 | 1.2 | LC1D40•• | 60 | 135 |
| ATV9x0D30M3 | 16 | VW3A7733 | 1.3 | LC1D65•• | 80 | 180 |
| ATV9x0D37M3 | 16 | VW3A7733 | 1.3 | LC1D80•• | 125 | 281 |
| ATV9x0D45M3 | 16 | VW3A7733 | 1.5 | LC1D80•• | 125 | 281 |
| ATV9x0D55M3 | 16 | VW3A7733 | 1.1 | LC1D115•• | 200 | 450 |
| ATV9x0D75M3 | 16 | VW3A7733 | 1.1 | LC1D115•• | 200 | 450 |

## Switch disconnector

If a DC switch-disconnector is used, it must be located as shown on the drawing above in order to disconnect the external soft charge circuit from the DC bus when the switch is opened.
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## Wiring Options

## Wiring blocks

| Type |  |  |  |
| :--- | :--- | :--- | :--- |
| Pass-through 1-pole 1x1 terminal block | NSYTRV102 | NSYTRV162 | NSYTRV352 |
| Jumper to connect 2 blocks | NSYTRAL102 | NSYTRAL162 | NSYTRAL352 |
| Rated current at 690 V | 54 A | 73 A | 126 A |
| Maximum current at 1000 V | 76 A | 101 A | 125 A |
| Cable cross section capability | $0.5-16 \mathrm{~mm}^{2}$ | $1.5-25 \mathrm{~mm}^{2}$ | $1.5-50 \mathrm{~mm}^{2}$ |



