



*From lab to production,  
providing a window into the process*



# Practical Rheology

## LCR 7001 Capillary Rheometer

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Proprietary & Confidential

# Outline

1. Introduction
2. Shear Sweep Test (Polymer Flow Behavior )
3. Rabinowicz and Bagley Corrections
4. Extensional Viscosity Measurements
5. Wall Slip Velocity Calculation
6. Time Sweep Test (Thermal Stability of Polymers )
7. Die Swell Measurements
8. MFR Correlation
9. Intrinsic Viscosity of PET
10. LCR Dies Information



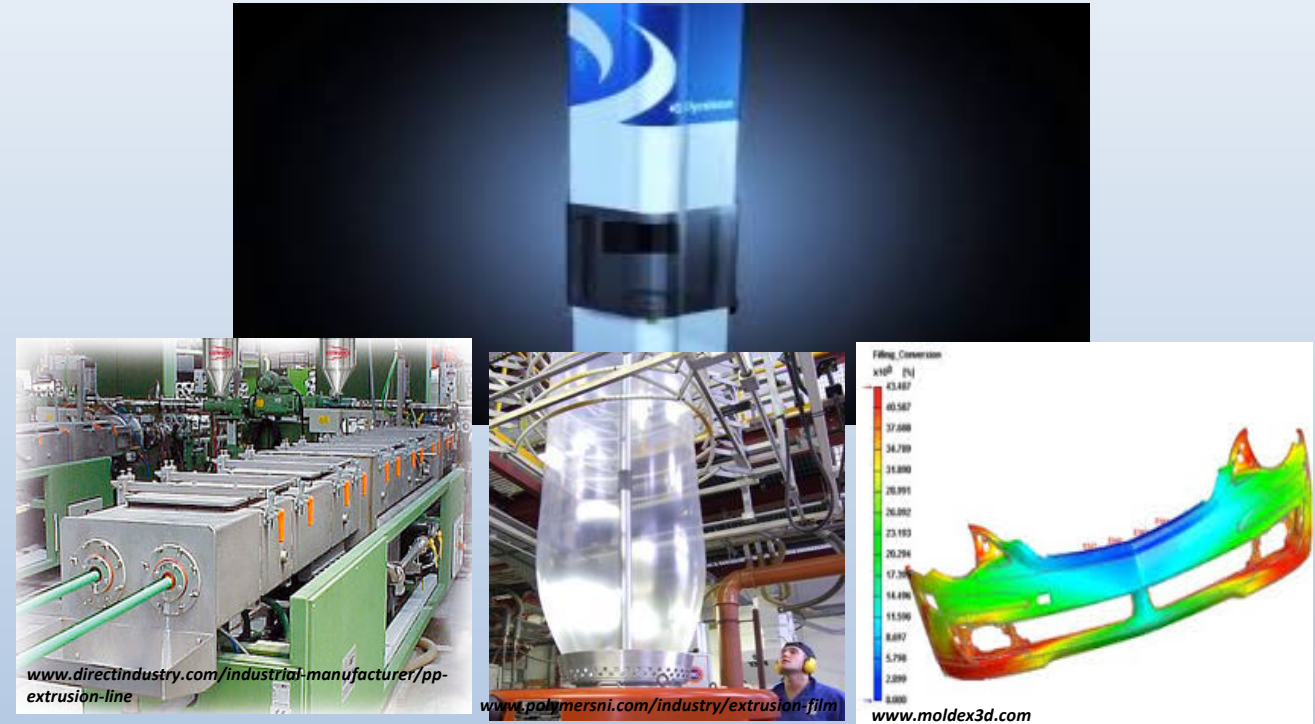
*From lab to production,  
providing a window into the process*



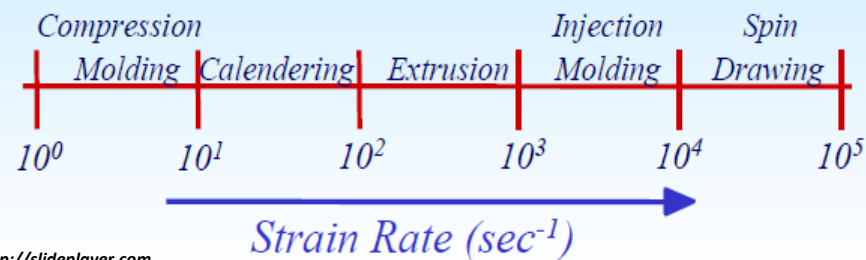
# Introduction

# Why Capillary Rheometer?

- ❖ The most common melt rheometer to analyze flow behavior of polymers under processing condition (shear rate, time, temperature).
- ❖ Duplication of processing parameters for design, simulation, and trouble shooting purposes in a faster way.
- ❖ Predict optimal operating condition based on correlation of rheological data from capillary rheometer to processing parameters.
- ❖ Analyze different materials for various applications and design.



## ***SHEAR RATES ENCOUNTERED IN PROCESSING***



<http://slideplayer.com>

## **APPLICATIONS**

- ✓ Polymer viscosity at wide deformation rate range
- ✓ Polymer melt flow behavior
- ✓ Shear thinning behavior
- ✓ Polymer stability over time/temperature
- ✓ Elastic properties (die swell, wall slip)



# Dynisco® LCR 7001

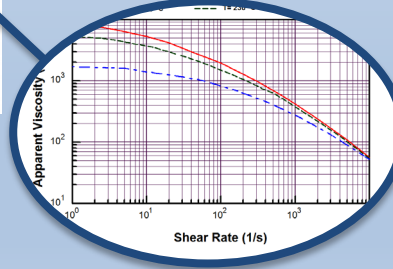
Force measurements  
from Load Cell



Pressure measurement  
from Pressure Transducer



RESULTS:  
Polymer flow curve  
(LabKars Software)



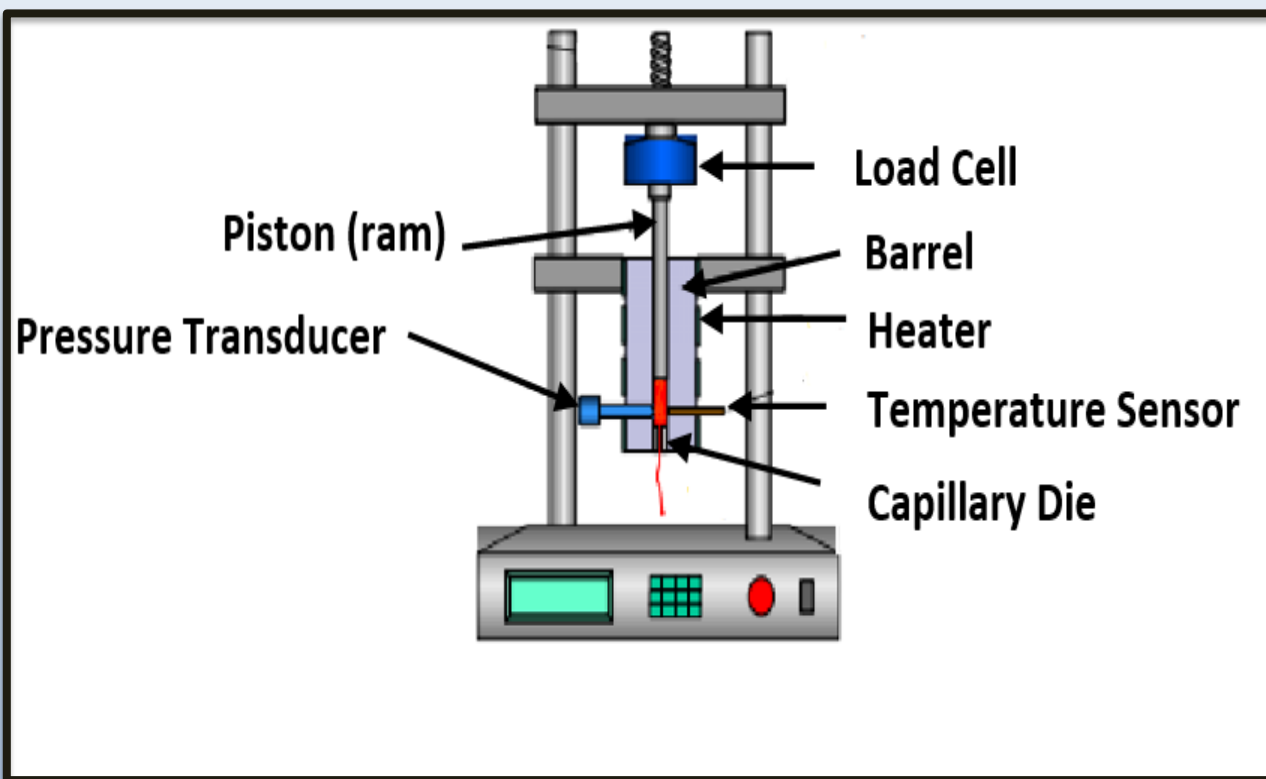
## ❖ MEASURES:

- ✓ Force
- ✓ Pressure
- ✓ Ram rate
- ✓ Time
- ✓ Temperature
- ✓ Expansion of extrudate

## ❖ CALCULATES:

- ✓ Shear stress
- ✓ Shear rate
- ✓ Shear/extensional Viscosity
- ✓ Die swell ratio

# General Specification

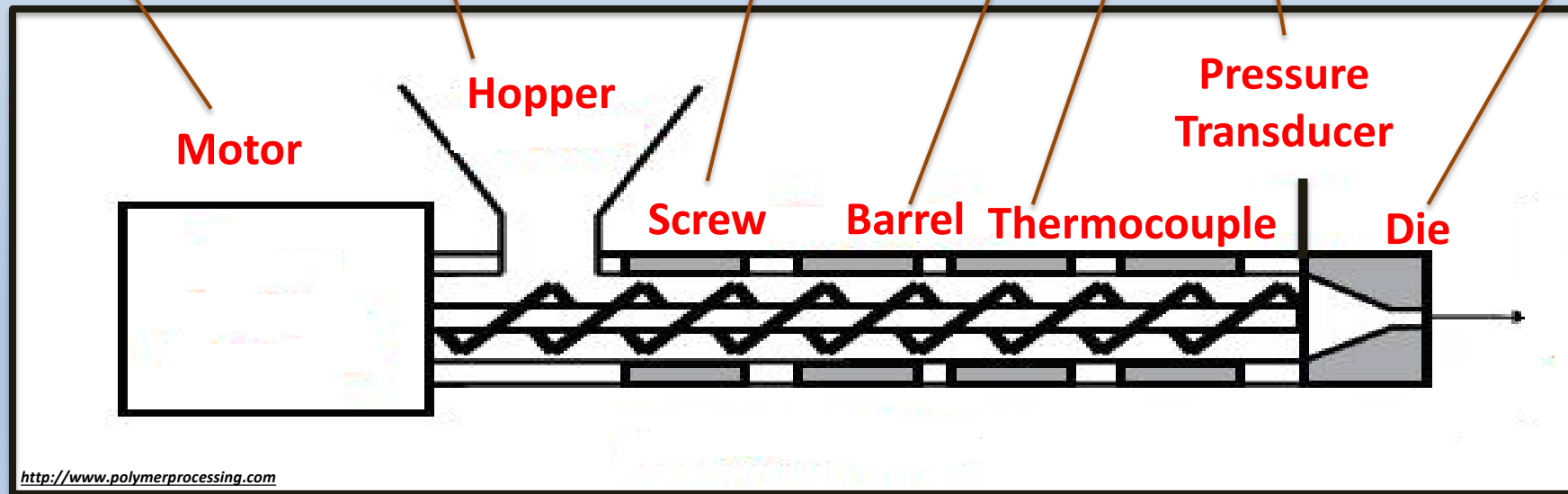
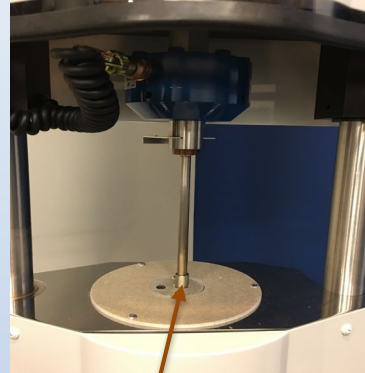
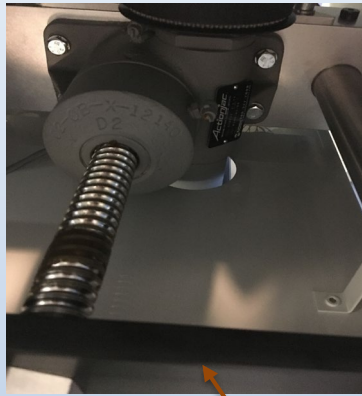


Based on **ASTM-D3835** "Standard Test Method for Determination of Properties of Polymeric Materials by Means of a Capillary Rheometer"

## ❖ LCR7001 SPECIFICATION

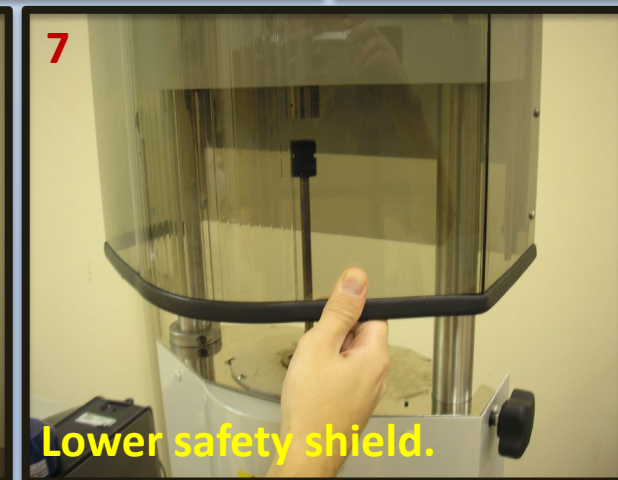
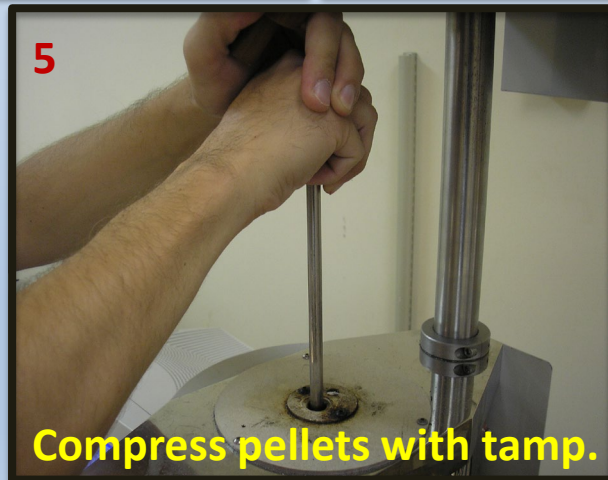
- ✓ Temp range: 25-500 °C
- ✓ Shear rate range: 1-100000 1/s
- ✓ Barrel diameter: 9.55 mm
- ✓ Available length: 227 mm
- ✓ Working length: 125 mm
- ✓ Min piston speed: 0.03 mm/min
- ✓ Max piston speed: 650 mm/min
- ✓ Max force measurement from load cell: 10 KN
- ✓ Max pressure measurements: 1400 Bar
- ✓ Accuracy of test-to-test~1.5-2%
- ✓ Accuracy of rheometer-to-rheometer~8%

# Extrusion & Capillary Rheometer



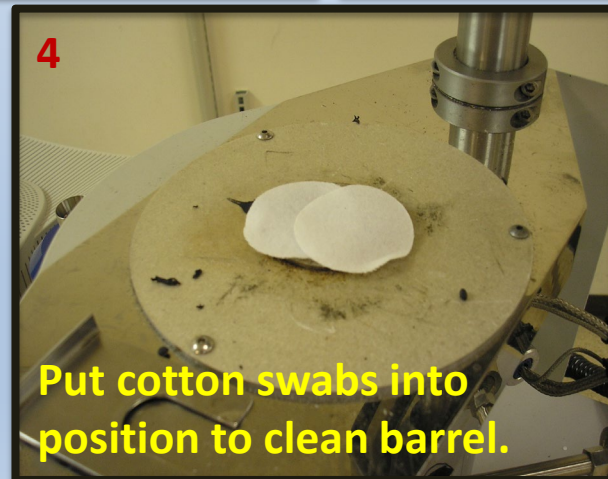


# LCR Preparation Before Running the Test





# LCR Cleaning After the Test

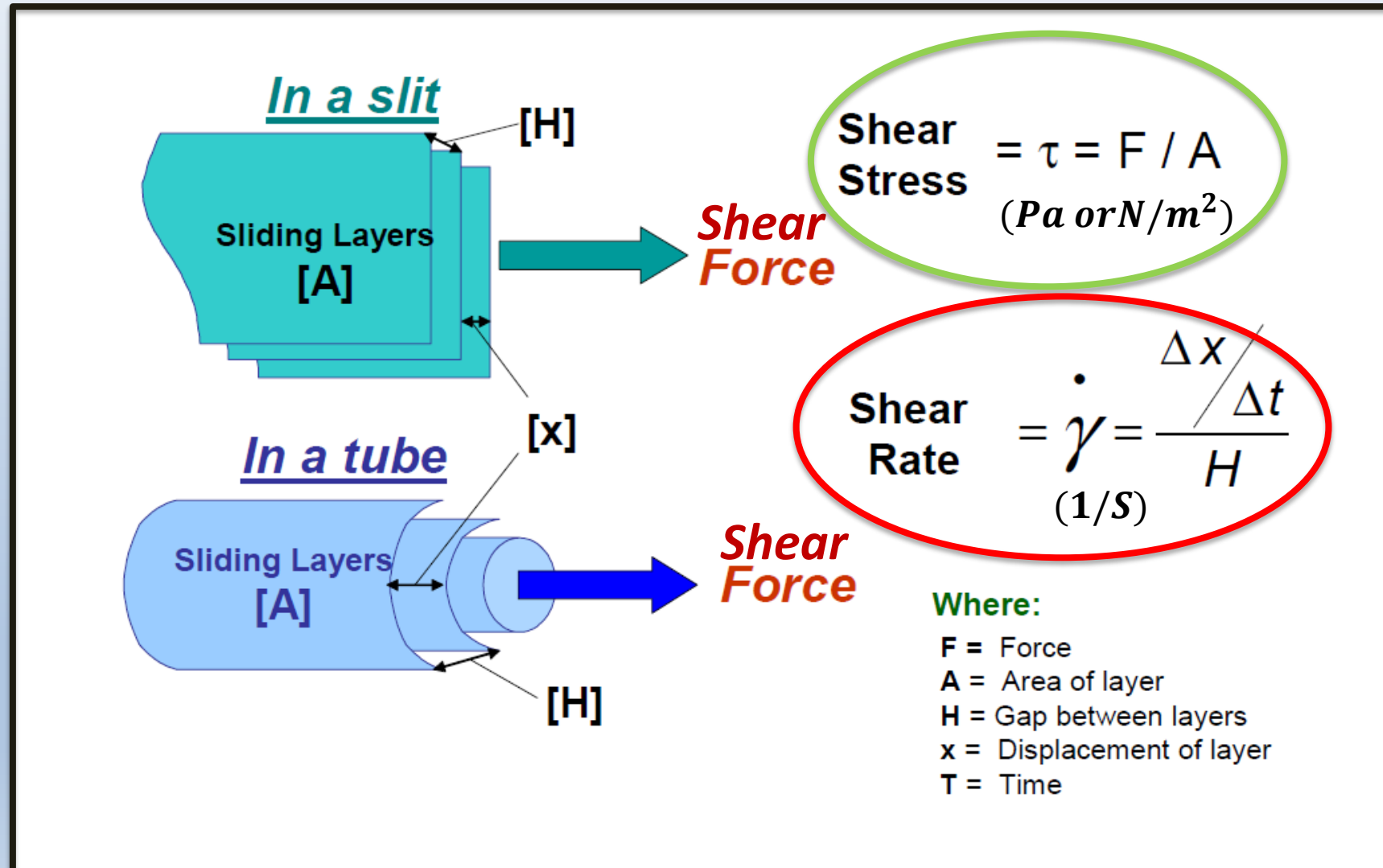




# Shear Sweep Test

(Polymer Flow Behavior)

# What is Shear?

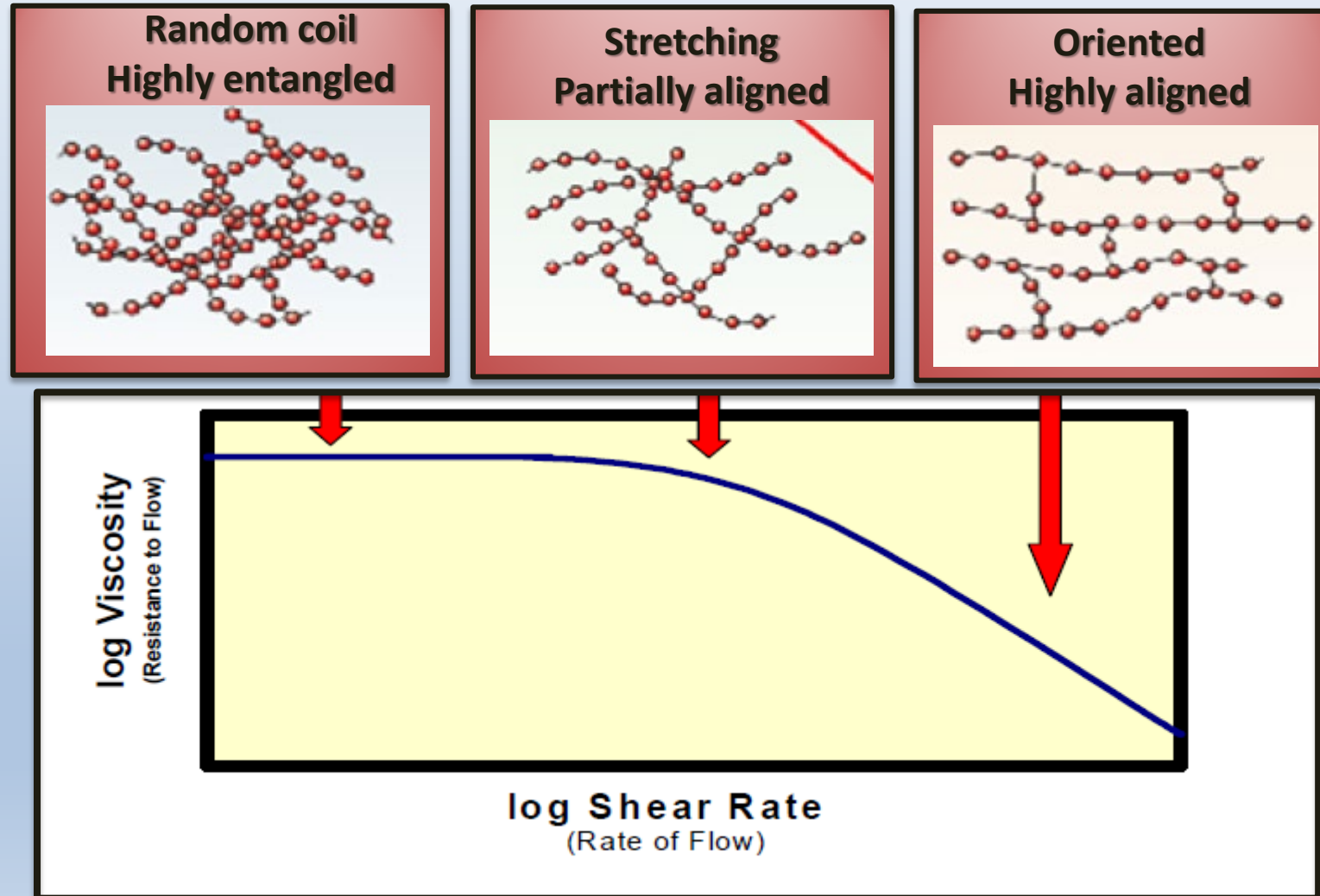




# Calculation of Rheological Data in LCR

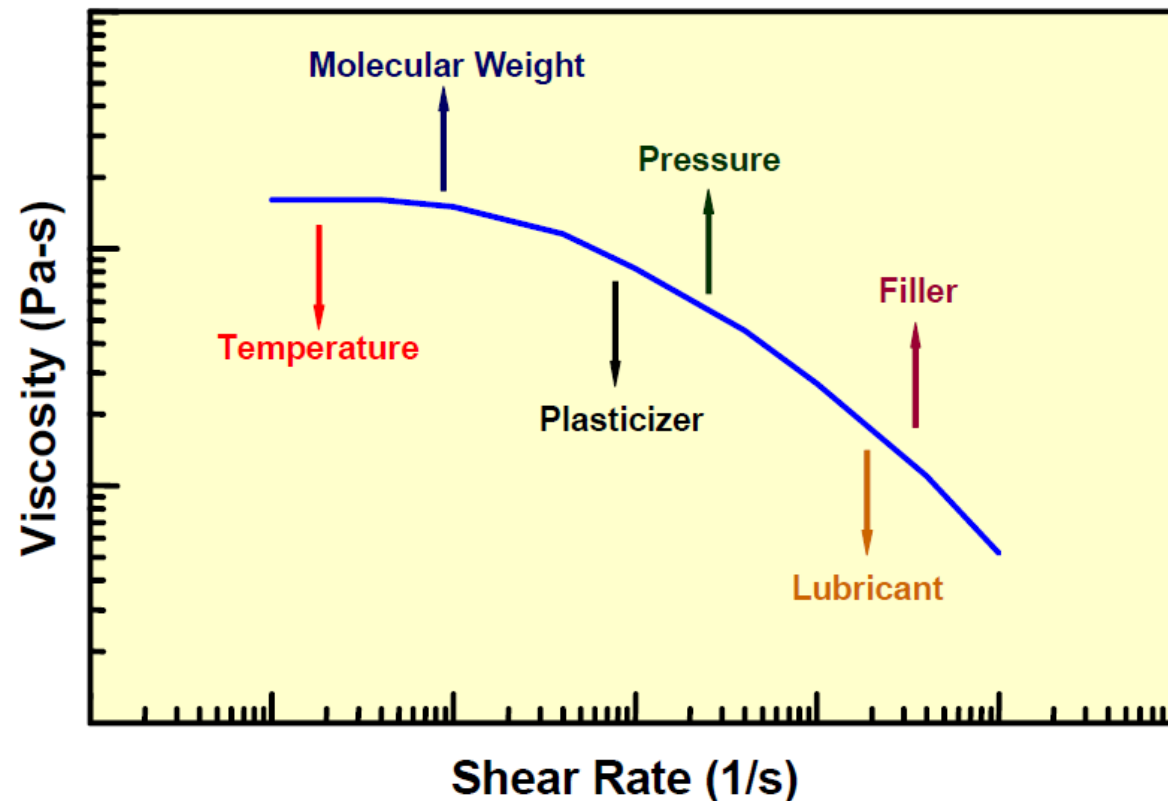
|                                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |
|--------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <p><b>Apparent shear rate<br/>(based on piston speed)</b></p>            | $\diamond \dot{\gamma}_a = \frac{4Q}{\pi R_c^3}$ $\diamond Q = S \left( \frac{\pi D_b^2}{4} \right)$ <ul style="list-style-type: none"> <li>➤ <math>\dot{\gamma}_a (1/s)</math>: apparent shear rate</li> <li>➤ <math>Q (mm^3/sec)</math>: volumetric flow rate</li> <li>➤ <math>S (mm/min)</math>: piston speed</li> <li>➤ <math>D_b (mm)</math>: barrel diameter</li> <li>➤ <math>R_c (mm)</math>: die radius</li> </ul>                                                             |
| <p><b>Wall shear stress<br/>(based on force or driving pressure)</b></p> | $\diamond \tau_w = \frac{F / \pi D_b^2}{4(L/D)_{die}}$ $\diamond \tau_w = \frac{P}{4(L/D)_{die}}$ <ul style="list-style-type: none"> <li>➤ <math>\tau_w (Pa)</math>: wall shear stress</li> <li>➤ <math>F (N)</math>: force from “load cell” on piston</li> <li>➤ <math>D_b (mm)</math>: barrel diameter</li> <li>➤ <math>L/D</math>: length to diameter ratio of the die</li> <li>➤ <math>P_d (Pa)</math>: driving pressure at the die entrance from “pressure transducer”</li> </ul> |
| <p><b>Apparent shear viscosity</b></p>                                   | $\diamond \eta_a = \frac{\tau_w}{\dot{\gamma}_a}$ <ul style="list-style-type: none"> <li>➤ <math>\eta_a (Pa-s)</math>: apparent shear viscosity</li> <li>➤ <math>\tau_w (Pa)</math>: wall shear stress</li> <li>➤ <math>\dot{\gamma}_a (1/s)</math>: apparent shear rate</li> </ul>                                                                                                                                                                                                    |

# Shear Flow in Viscoelastic Polymer Melts



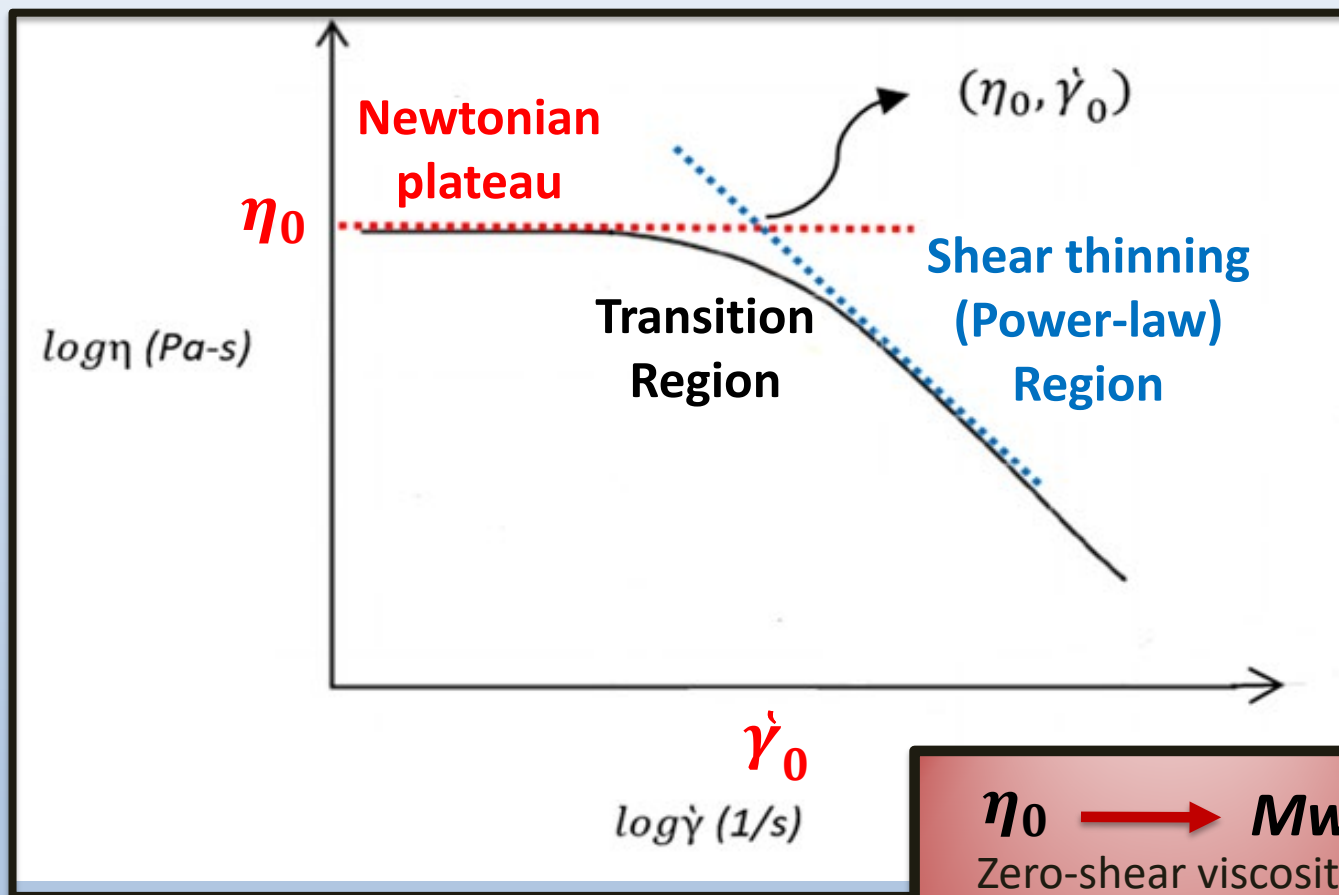
# Effect of Various Factors on Polymer Flow Curve

## How an Increase in Various Factors Affects the Polymer Melt Viscosity Curve



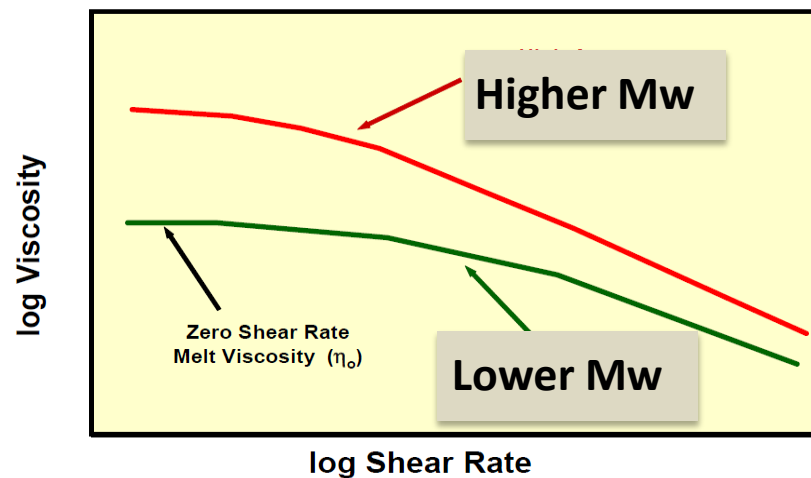
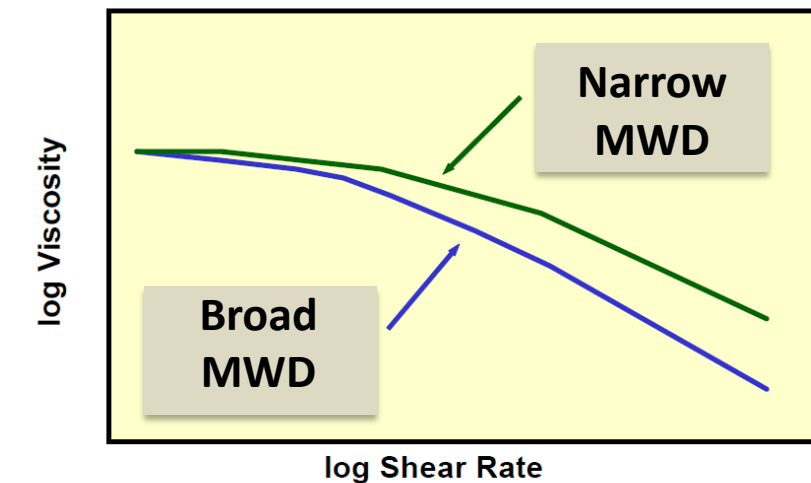


# Flow Curve of Polymer Melts



$\eta_0 \longrightarrow Mw$   
Zero-shear viscosity

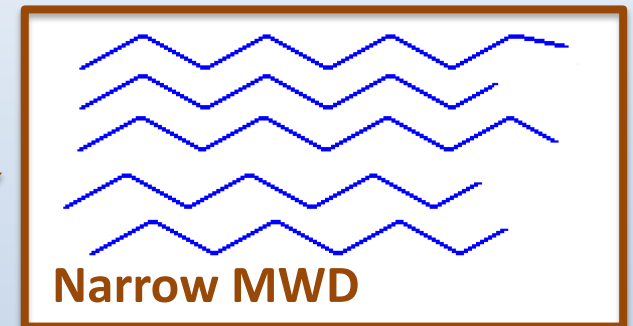
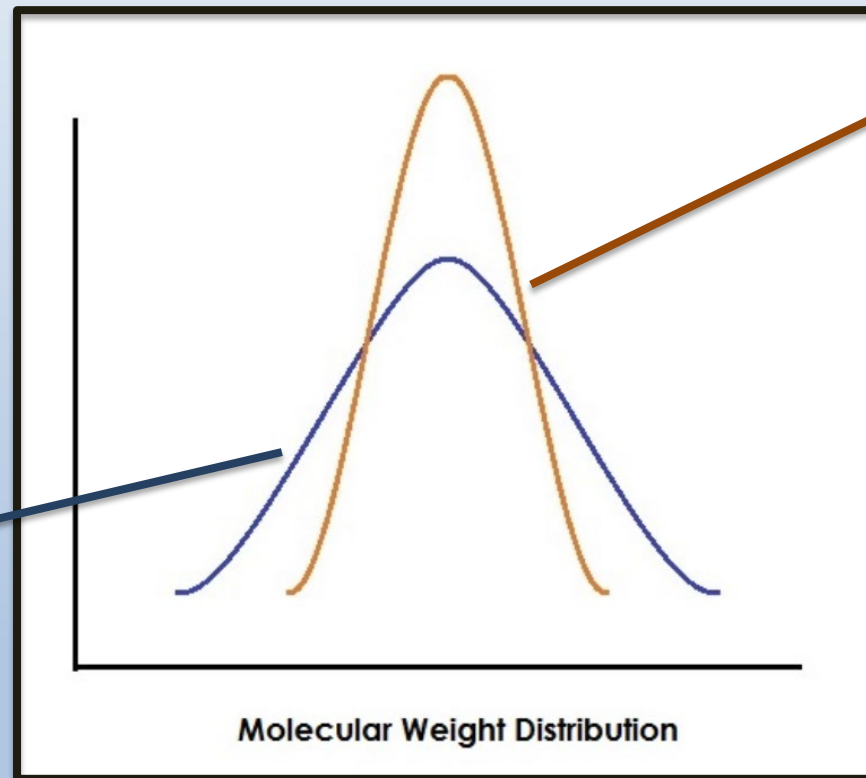
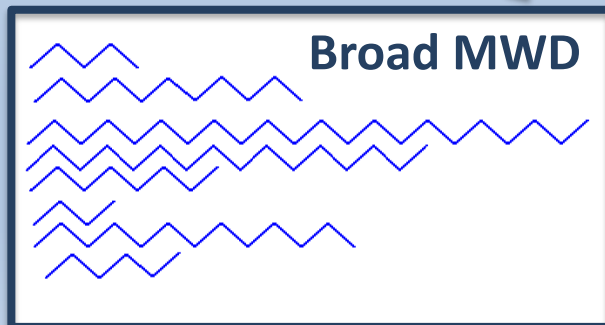
$\dot{\gamma}_0 \longrightarrow MWD$   
Characteristic shear rate



# Molecular Weight Distribution (MWD)

## Polymers with Broader MWD:

- Better processability (fluidity)
- Less viscous dissipation during their process
- Less energy consumption during their process
- Lower mechanical properties



# Analyzing Polymer Degradation from Flow Curve

## Extrusion Condition

Heat

➤ Barrel temp

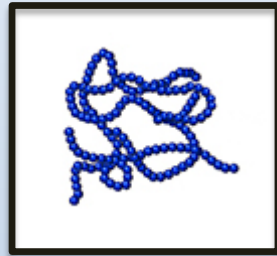
Mechanical shear

➤ Screw speed

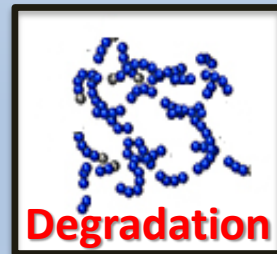
Residence time

➤ Flow rate

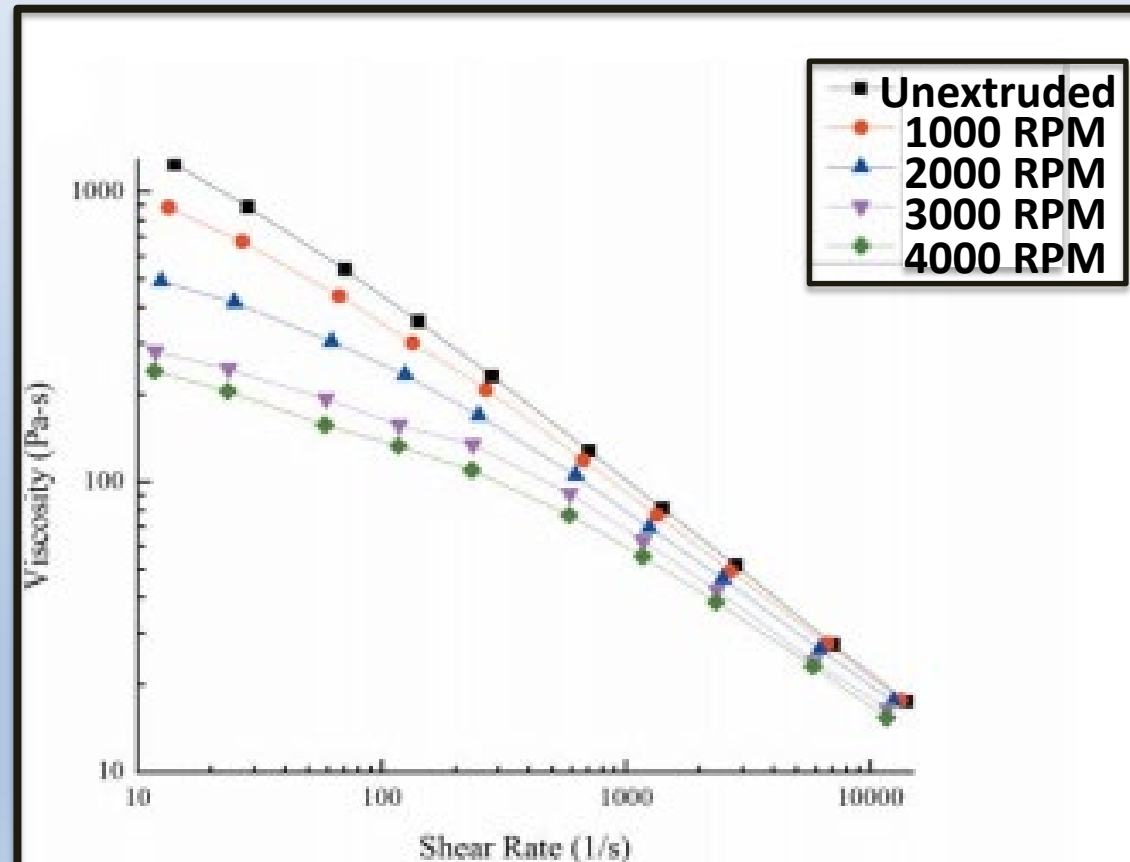
Higher  $\eta_0$  and  $M_w$



Lower  $\eta_0$  and  $M_w$



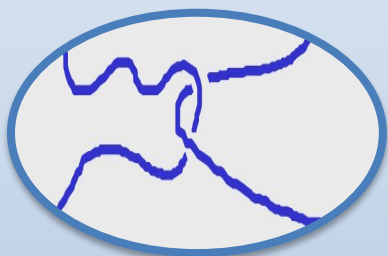
Flow curve of plastic samples before process and after process at various screw speeds in an extrusion



Farahanchi, A., Malloy, R., Sobkowicz, M.J. (2016), *Polymer Engineering & Science* 56: pp. 743-751

# Mw Dependence of Zero-Shear Viscosity

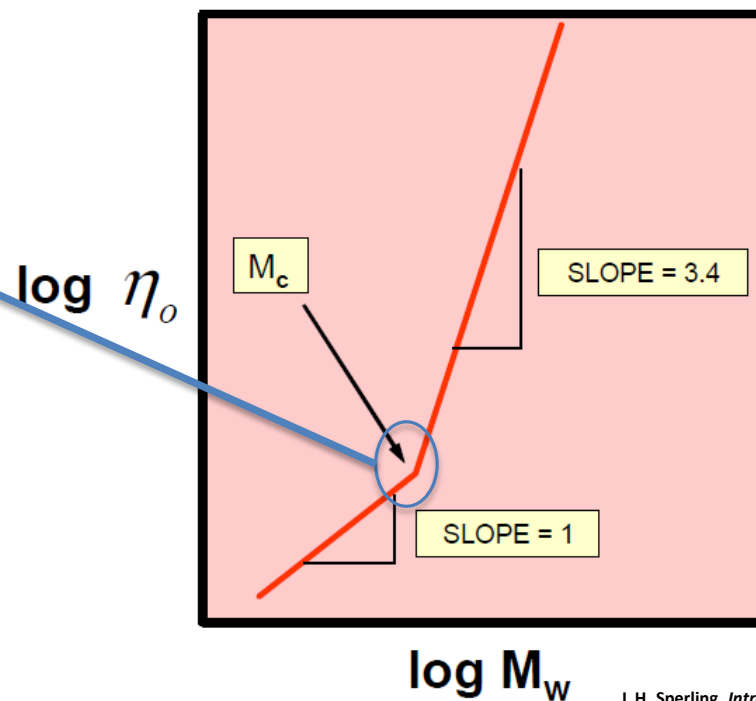
*Critical Molecular wt. ( $M_c$ )*  
molecular entanglements occur



Polymers with higher Mw:

- ✓ Higher intermolecular entanglement
- ✓ Higher strength
- ✓ Higher chemical resistance

## Relationship of the Molecular Weight to Melt Viscosity



Fox-Flory Equation

$$\eta_0 = K_2 (M_w)^{3.4}$$

Where:

$\eta_0$  = "Zero shear rate"  
melt viscosity.

$K_2$  = Constant

$M_w$  = Wt. avg. molecular wt.

$M_c$  = "Critical" molecular wt.

L.H. Sperling, *Introduction to Physical Polymer Science*, John Wiley & Sons, 4<sup>th</sup> Edition.

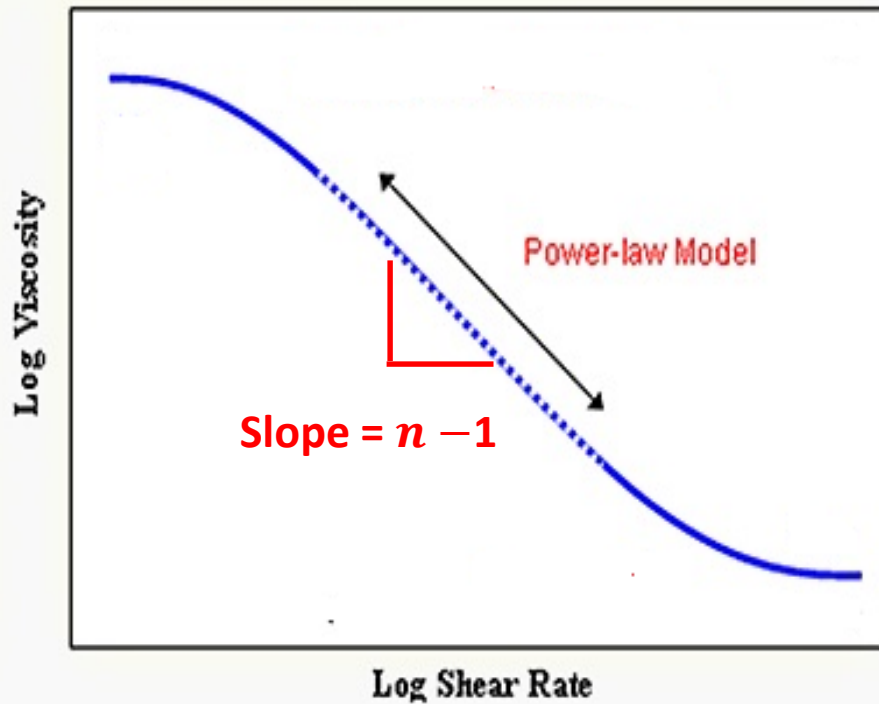


# Quantitative Relationships for the Dependence of Viscosity upon Shear Rate

## Power-law Model

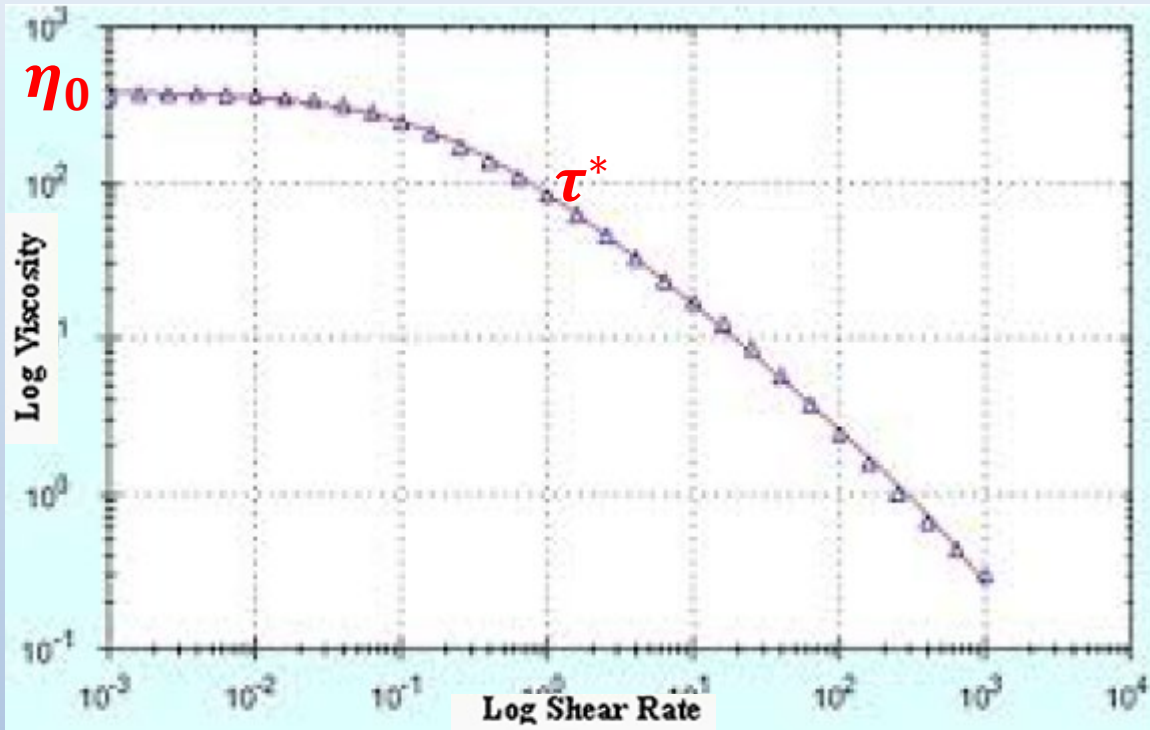
$$\eta(\dot{\gamma}) = k\dot{\gamma}^{n-1}$$

- $k$  (Pa-s): Consistency
- $n$ : Power-law index



- ❖ “Only” fits the shear-thinning (power-law) portion of the curve
- ❖ Shear-thinning exponents dependent on intermolecular forces.
- ❖  $n$  ranges from 0.2-0.9 depending upon the type of polymer.
- ❖  $n$  equals to 1 for Newtonian materials.
- ❖  $n$  represents the processability (shear-thinning intensity).
- ❖ Polymers with lower  $n$  are more sensitive to the shear rate.
- ❖  $n$  decrease with broader MWD.
- ❖  $k$  has temperature dependency and controlled by Mw.

# Quantitative Relationships for the Dependence of Viscosity upon Shear Rate



## Modified Cross Model

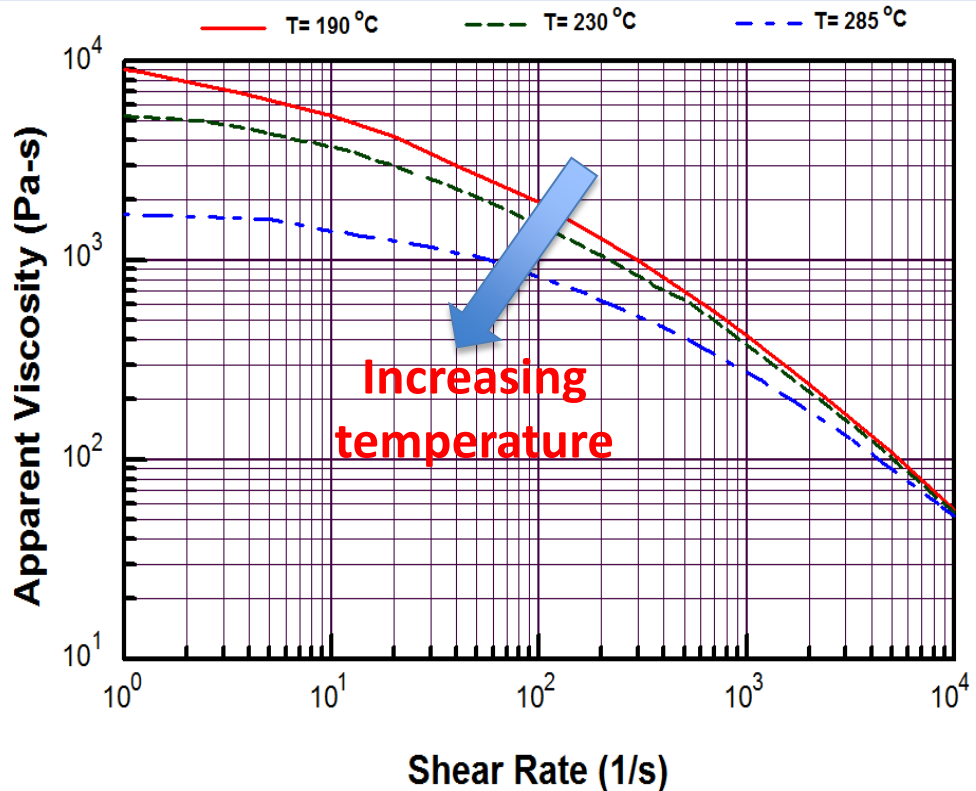
$$\eta(\dot{\gamma}) = \frac{\eta_0}{1 + \left(\frac{\eta_0 \dot{\gamma}}{\tau^*}\right)^{1-n}}$$

- $\eta_0$  (Pa-s): Zero-shear viscosity
- $\tau^*$  (Pa): Critical shear stress
- $n$ : Power-law index

- ❖ Combines the power-law and Newtonian regions.
- ❖ Also fits the low shear Newtonian plateau.
- ❖  $\eta_0$  is controlled by molecular weight.
- ❖  $\tau^*$  is stress at the beak in curve and controlled by MWD.
- ❖ Broader MWD (by blending or branching) cause earlier  $\tau^*$ .

# Viscosity-Temperature Dependence

## Window into the process



❖ Williams-Landel-Ferry (WLF) model: ( $T_g < T < T_g + 100$ )

$$\log(a_T) = \frac{\eta_0(T)}{\eta_0(T_{ref})} = \left[ \frac{-C_1(T - T_g)}{C_2 + T - T_g} \right]$$

$$C_1 = 17.44$$

$$C_2 = 51.6 \text{ K}$$

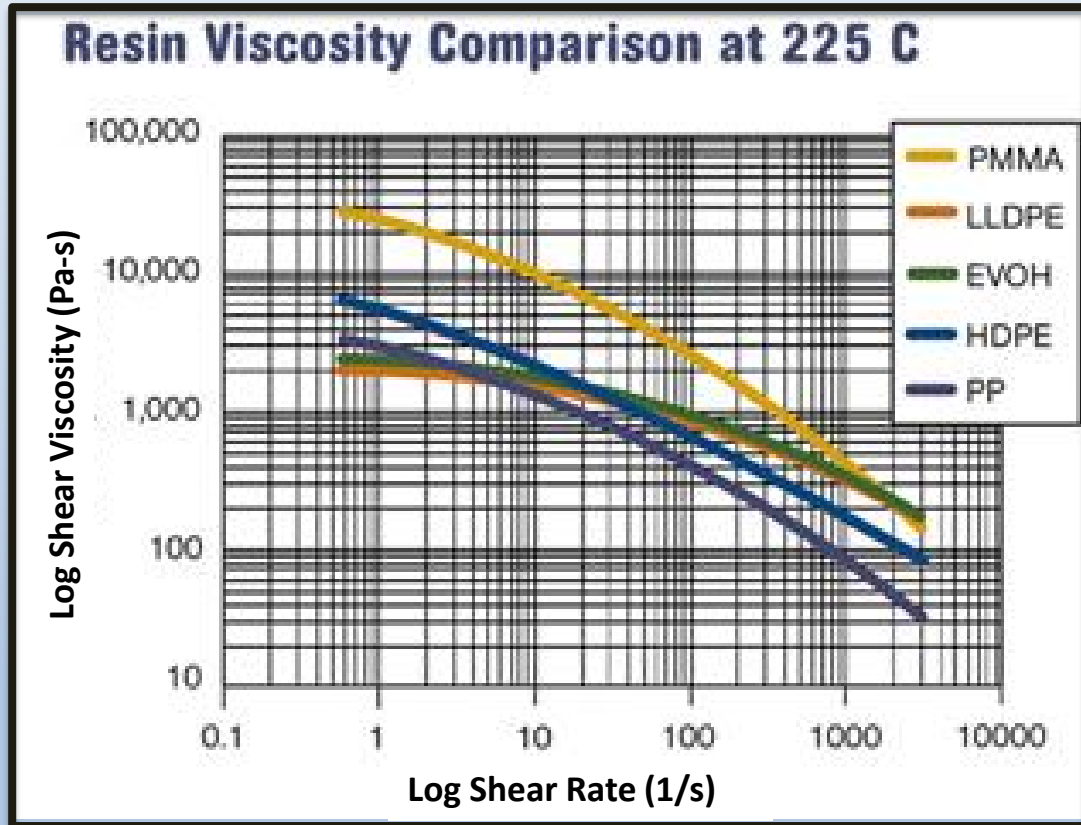
❖ Arrhenius model: ( $T > T_g + 100$ )

$$a_T = \frac{\eta_0(T)}{\eta_0(T_{ref})} = \exp\left[\frac{E_a}{R} \left(\frac{1}{T} - \frac{1}{T_{ref}}\right)\right]$$

$E_a$ : Activation Energy

$R$ : Universal gas constant =  $8.314 \times 10^{-3} \text{ kJ/mol.K}$

# A Window into Your Process!

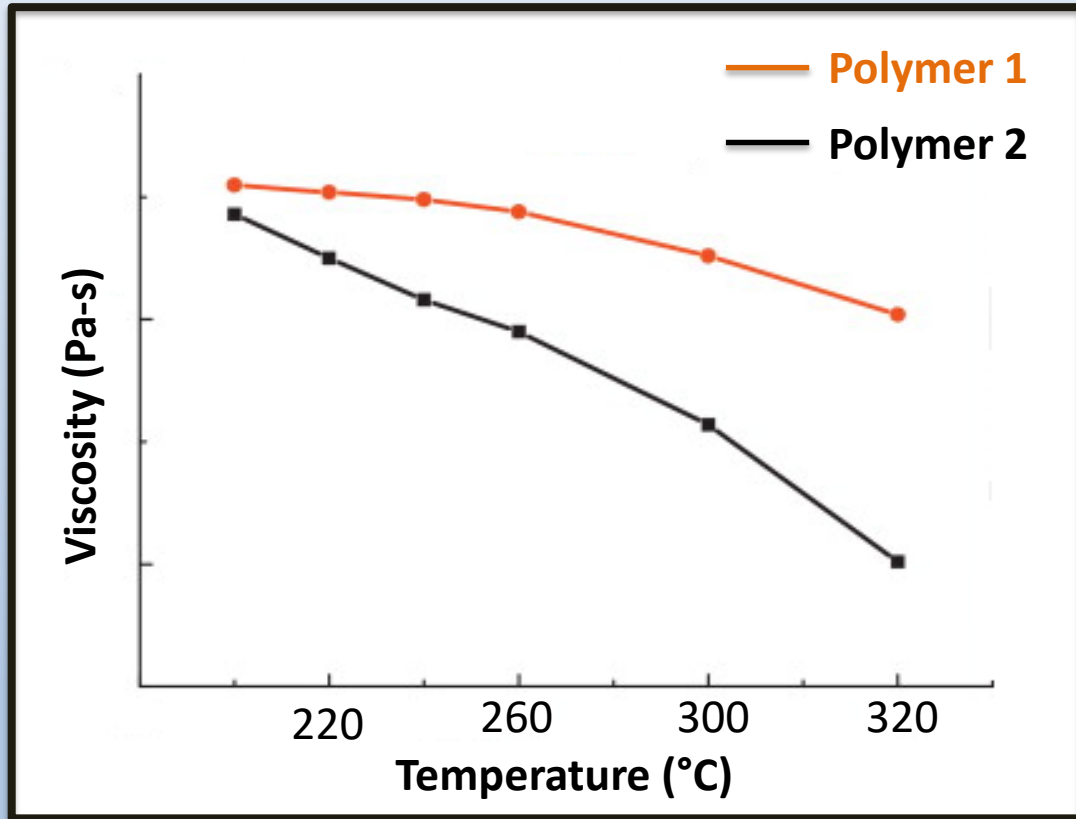


<https://www.ptonline.com/columns/how-to-spec-a-flat-die>

- At shear rate 100-1000 1/s (common at normal RPM in extrusion), the processing of which polymer cause higher torque and head pressure, and viscous heating in the extrusion?
- Which polymer has higher shear-thinning behavior (easier process-ability)?
- With increasing screw speed which polymer will have the highest flow rate?
- Which polymer has the highest molecular weight?
- Which polymer had the Broader MWD?
- Which polymer might have linear might have long chain-branching and which one might have linear structure?



# A Window into Your Process!



- Which polymer might face higher thermal degradation with increasing temperature?
- Which polymer has wider processing temperature?

# Shear-Sweep Test Setup in LabKars

Setup

◀ ▶ ⏪ ⏩ 🔍 ↺

2 3 4 Data Point Setup # 312 5 6 7

| Setup # | Program Name     | Start Pos. | Temperature | Melt Time | Sensor1 ID | Die      |
|---------|------------------|------------|-------------|-----------|------------|----------|
| 312     | Shear Rate Sweep | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 313     | PE Sweep         | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 314     | PE Stability     | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 315     | PE Stability II  | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 316     | PE Short         | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 317     | PE Long          | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 318     | PE Slip Small    | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 319     | PE Slip Large    | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 320     | PP Sweep         | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 321     | PP Stability     | 100        | 190         | 300       | LC-502N    | CX394-30 |

Control Mode  
☒ Rate ☐ Stress

Test Type  
☒ Steady State 9  
☐ Position (Acquire At - mm)  
☐ Manual  
☐ Time Delay (Acquire At - sec)  
☐ Elapse Time (Acquire At - sec)

8 Minimum Speed 0.03  
 Maximum Speed 650

◀ ▶ ⏪ ⏩ 🔍 ↺ 10 11

| Point # | Speed Control | Shear Rate | Delay Sec |
|---------|---------------|------------|-----------|
| 1       | 180.00        | 2189.04    | 0         |
| 2       | 124.22        | 1510.68    | 0         |
| 3       | 85.72         | 1042.47    | 0         |
| 4       | 59.16         | 719.47     | 0         |
| 5       | 40.82         | 496.43     | 0         |
| 6       | 28.17         | 342.59     | 0         |
| 7       | 19.44         | 236.42     | 0         |
| 8       | 13.42         | 163.21     | 0         |
| 9       | 9.26          | 112.61     | 0         |
| 10      | 6.39          | 77.71      | 0         |

Close

Add New Data Point Setup 1  
 Delete Last Data Point Setup

Export Test Definition  
 Import Test Definition

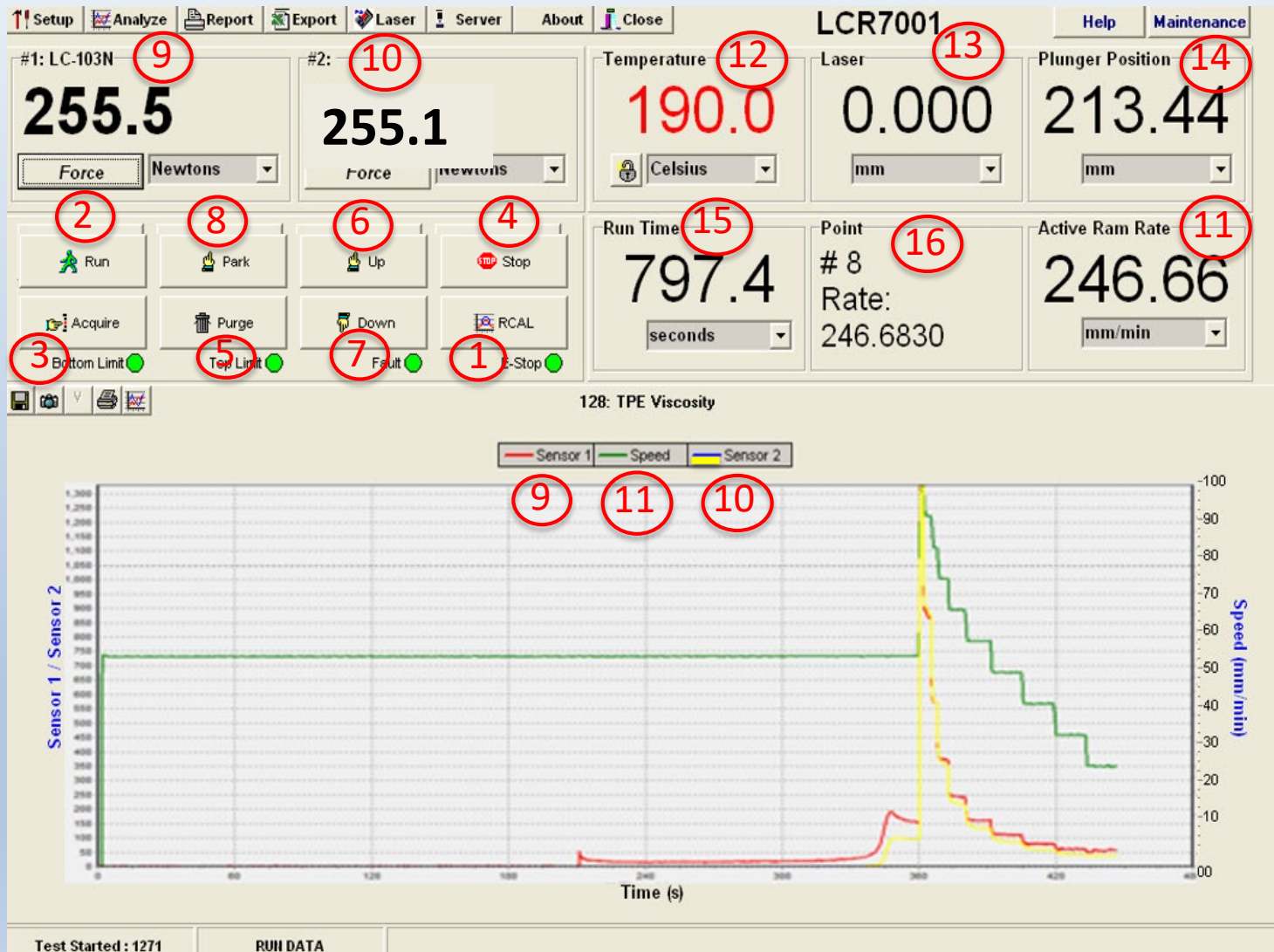
Generate Speed Control  
 Generate Shear Rate

Sweep Generation  
 Point Speed Control  
 Start: 1  
 End:   
☒ Value in Speed Control  
 Generate Method  
☒ Logarithmic  
☐ Linear  
 Auto Generate Points

➤ Send 12

1. Add/delete Data Point Setup
2. Program Name
3. Start Position (mm): 89-100 mm
4. Temperature (°C): barrel temperature set point
5. Melt time (sec): 180-360 sec
6. Sensor1 ID: LC-103N
7. Die: choose entrance angle, D and L/D from list
8. Minimum/Maximum Speed (mm/min):  
Min at 0.03 and Max at 650 mm/min
9. Data Acquisition mode:  
Steady state, Position, Time Delay, Manual
10. Speed Control range (mm/min)
11. Shear Rate range (1/s)
12. Send: sending test setup to rheometer

# LabKars Software (Control Screen)

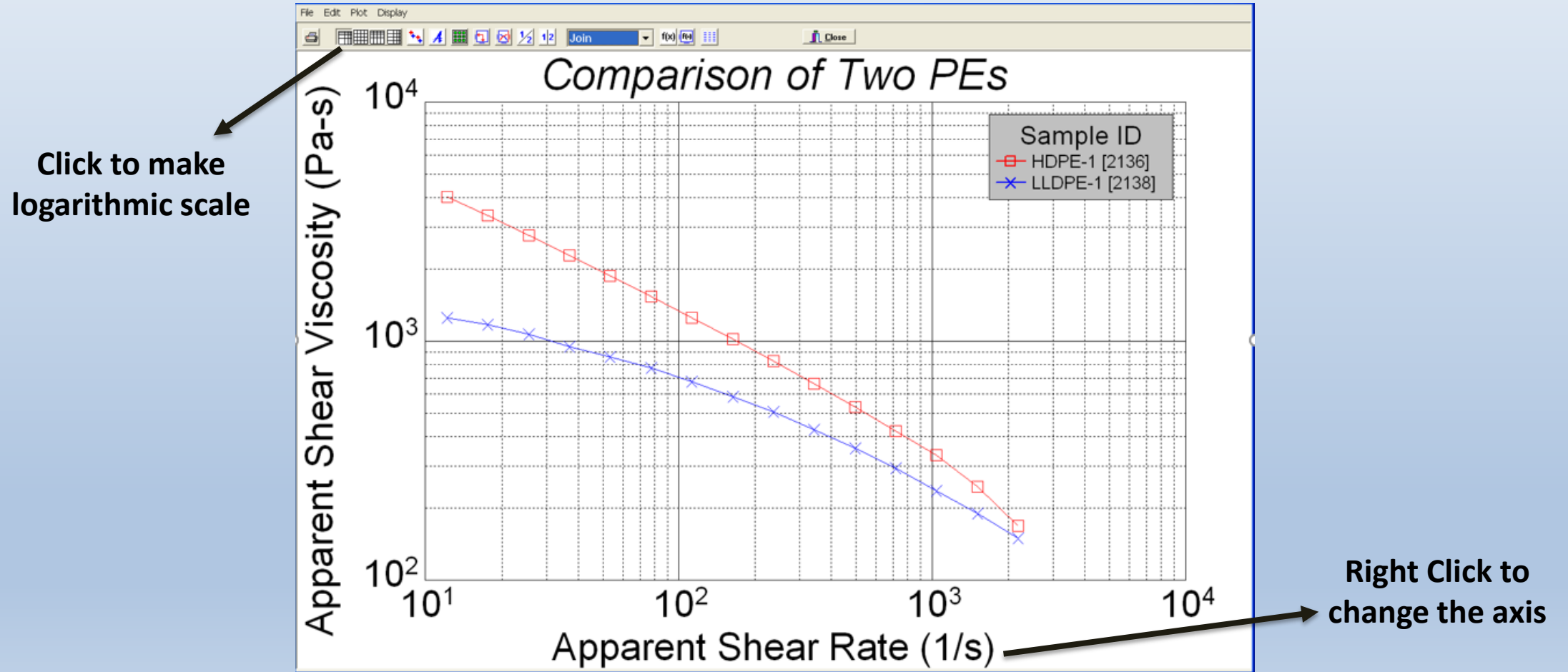


## Real-time data graph during the test

- RCAL:** balance transducers!
- Run:** run the test!
- Acquire:** collect data!
- Stop:** stop the test!
- Purge:** purge all the material in barrel!
- Up:** move plunger upward!
- Down:** move plunger downward!
- Park:** go to park position (25mm)!
- Sensor #1 (N):** force on load cell
- Sensor #2 (N):** force on pressure transducer
- Active Ram Rate (mm/min):** piston speed
- Temperature (°C):** actual barrel temperature
- Laser (mm):** die swell detection
- Plunger position (mm)**
- Run time (sec)**
- Collected point:** at each shear rate

# Data Analysis

## Plot of log apparent viscosity versus apparent shear rate

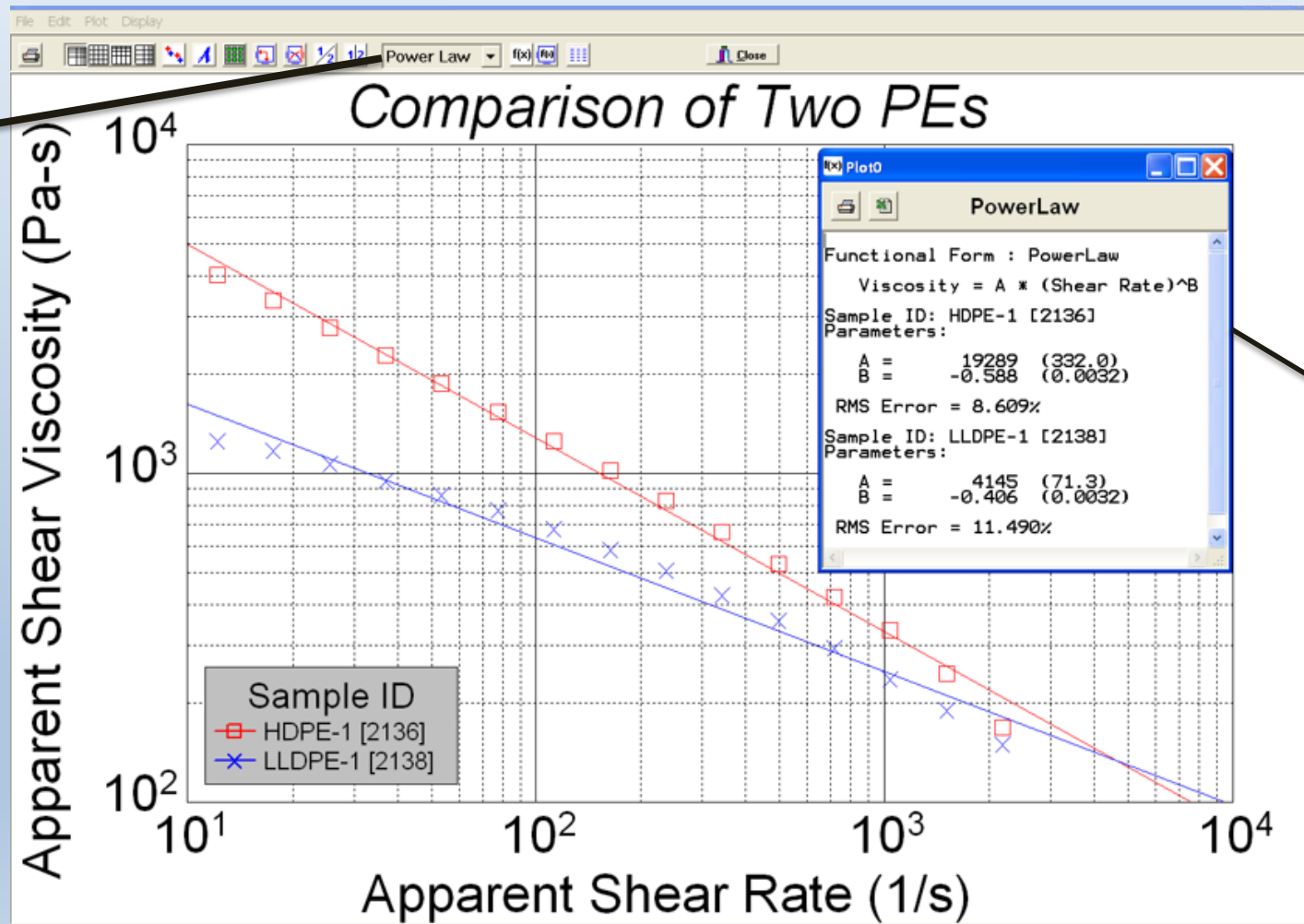




# Data Analysis

## Power-law model analysis

Choose  
"Power Law"

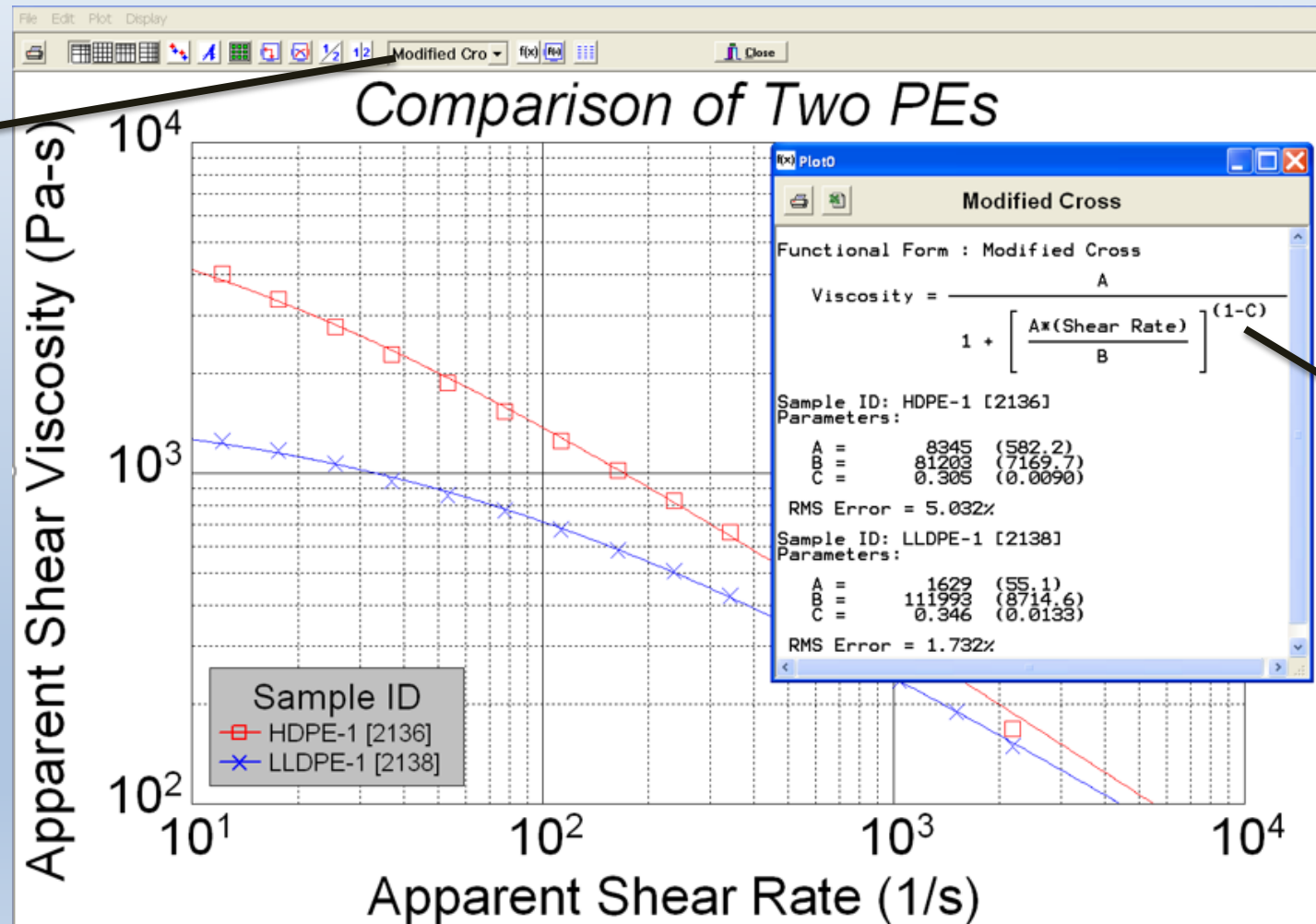


Power law  
fitting data

# Data Analysis

## Modified cross model analysis

Choose  
"Modified Cross"



Modified cross  
fitting data

# Raw Data in LabKars

Select "Single Run/Modify" to see the raw data

Select the type of sensor

- Sensor 1: Load cell
- Sensor2: Pressure transducer

Max, min, average, mean, and standard deviation information of all parameters

Raw data

**Dynisco Polymer Test - Analyze**

File Edit Plot

Print Plot Refresh Copy

Database Path: d:\PROGRA~1\LABKAR~2\Database

Database / Filters Single Run / Modify Interpolate Plot Table

Charge #: 1270

Points: 6

Operator: MC

Material: HDPE

Machine: 7001

Date: 09/10/2007 10:37 am

Die: CZ787-15

Comment: CZ787-15, CZ787-15

Sample ID: 2.5 N

Lot #: 9-10-07

Sensor 1: LC-103N

Sensor 2:

Melt Time: 300 s

RCal: 102.1 %

Melt Pause: 0 s

Temperature: 210 C

Start Position: 100 mm

Program Name: 127:F2LR

Select Report Type:

- ☒ Sensor 1
- ☐ Sensor 2
- ☐ Sensor 1 & 2

Printer Format:

- ☒ Portrait
- ☐ Landscape

Save Screen Settings

| Point | Sensor1 (N) | Pos (mm) | Ram (mm/min) | Time (sec) | Stress (Pa) | Rate (1/s) | Visc. (Pa-s) | Real Temp (C) | Delay Time |
|-------|-------------|----------|--------------|------------|-------------|------------|--------------|---------------|------------|
| 1     | 198         | 105      | 1.13         | 631.89     | 46139       | 1.72       | 26818.6      | 210           | 0          |
| 2     | 199         | 110      | 0.98         | 931.13     | 46281       | 1.49       | 31018.3      | 210           | 0          |
| 3     | 206         | 115      | 1.20         | 1229.09    | 47838       | 1.83       | 26183.8      | 210           | 0          |
| 4     | 930         | 140      | 61.27        | 1260.80    | 216402      | 93.29      | 2319.8       | 210           | 0          |
| 5     | 958         | 165      | 72.97        | 1282.65    | 222771      | 111.10     | 2005.1       | 209.8         | 0          |
| 6     | 962         | 190      | 80.80        | 1302.16    | 223761      | 123.01     | 1819.0       | 209.9         | 0          |

|          | Force   | Position | Ram rate | Time     | Stress     | Rate   | Viscosity |
|----------|---------|----------|----------|----------|------------|--------|-----------|
| Average: | 575.4   | 137.5    | 36.4     | 1106.3   | 133865     | 55.4   | 15027.4   |
| Max:     | 961.8   | 190.0    | 80.8     | 1302.2   | 223761     | 123.0  | 31018.3   |
| Min:     | 198.3   | 105.0    | 1.0      | 631.9    | 46139      | 1.5    | 1819.0    |
| Count:   | 6       | 6        | 6        | 6        | 6          | 6      | 6         |
| Mean:    | 575.377 | 137.508  | 36.392   | 1106.253 | 133865.300 | 55.406 | 15027.430 |
| St. Dev: | 410.315 | 34.177   | 39.153   | 269.850  | 95462.460  | 59.610 | 14315.950 |

# Export Raw Data in Excel

Capillary Rheometer Control Center

LCR 7001

#1: LC-103N Diff. #1-#2 9.9 #2: PT-142BAR

Temperature 200.0

Plunger Position 25.34

Ram Rate 0.00

Export to Excel

Switch Database Database Path: d:\PROGRA~1\LABKAR~2\Database

| Charge | DateTime            | Sample ID | Operator | Material | Lot                                | Die      | Die |
|--------|---------------------|-----------|----------|----------|------------------------------------|----------|-----|
| 1261   | 09/06/2007 01:17 pm | LDPE      | MC       | HDPE     | Low Stress First with intermediate | CX394-20 | CX3 |
| 1262   | 09/06/2007 01:51 pm | 2.5 N     | MC       | HDPE     | Low Stress First with intermediate | CX394-20 | CX3 |
| 1263   | 09/06/2007 03:52 pm | 2.5 N     | MC       | HDPE     | Low Stress First with intermediate | CX394-20 | CX3 |
| 1264   | 09/07/2007 09:17 am | 2.5 N     | MC       | HDPE     | 787 Die                            | CZ787-15 | CZ7 |
| 1265   | 09/07/2007 03:48 pm | 2.5 N     | MC       | HDPE     | 787 Die                            | CZ787-15 | CZ7 |
| 1266   | 09/07/2007 04:15 pm | 2.7 N     | MC       | HDPE     | 787 Die                            | CZ787-15 | CZ7 |
| 1267   | 09/10/2007 08:59 am | 2.7 N     | MC       | HDPE     | 9-10-07                            | CZ787-15 | CZ7 |
| 1268   | 09/10/2007 09:31 am | 2.7 N     | MC       | HDPE     | 9-10-07                            | CZ787-15 | CZ7 |
| 1269   | 09/10/2007 10:04 am | 2.5 N     | MC       | HDPE     | 9-10-07                            | CZ787-15 | CZ7 |
| 1270   | 09/10/2007 10:37 am | 2.5 N     | MC       | HDPE     | 9-10-07                            | CZ787-15 | CZ7 |

Starting Row #: 10 Export To: Single File Multiple Files Charge #: 1270

Status READY

Time (s)

Select  
"Export"

Select "Single  
File" to export  
the data in Excel

Choose your  
data set

Microsoft Excel - Sheet1

| CHARGE | DateTime        | SampleID | Operator | MatID | Lot       | ProgramID | ProgramName | Temperature | POINT | Time    | RamRate | Sensor1  | Sensor2 | Position | StarPosiv |
|--------|-----------------|----------|----------|-------|-----------|-----------|-------------|-------------|-------|---------|---------|----------|---------|----------|-----------|
| 1270   | 9/10/2007 10:37 | 2.5 N    | MC       | HDPE  | 9/10/2007 | 127       | FLIR        | 210         | 1     | 631.89  | 1.13    | 188.9148 | 0       | 105      | 100       |
| 1270   | 9/10/2007 10:37 | 2.5 N    | MC       | HDPE  | 9/10/2007 | 127       | FLIR        | 210         | 2     | 951.13  | 0.98    | 188.9332 | 0       | 110      | 100       |
| 1270   | 9/10/2007 10:37 | 2.5 N    | MC       | HDPE  | 9/10/2007 | 127       | FLIR        | 210         | 3     | 1229.09 | 1.2     | 205.8148 | 0       | 115      | 100       |
| 1270   | 9/10/2007 10:37 | 2.5 N    | MC       | HDPE  | 9/10/2007 | 127       | FLIR        | 210         | 4     | 1289.8  | 81.272  | 820.1331 | 0       | 140.02   | 100       |
| 1270   | 9/10/2007 10:37 | 2.5 N    | MC       | HDPE  | 9/10/2007 | 127       | FLIR        | 210         | 5     | 1283.65 | 72.974  | 867.6079 | 0       | 195.01   | 100       |
| 1270   | 9/10/2007 10:37 | 2.5 N    | MC       | HDPE  | 9/10/2007 | 127       | FLIR        | 210         | 6     | 1302.19 | 80.795  | 961.7663 | 0       | 190.02   | 100       |

Raw data in  
Excel sheet





*From lab to production,  
providing a window into the process*



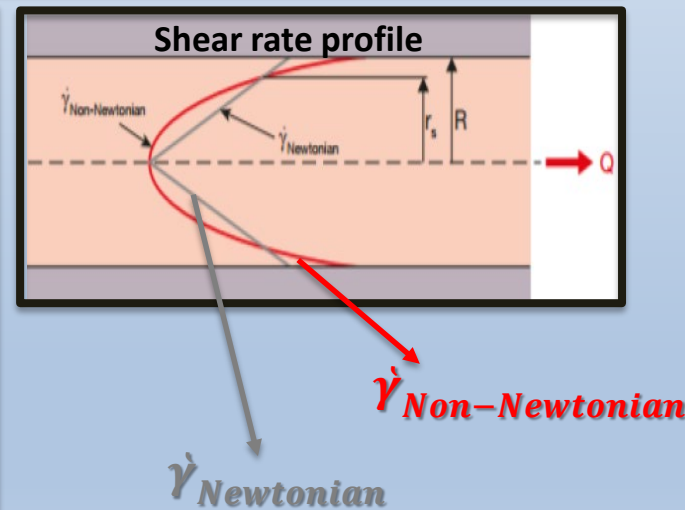
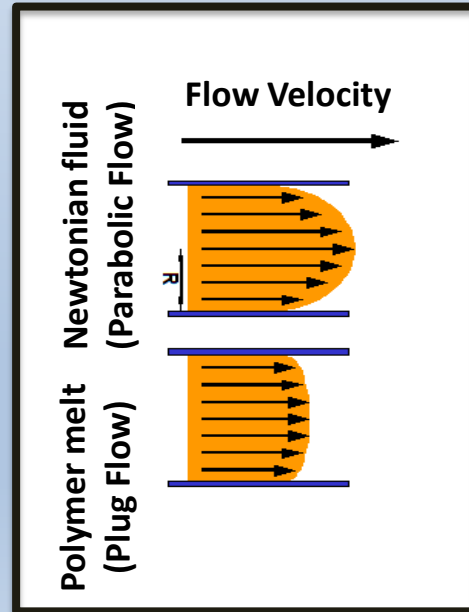
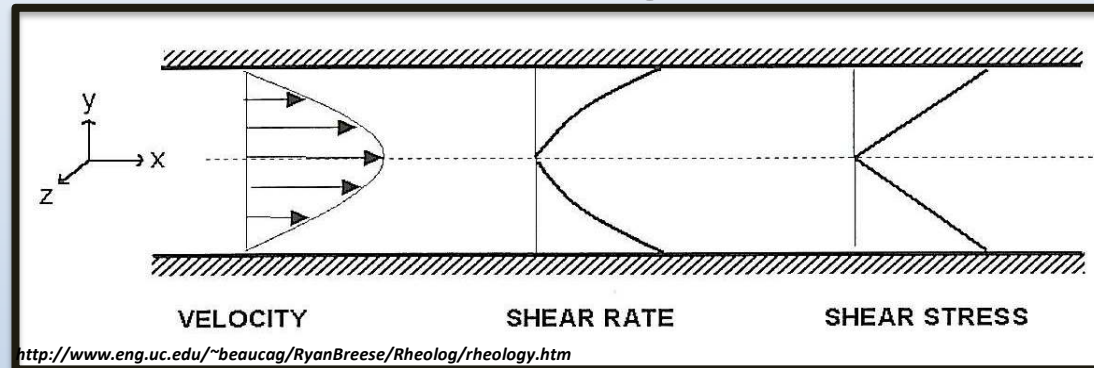
# Rabinowicz and Bagley Corrections

# Corrections

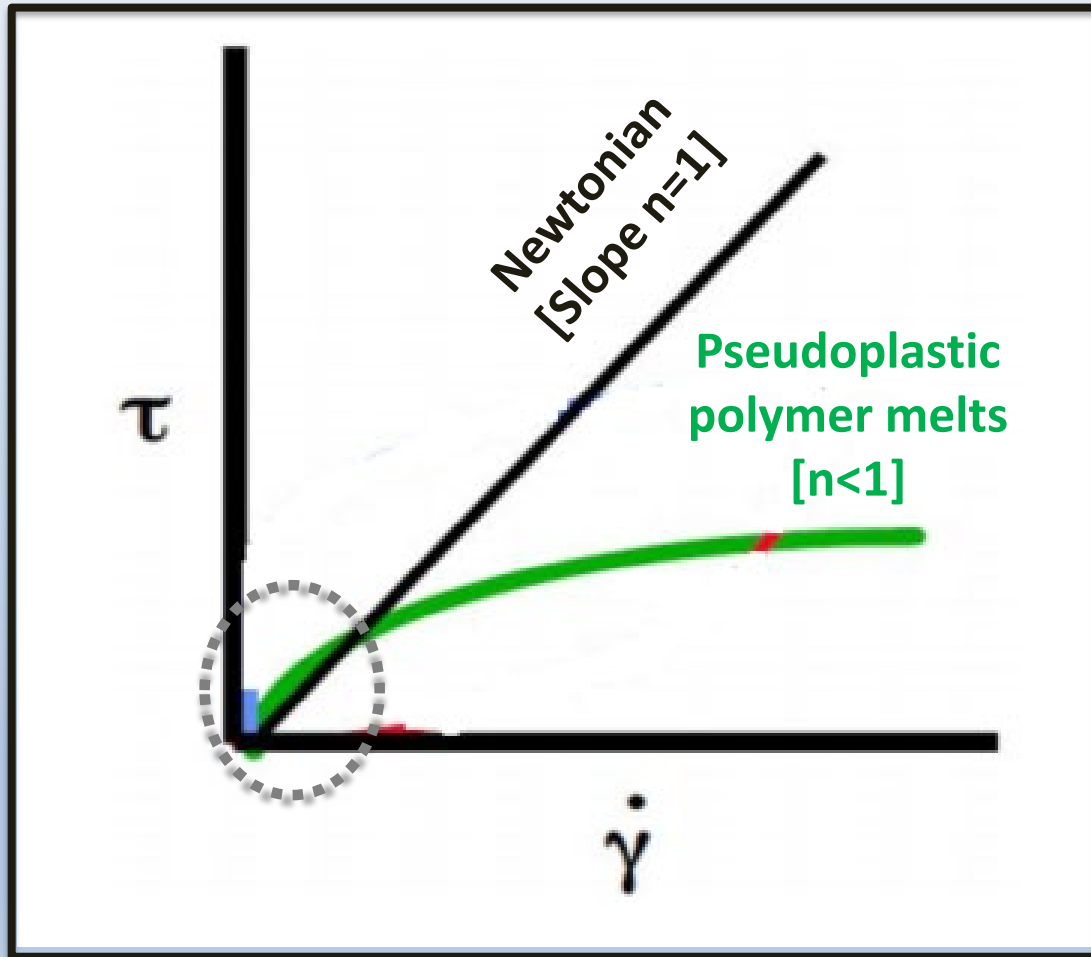
- ❖ All calculations we discussed are “Apparent” values since they assume Newtonian behavior and that the entire pressure drop occurs inside through die. (Assuming no die entrance/exit effect)
- ❖ **Rabinowicz correction** needs to be applied in order to rectify the data for non-Newtonian character of polymer melt. (Calculation of **corrected shear rate**)
- ❖ **Bagley correction** needs to be applied to consider the extra pressure drop that may happen at the entrance/exit of the die. (Calculation of **corrected shear stress**)

# Why Rabinowicz Corrections?

## Flow through a die



# Rabinowicz Corrections



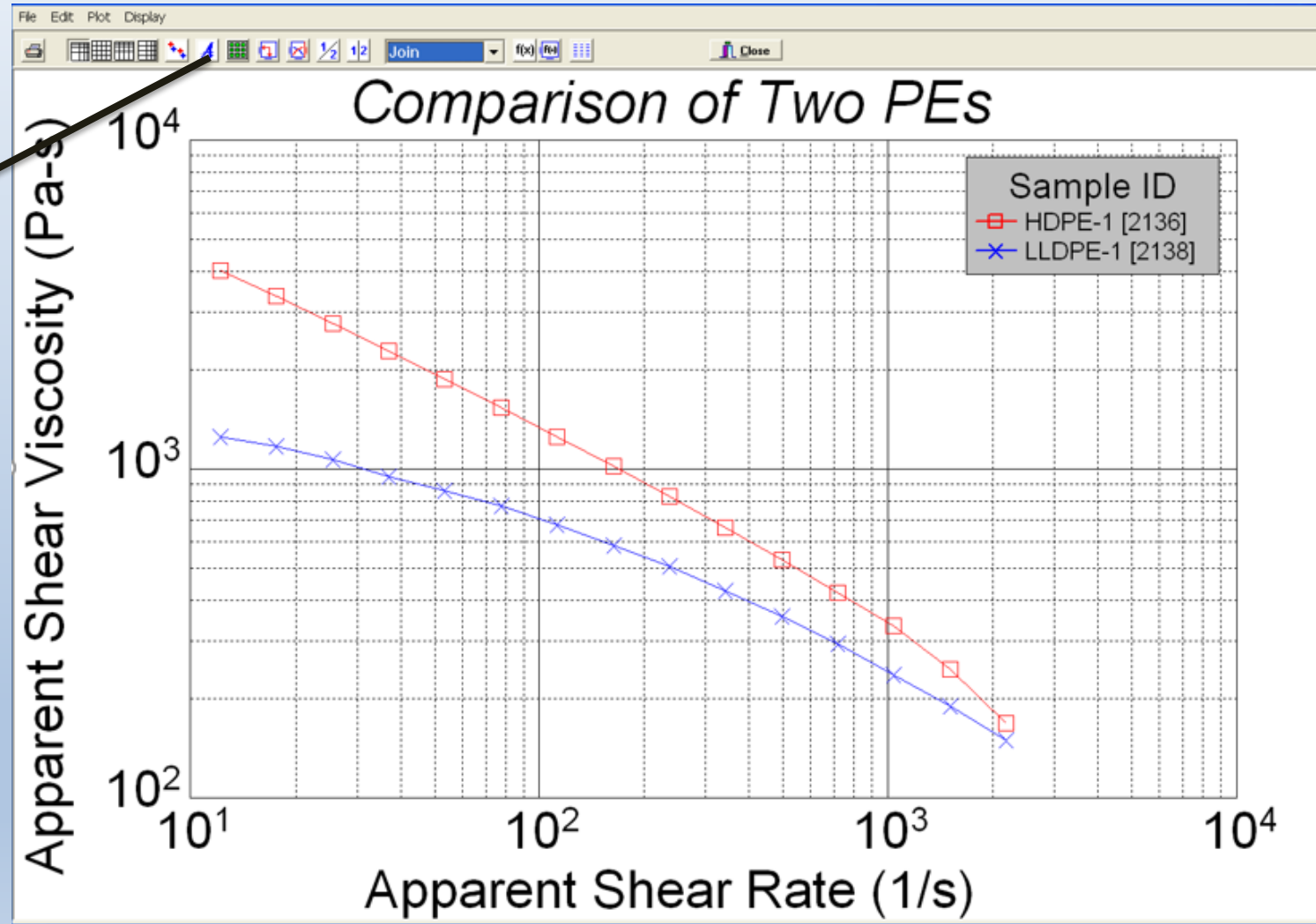
$$\dot{\gamma}_{corrected} = \left( \frac{3n + 1}{4n} \right) \dot{\gamma}_{apparent}$$

Correction Factor

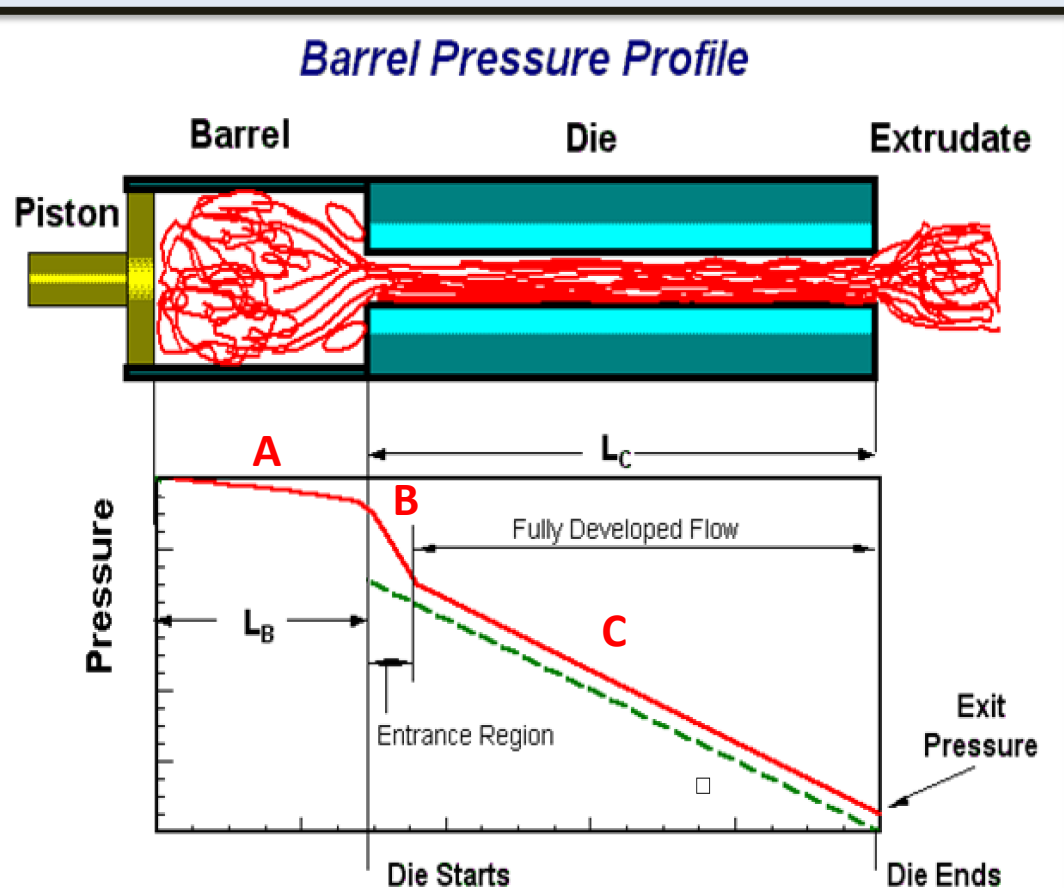


# How to Apply Rabinowicz Corrections in LabKars?

Click to plot viscosity  
versus “corrected”  
shear rate



# Why Bagley Corrections?



- **$A = \Delta p_{\text{Barrel}}$** : Very minor pressure drop in barrel
- **$B = \Delta p_{\text{Entrance}}$** : Excess pressure drop in die entrance
- **$C = \Delta p_{\text{Capillary}}$** : Fully developed flow region in capillary die

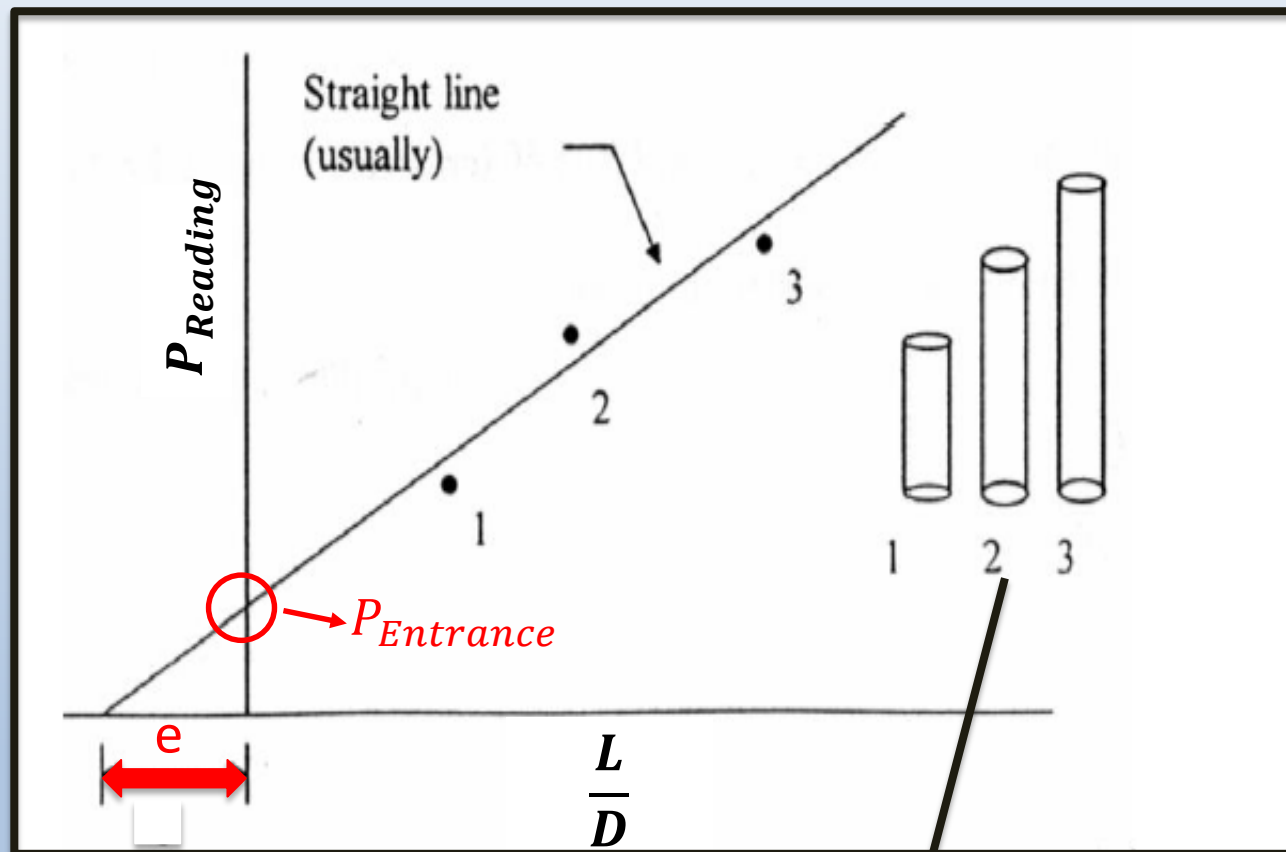
- ❖ Large pressure drop associated with the flow entrance region due to viscoelasticity of polymers.
- ❖ After entrance region, The pressure gradient approaches a constant value (fully developed flow region)

- ❖ In reality:

$$\Delta P_{\text{total}} = \Delta P_{\text{Entrance}} + \Delta P_{\text{capillary}}$$

- ❖ Bagley correction needs to be applied to calculate the entrance pressure drop

# How to Calculate the Entrance Pressure?



Three dies, same diameter  
but different lengths  
(e.g.  $L/D$ : 10, 20, and 30)

$$\tau_{Corrected} = \frac{P_{Reading} - P_{Entrance}}{4\left(\frac{L}{D}\right)}$$

where

$$P_{Entrance} = P \left( \text{at } \frac{L}{D} = 0 \right)$$

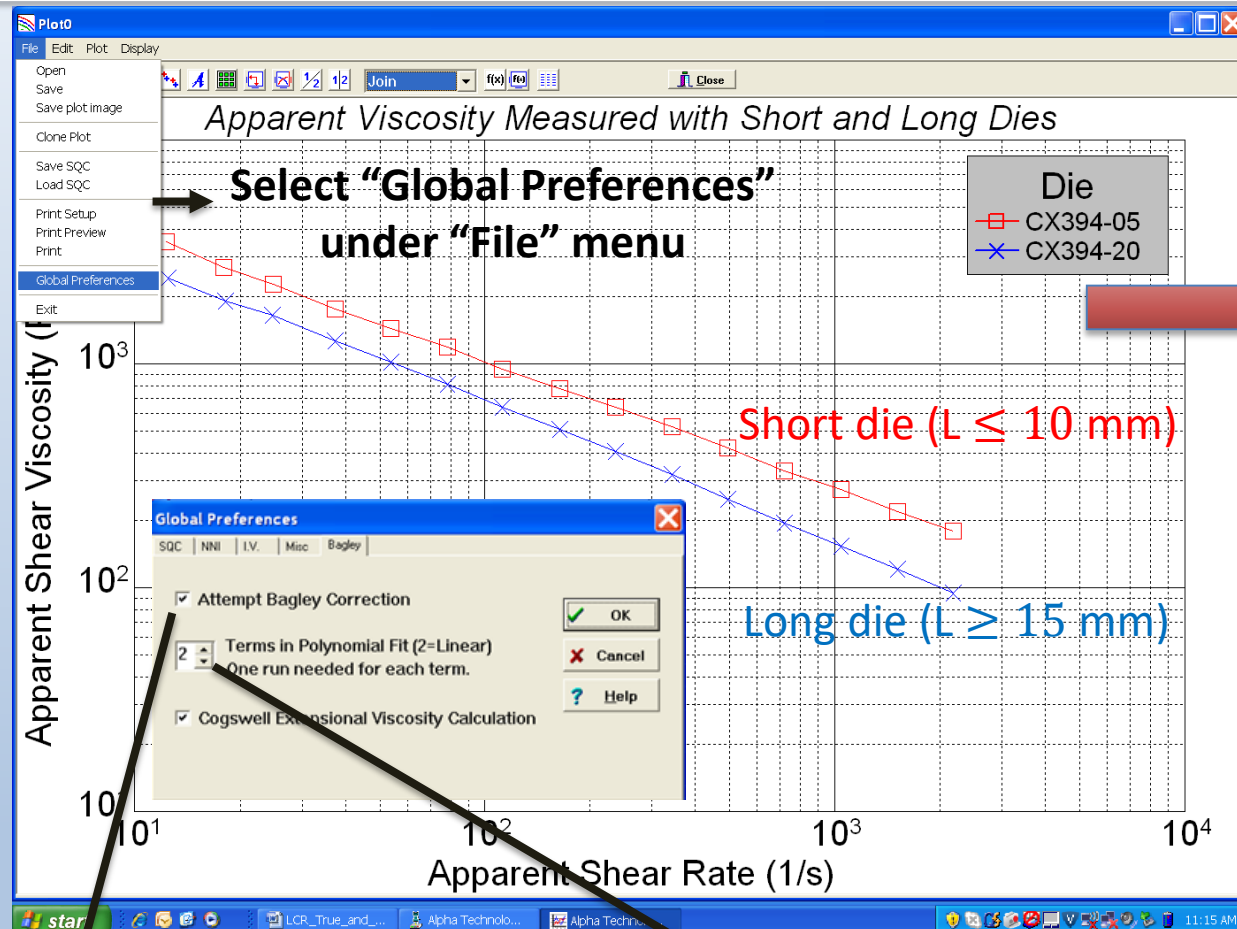
OR

$$\tau_{Corrected} = \frac{P_{Reading}}{4\left(\frac{L}{D} + e\right)}$$

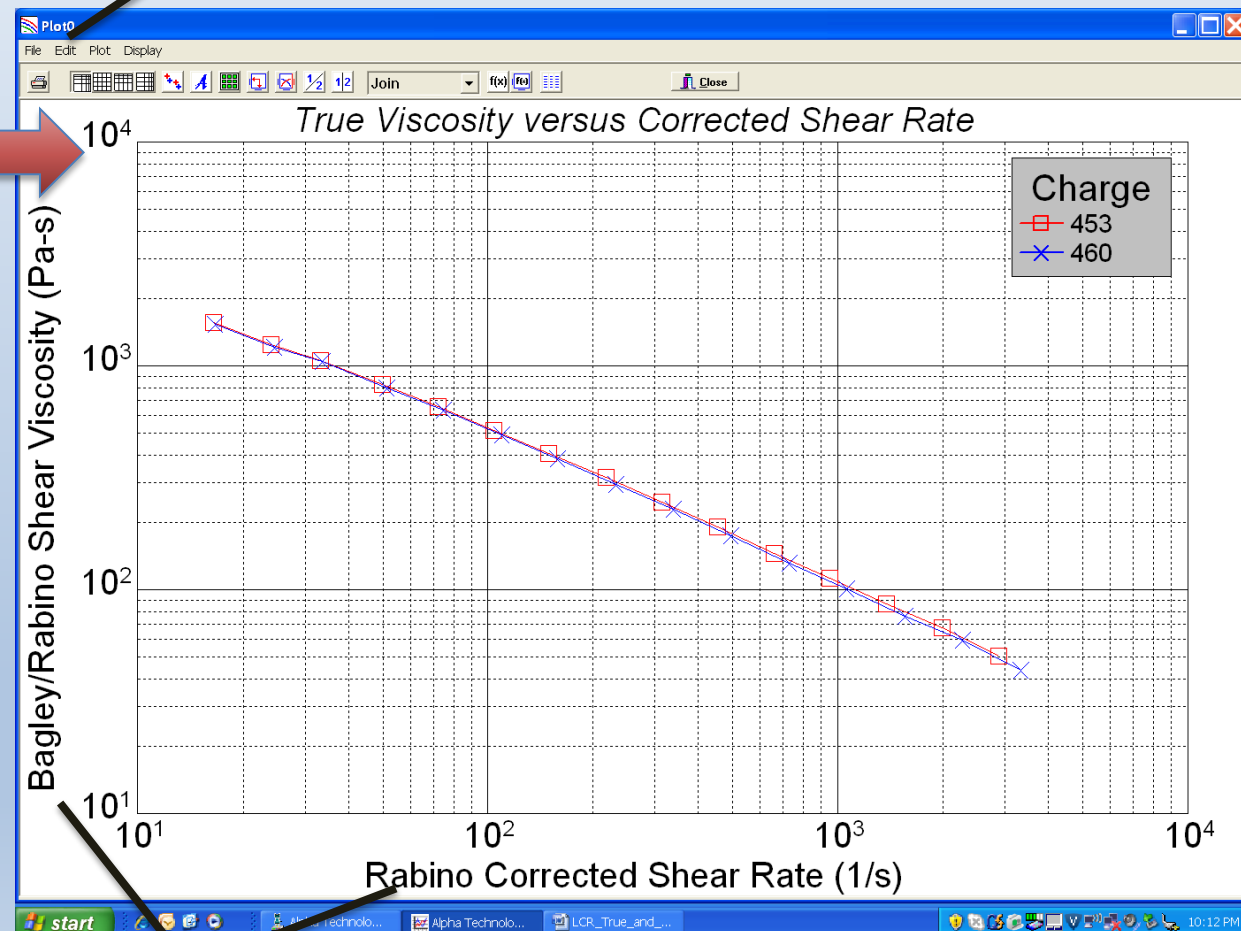
where

$$e = \text{end correction} = \frac{-L_{Entrance}}{D}$$

# How to Apply Bagley Corrections in LabKars?



Select "Copy Table to Clipboard" under "Edit" menu to get the raw data



Select "Attempt Bagley Correction"

Insert number "2"



# How to Calculate True Viscosity?

$$\eta_{True} = \frac{\tau_C}{\dot{\gamma}_C}$$

where

- $\eta_{True}$  (Pa-s): Viscosity with Bagley and Rabinowicz Corrections
- $\tau_C$  (Pa): Bagley corrected shear stress
- $\dot{\gamma}_C$  (1/s): Rabinowicz corrected shear rate



*From lab to production,  
providing a window into the process*

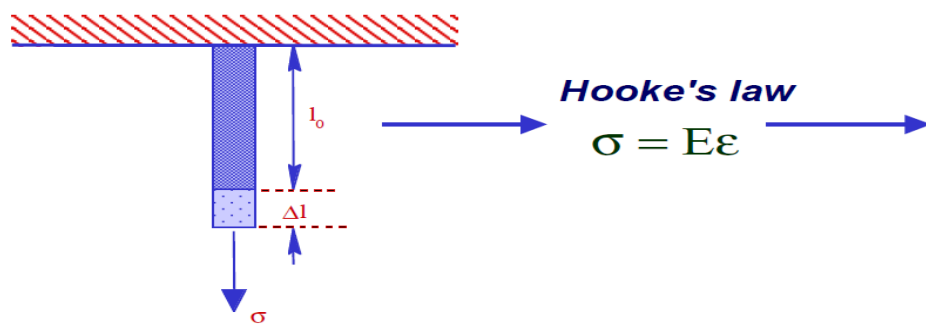
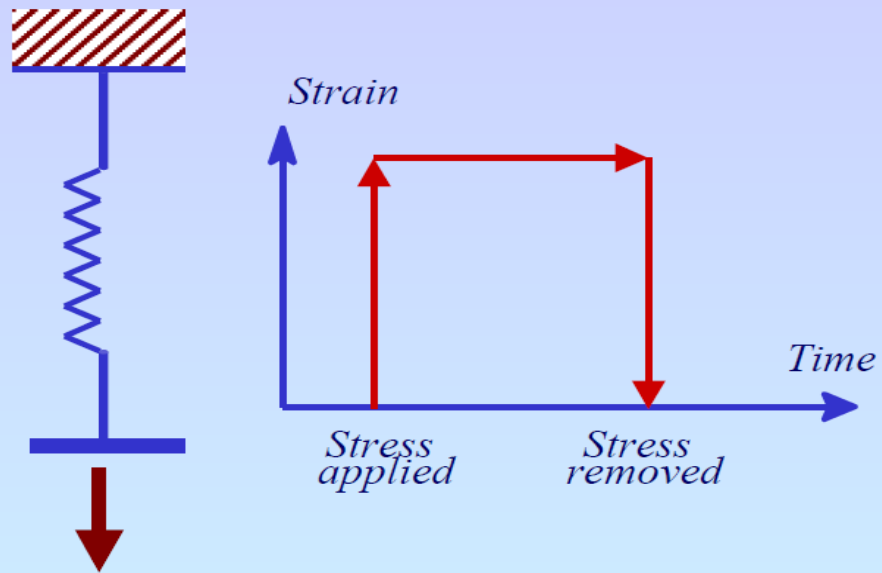


# Viscoelasticity

# Mechanical Models of Viscoelastic Behavior

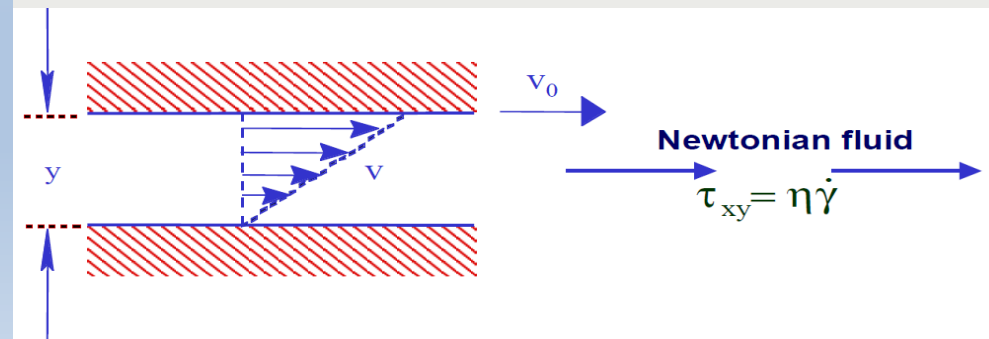
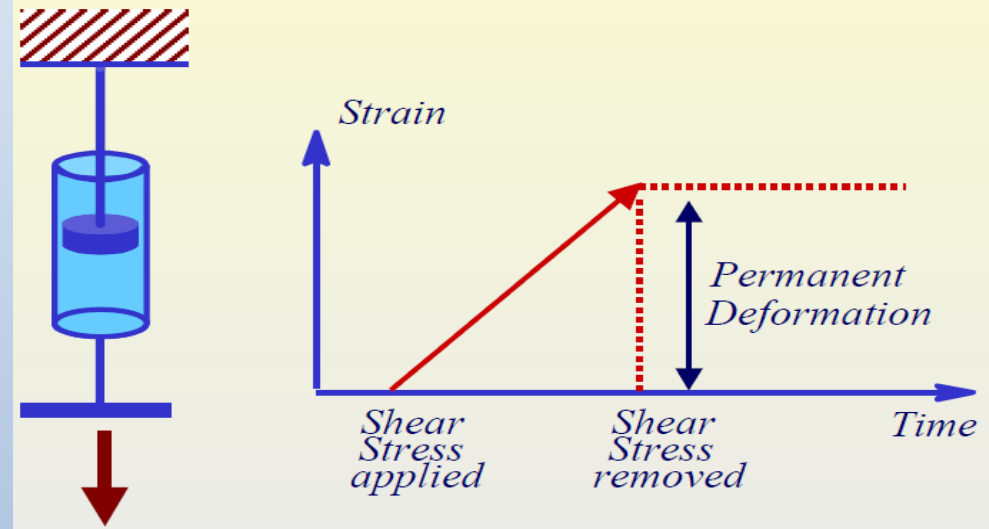
## PURELY ELASTIC RESPONSE

$$\sigma = E\varepsilon$$

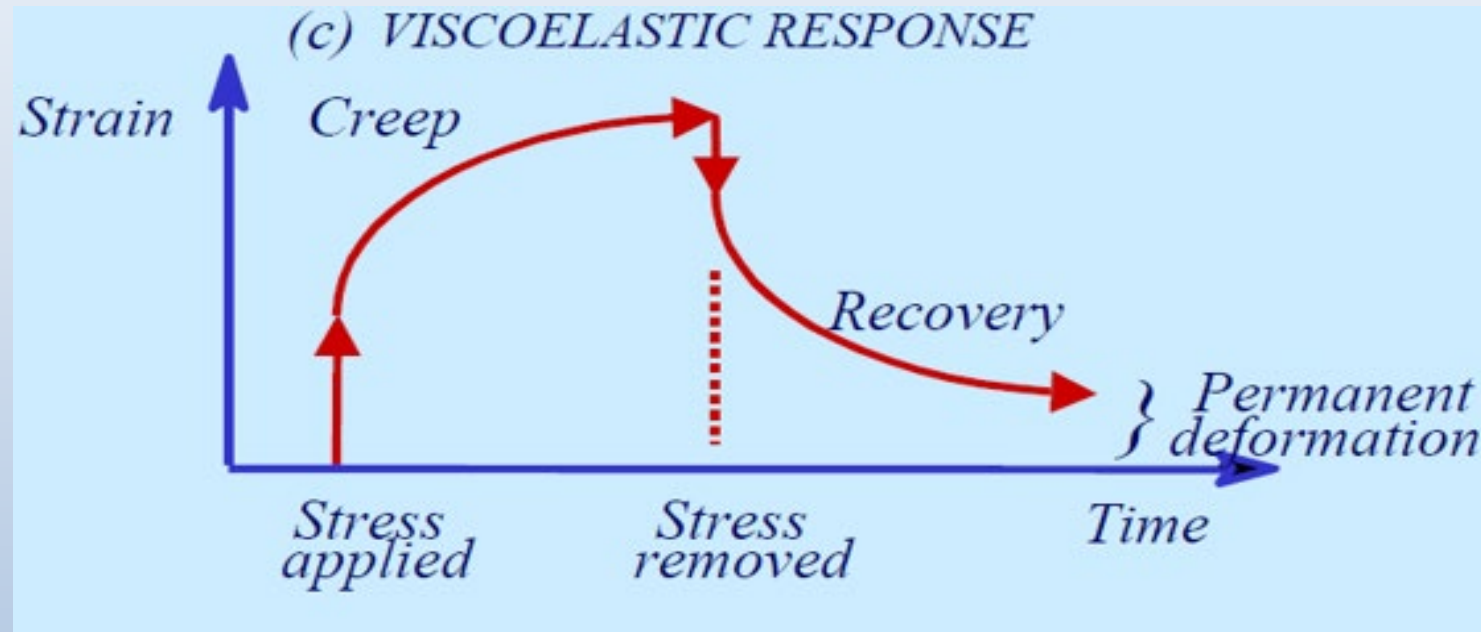


## PURELY VISCOUS RESPONSE

$$\sigma = \eta \frac{d\varepsilon}{dt}$$



# Mechanical Models of Viscoelastic Behavior







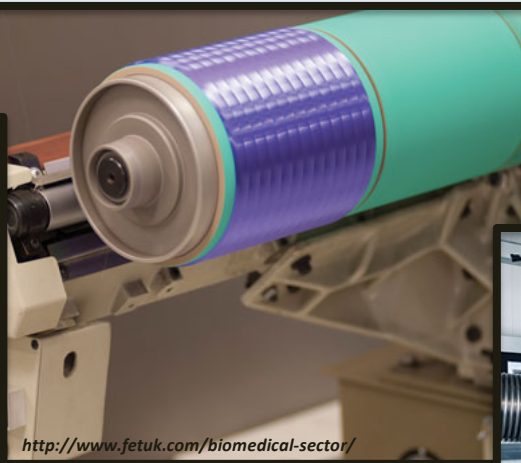
*From lab to production,  
providing a window into the process*



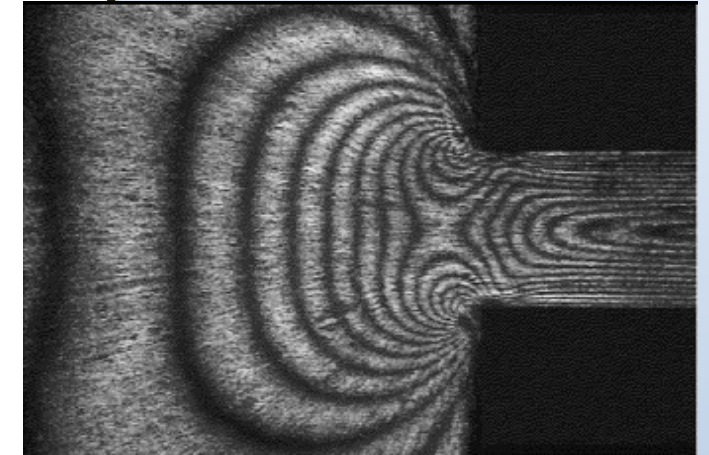
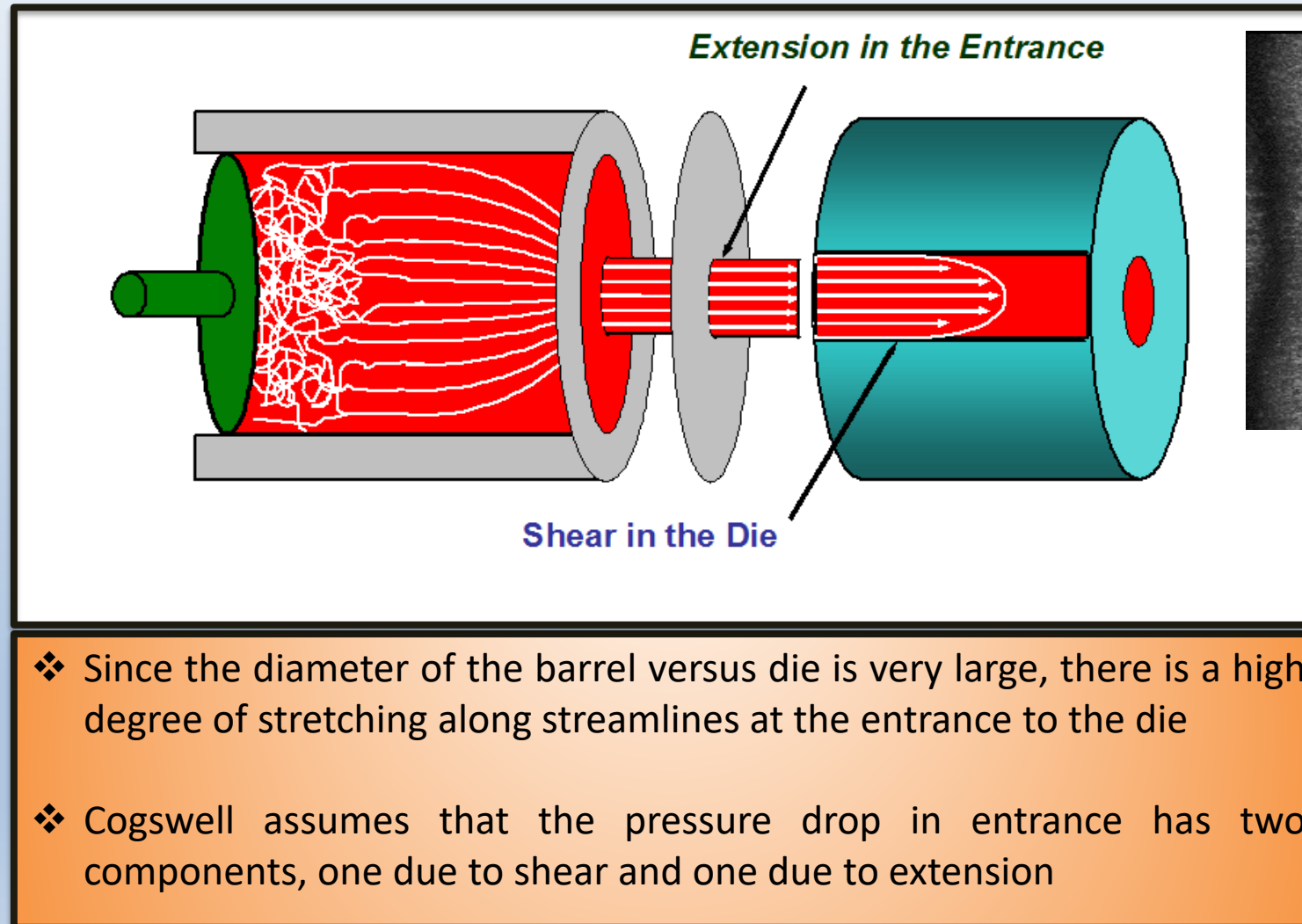
# Extensional Viscosity Measurements

# When Extensional Viscosity is important?

Any process that has stretch!



# What is Extensional (Elongational) Viscosity?





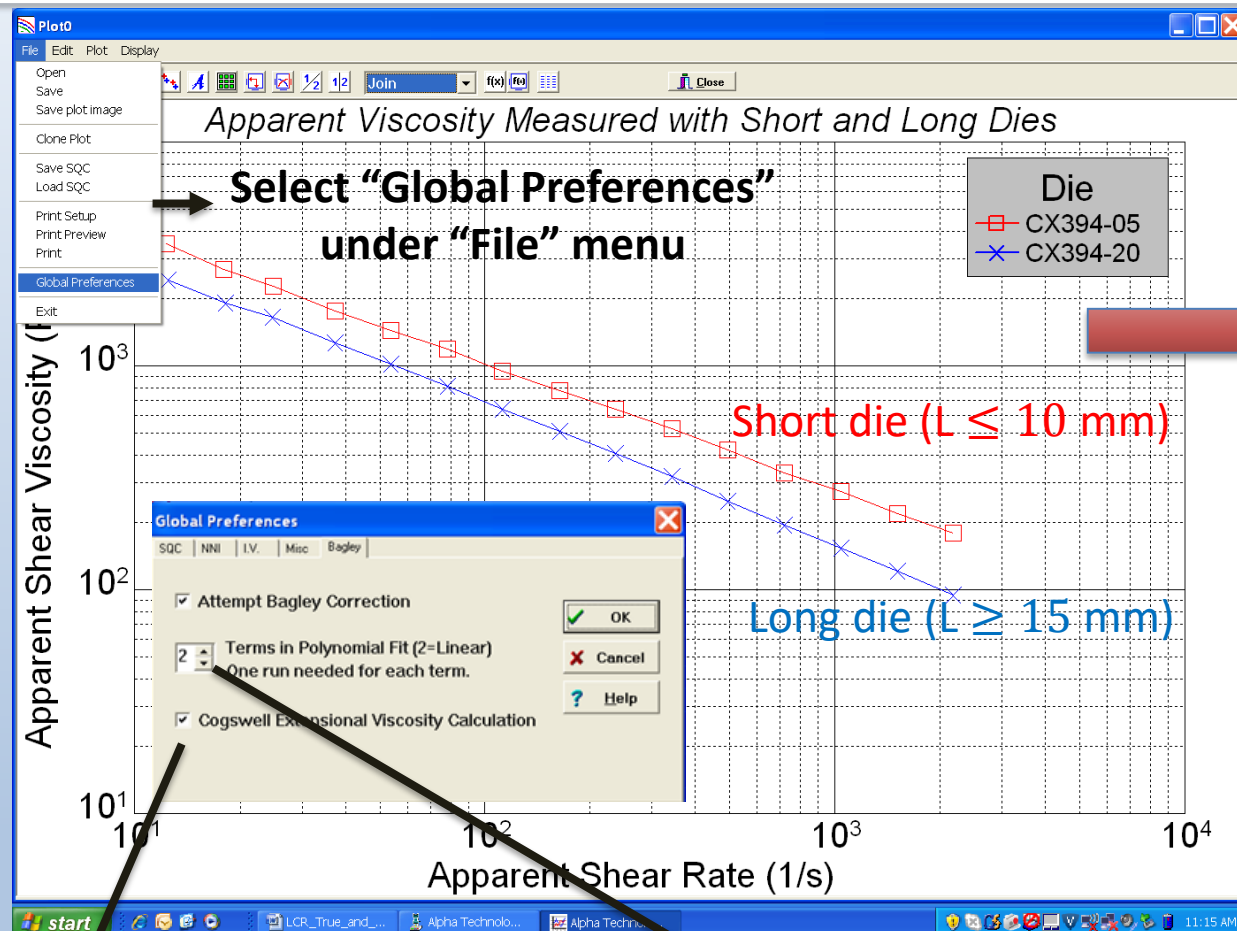
# Cogswell's Equations

|                                     |                                                                                                                                                                                                                                                                                                                   |
|-------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| <p><b>Extensional Stress</b></p>    | <p>❖ <math>\sigma_{Ext} = \frac{3}{8}(n + 1)P_{Ent}</math></p> <ul style="list-style-type: none"> <li>➤ <math>\sigma_{Ext}</math> (Pa): Extensional stress</li> <li>➤ <math>n</math>: Power law index</li> <li>➤ <math>P_{Ent}</math> (Pa): Entrance pressure</li> </ul>                                          |
| <p><b>Extensional Rate</b></p>      | <p>❖ <math>\dot{\epsilon} = \frac{4\dot{\gamma}_a^2 \eta_a}{3(n+1)P_{Ent}}</math></p> <ul style="list-style-type: none"> <li>➤ <math>\epsilon</math> (1/s): Extensional rate</li> <li>➤ <math>\dot{\gamma}_a</math> (1/s): Apparent shear rate</li> <li>➤ <math>P_{Ent}</math> (Pa): Entrance pressure</li> </ul> |
| <p><b>Extensional Viscosity</b></p> | <p>❖ <math>\eta_{Ext} = \frac{9(n+1)^2 P_{Ent}^2}{32\eta_a \dot{\gamma}_a^2}</math></p> <ul style="list-style-type: none"> <li>➤ <math>\eta_{Ext}</math> (Pa-s): Extensional viscosity</li> </ul>                                                                                                                 |

J.M. Dealy, K.F. Wissbrun, *Melt Rheology and its Role in Plastics Processing: Theory and Applications*, Van Nostrand Reinhold, New York (1990).

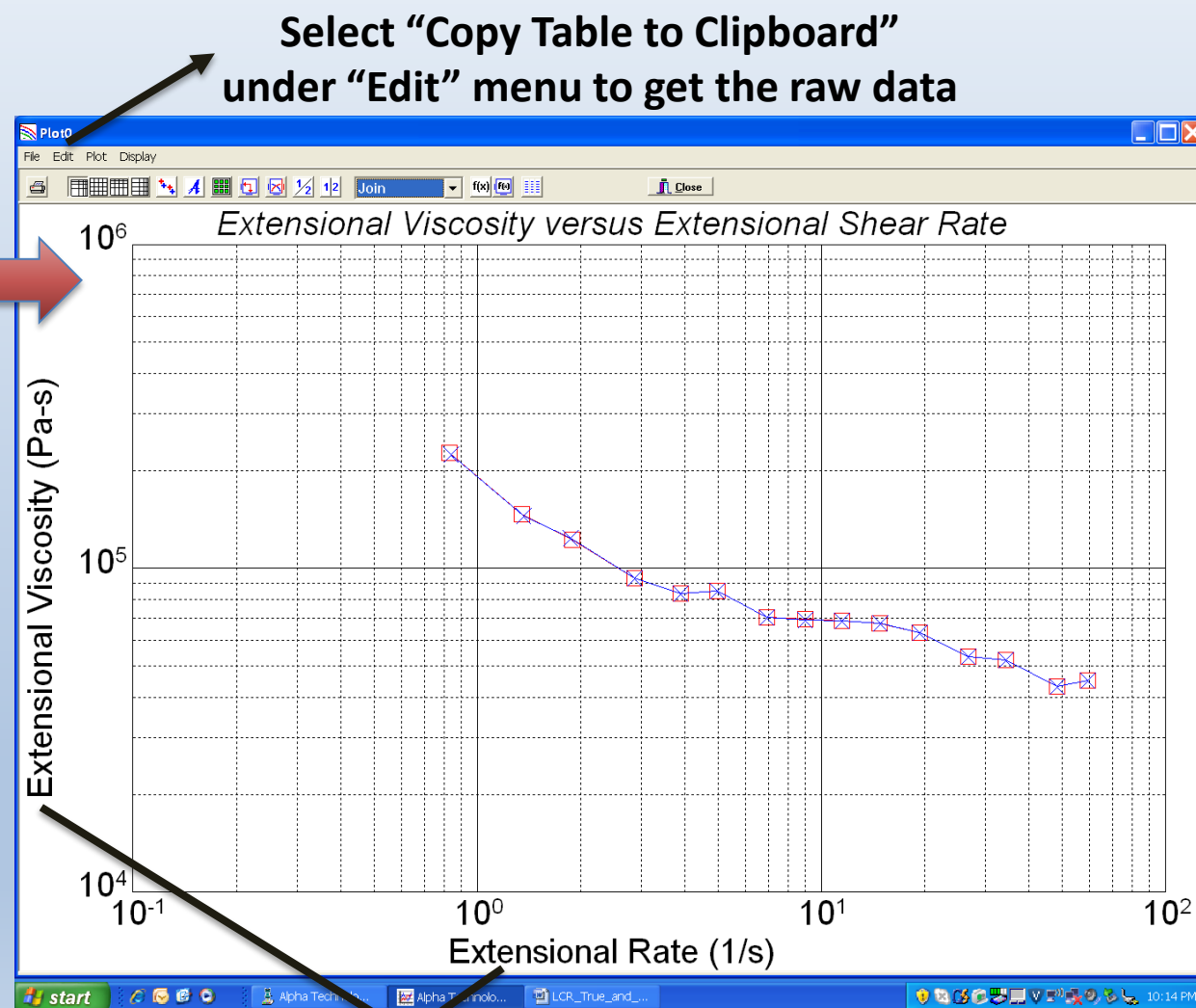


# How to Perform Extensional Viscosity Measurements in LabKars?

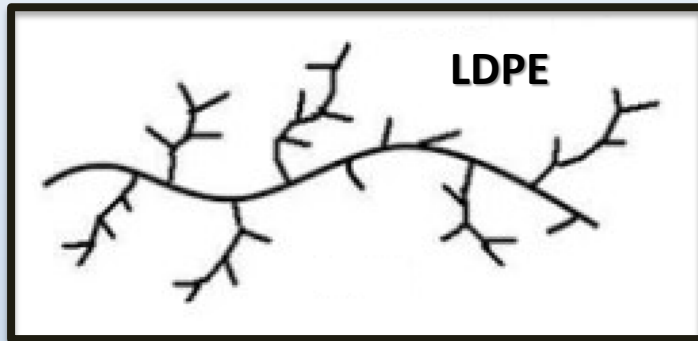


Select "Cogswell Extensional Viscosity Calculation"

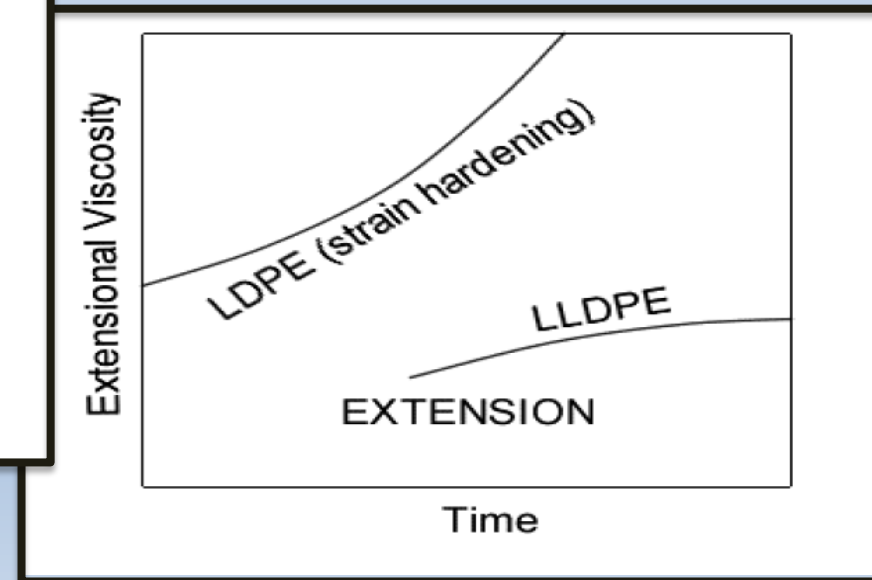
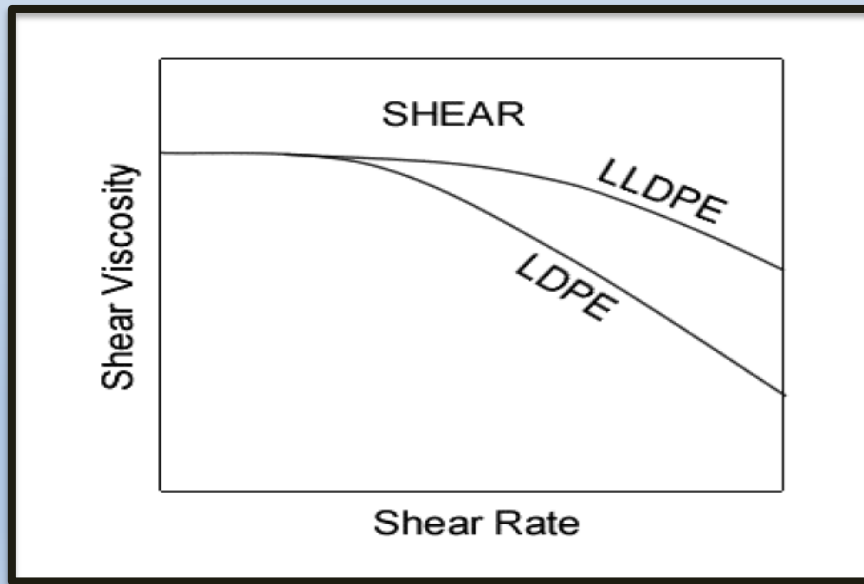
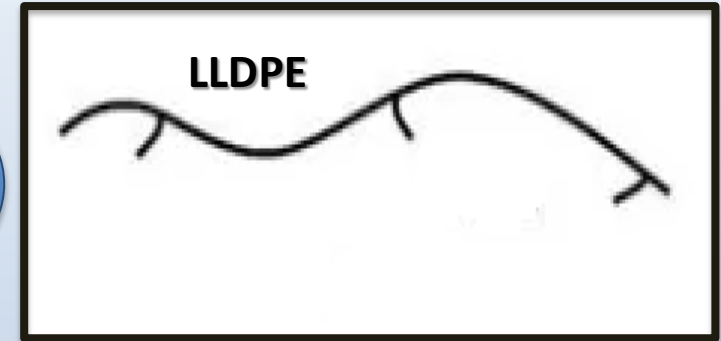
Insert number "2"



# Example!



LLDPE (Linear structure) is stiffer than LDPE (branched structure) in shear but softer in extension



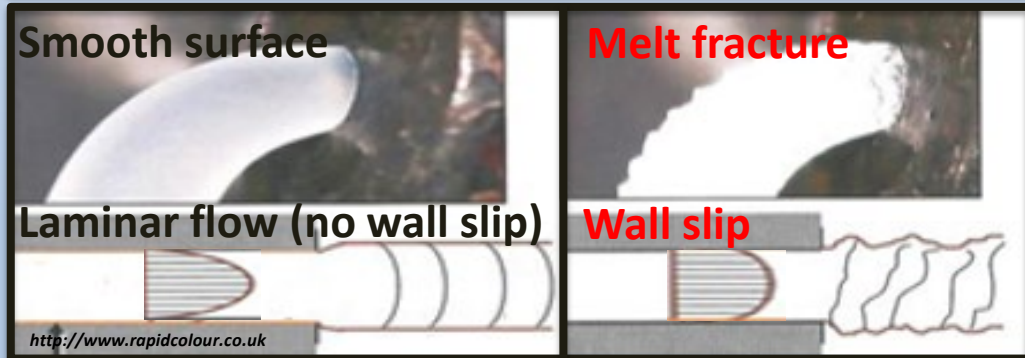
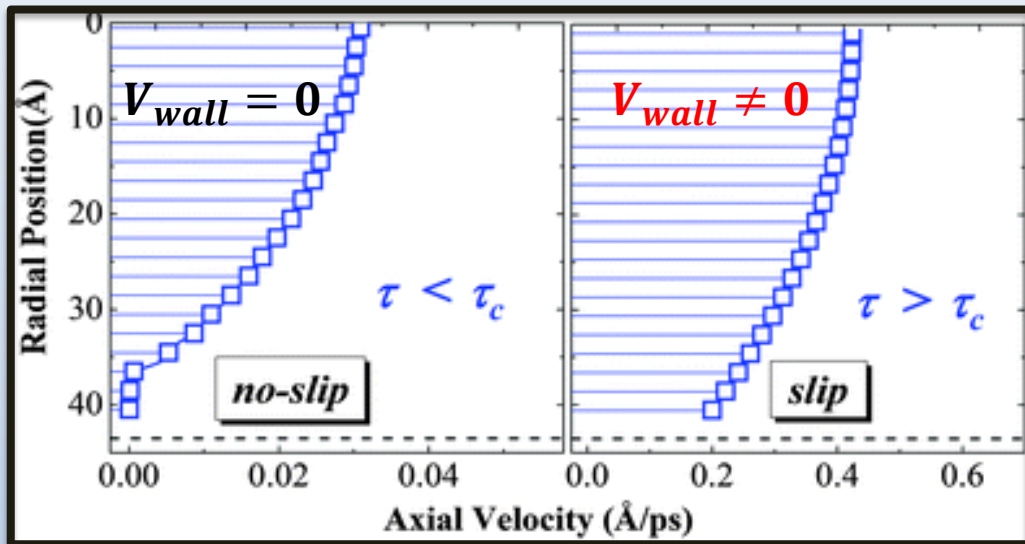


*From lab to production,  
providing a window into the process*



# Wall Slip Velocity & Melt Fracture

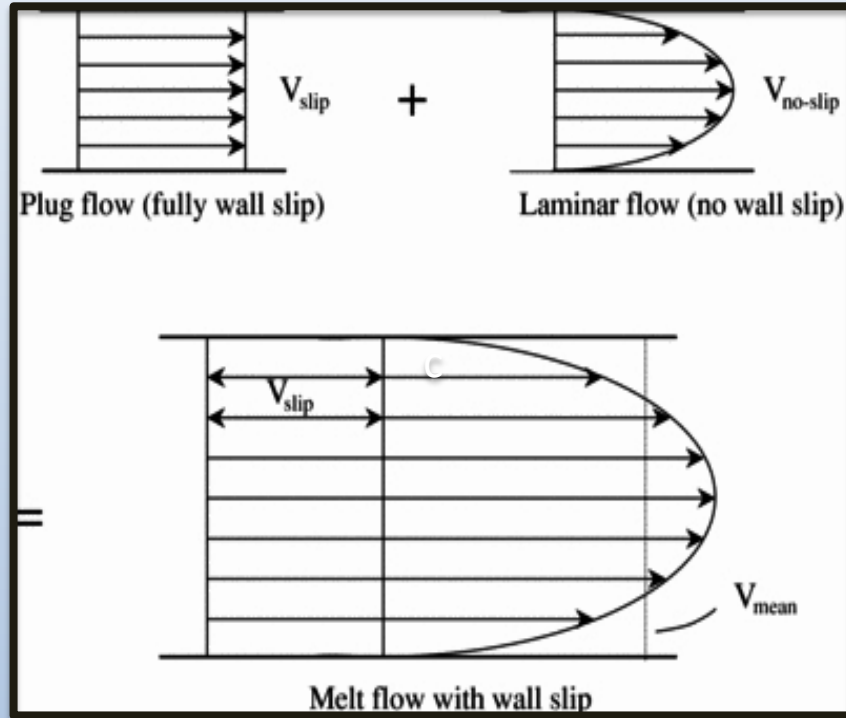
# Wall Slip in Capillary Flow



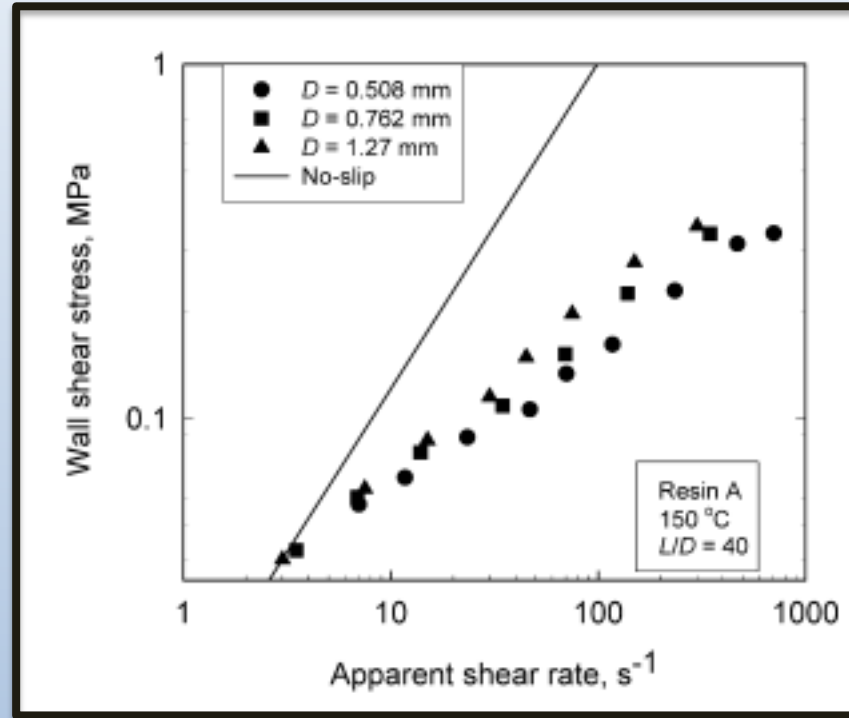
- ❖ Wall slip velocity increases dramatically above critical shear stress ( $\sim 0.1$  MPa).
- ❖ Slippage reduces apparent viscosity. Also, the surface of the extrudate begins to be rough (**melt fracture**).
- ❖ Wall slip happens due to elastic properties of polymer materials.
- ❖ Critical shear stress is lower for polymers with higher molecular weight
- ❖ Trouble shooting by using larger die diameter, longer die, tapering the die, higher temperature, or lower shear rate.



# Effect of Wall Slip on Capillary Rheometer Results



R.D. Chien, W.R. Jong, S.C. Chen, Study on Rheological Behavior of Polymer Melt Flowing Through Micro-Channels Considering the Wall-Slip Effect, *J. Micromech. Microeng.* 15, (2005), 1389



S. G. Hatzikiriakos, Wall Slip of Molten Polymers, *Progress in Polymer Science*, 37 (2012), 624-643

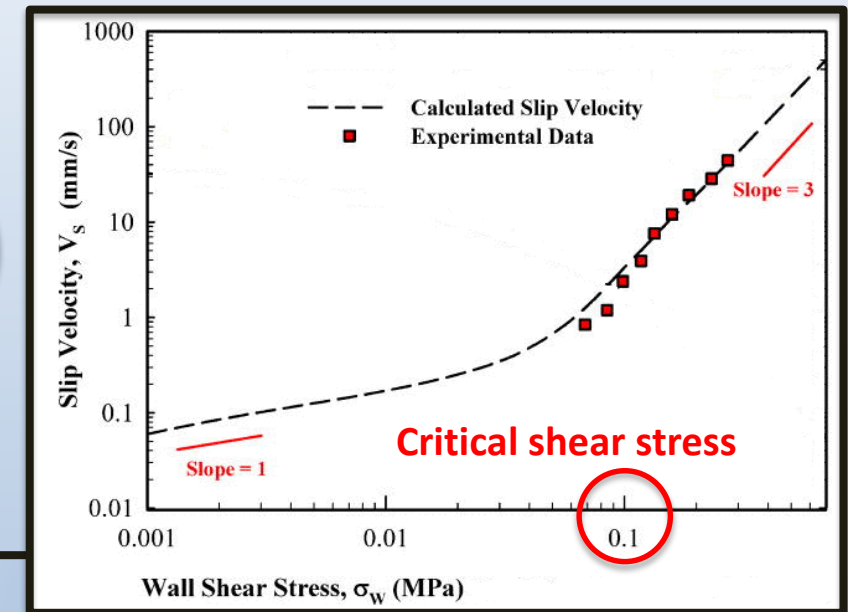
Wall slip causes formation of plug flow and a discontinuity in flow curve.

# How to Calculate Wall Slip Velocity?

$$\dot{\gamma}_a = 4V_w \left( \frac{1}{R_C} \right) + X$$

where

- $V_w$  (mm/sec): Wall slip velocity
- $\dot{\gamma}_a$  (1/s): apparent shear rate at a given value of shear stress
- $R_C$  (mm): Capillary die radius
- $X$ : Dimensionless parameter (a function of the shear stress)



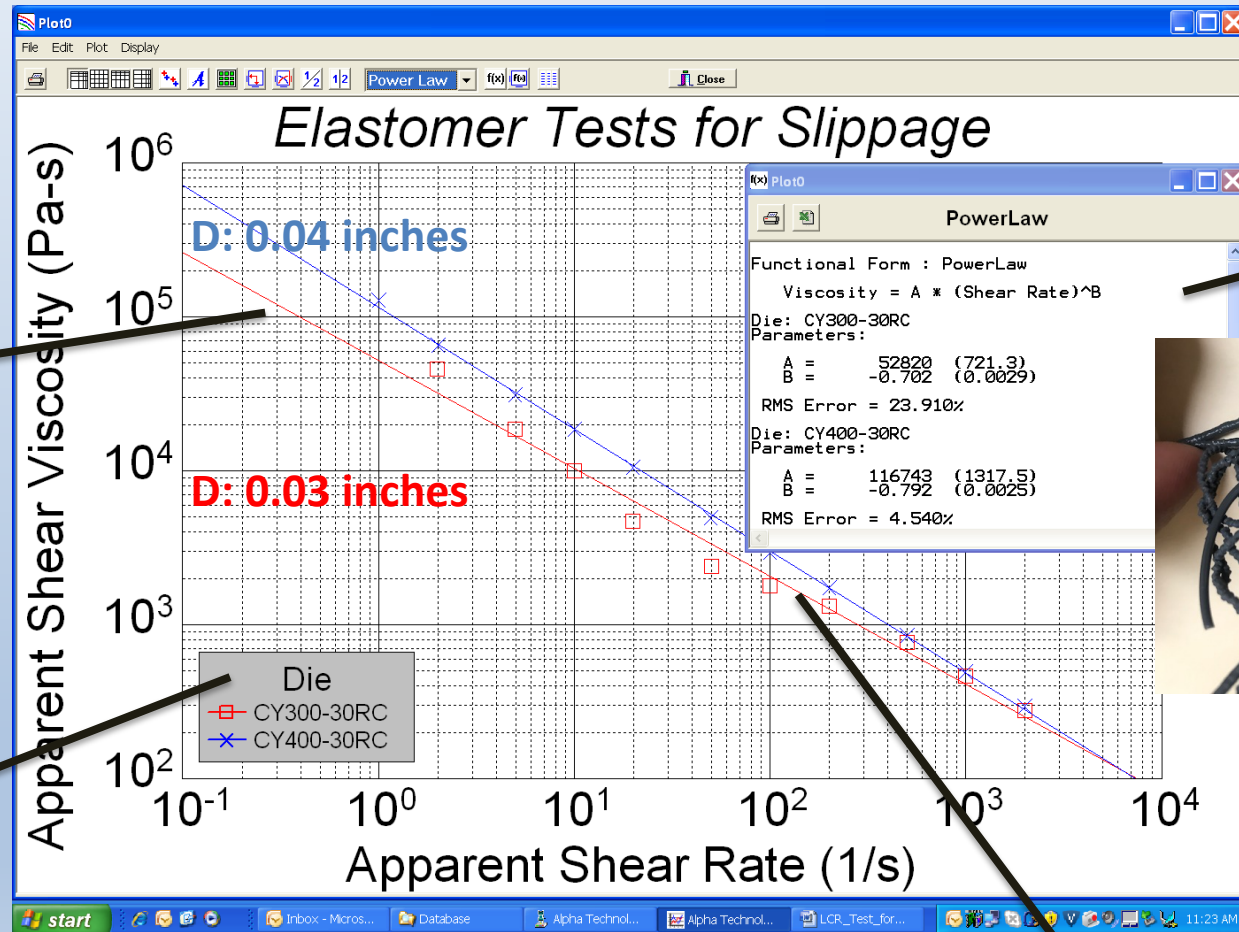
## Steps:

1. Produce a series of flow curves using a set of dies of varying radius ( $R_C$ ).
2. At a given value of shear stress, make a plot of apparent shear rate ( $\dot{\gamma}_a$ ) versus inverse radius ( $\frac{1}{R_C}$ ).
3. Slip velocity at a given shear stress will be one quarter of the slope of  $\dot{\gamma}_a$ -vs- $\frac{1}{R_C}$  plot.
4. Repeat the test at other shear stresses and calculate the slip velocity at each specific shear stress.
5. Make the plot of slip velocity versus shear stress.

# How to Notice Wall Slippage from Flow Curve in LCR?

NOT overlapping of results from two dies means slippage happened at the smaller die

Perform shear rate sweep on two dies with same L/D but different diameters

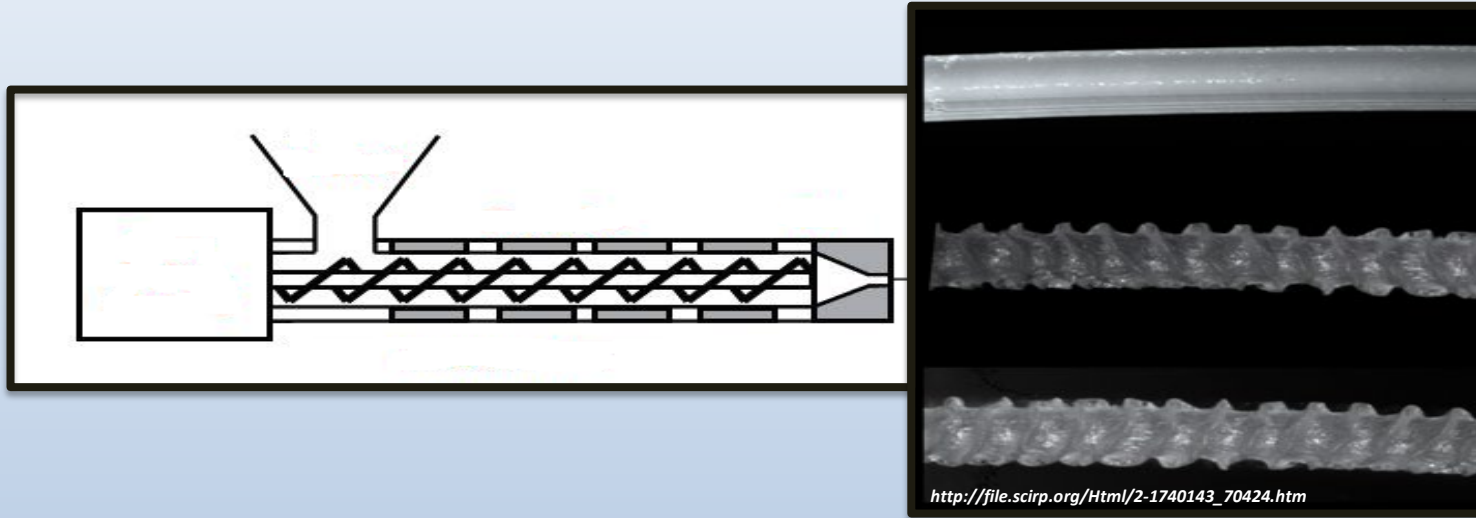


Slippage affect Power-Law model parameters



Viscosity is lower when slippage happens in smaller die diameter.

# Melt Fracture Trouble Shooting in Extrusion Process



This phenomena happens due to elasticity of polymer melts. **Any procedure that reduces the melt elasticity will help to troubleshoot.** e.g.:

- ✓ Increasing temperature
- ✓ Reducing screw speed (shear rate)
- ✓ Increasing the die length or die diameter
- ✓ Tapering the die

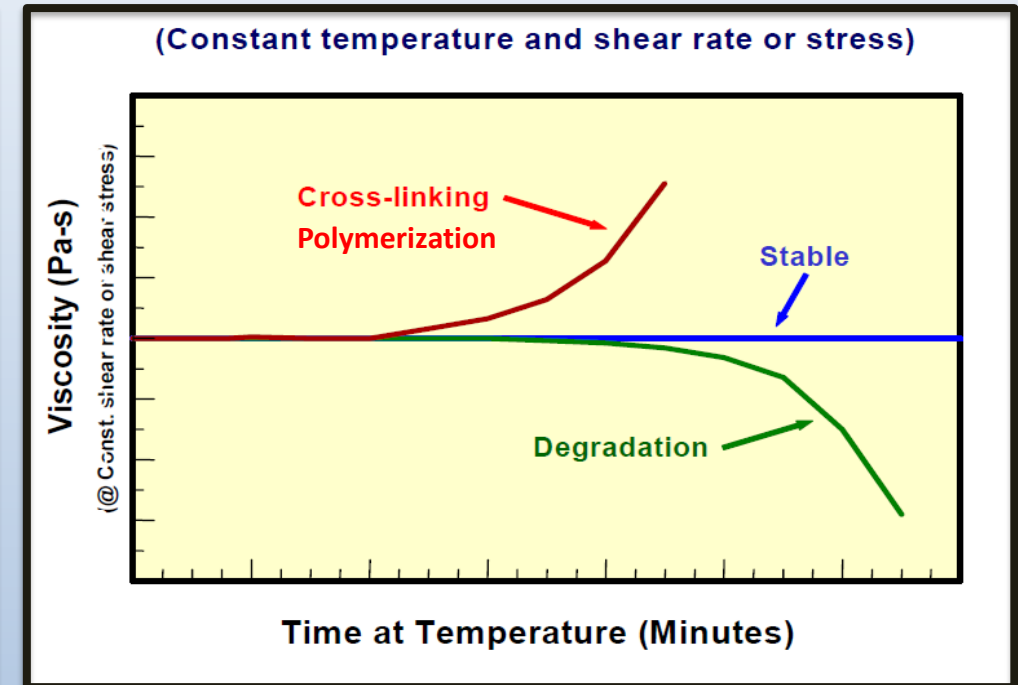
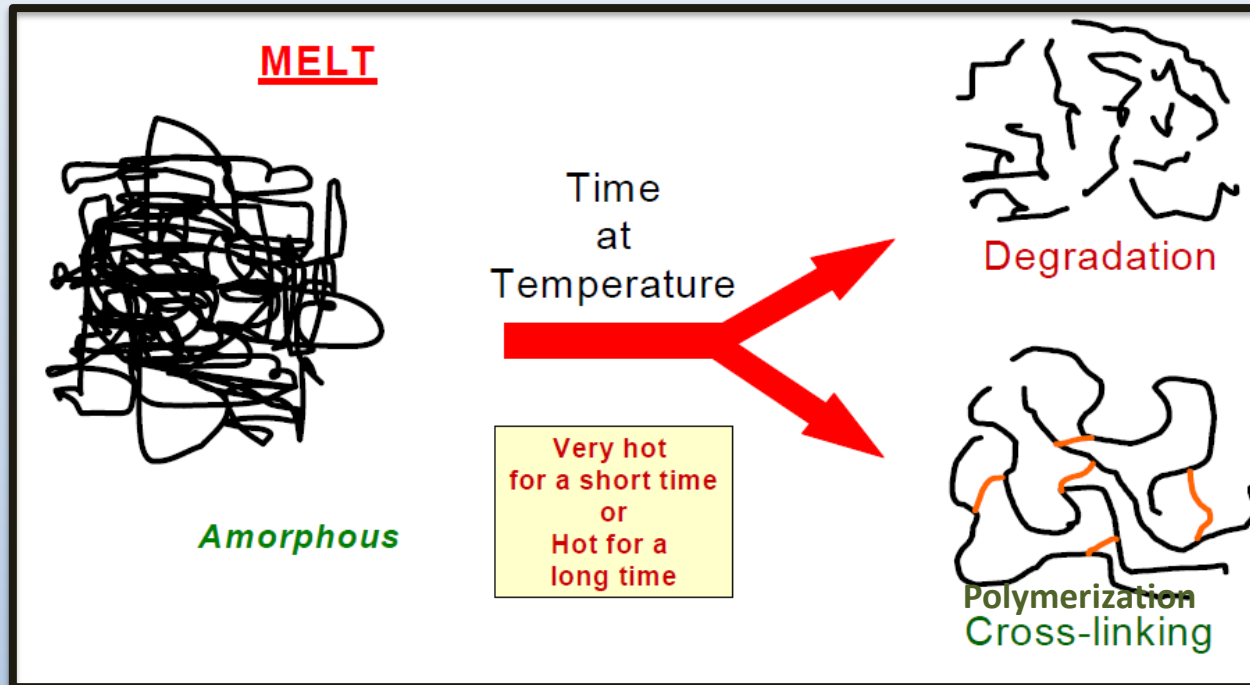




# Time Sweep Test

(Thermal Stability of Polymers)

# Thermal Stability of Polymer Melt



- ❖ The stability test can determine the resistance of a material to a change in viscosity at the test temperature.
- ❖ The stability of polymer melts varies depending on temperature, time at temperature, formulation, and contaminants.
- ❖ This test can be used to show the presence of moisture or reactive chemicals in a polymer.
- ❖ This test can be used to measure the degradation rate or reactivity of a sample

# How to Set up Thermal Stability Test (Time Sweep) in LabKars?

**Setup**

**Data Point Setup # 11**

| Setup # | Program Name          | Start Pos. | Temperature | Melt Time | Sensor1 ID  | Die      |
|---------|-----------------------|------------|-------------|-----------|-------------|----------|
| 2       | 7523 Control Grey PP  | 100        | 230         | 300       | LC-103N     | CY300-33 |
| 3       | Polycarbonate         | 100        | 300         | 300       | LC-103N     | CY300-33 |
| 4       | Position Based Test   | 90         | 190         | 300       | LC-103N     | CX300-33 |
| 5       | Bagley Test           | 100        | 230         | 300       | PT-142BAR-A | CX394-40 |
| 6       | Thermalstability Test | 100        | 285         | 120       | LC-103N     | CZ600-20 |
| 7       | Nylon                 | 90         | 240         | 240       | LC-103N     | CZ394-20 |
| 8       | HDPE                  | 90         | 90          | 360       | LC-103N     | CZ787-15 |
| 9       | PEEK                  | 100        | 400         | 300       | LC-103N     | CY400-15 |
| 10      | PET I.V.              | 100        | 285         | 240       | LC-103N     | CX300-33 |
| 11      | Nylon Stability       | 89         | 240         | 180       | LC-502N     | CZ394-20 |

**Control Mode**  
☒ Rate ☐ Stress

**Test Type**  
☐ Steady State  
☒ Position (Acquire At - mm)  
☐ Manual  
☐ Time Delay (Acquire At - sec)  
☐ Elapse Time (Acquire At - sec)

Minimum Speed **0.03**  
 Maximum Speed **650**

| Point # | Speed Control | Shear Rate | Delay Sec | Time Min | Acquire At-mm |
|---------|---------------|------------|-----------|----------|---------------|
| 1       | 6.50          | 79.05      |           |          | 102.0         |
| 2       | 6.50          | 79.05      |           |          | 115.0         |
| 3       | 6.50          | 79.05      |           |          | 128.0         |
| 4       | 6.50          | 79.05      |           |          | 141.0         |
| 5       | 6.50          | 79.05      |           |          | 154.0         |
| 6       | 6.50          | 79.05      |           |          | 167.0         |
| 7       | 6.50          | 79.05      |           |          | 180.0         |
| 8       | 6.50          | 79.05      |           |          | 193.0         |
| 9       | 6.50          | 79.05      |           |          | 206.0         |
| 10      | 6.50          | 79.05      |           |          | 219.0         |

Select  
"Position"  
Test Type

$$\Delta L = S \times \Delta t$$

$$\frac{13 \text{ mm}}{6.5 \text{ mm/sec}} = 2 \text{ sec}$$

Where

➤  $\Delta L$ : Piston travel distance between points

➤  $S$ : Piston speed  
 $= \frac{\text{Max plunger travel (130 mm)}}{\text{Test time (e.g. 20 min)}}$

➤  $\Delta t$ : Piston time travel between points  
 $= \frac{\text{Test time (e.g. 20 min)}}{\text{\# of points (e.g. 10)}}$

Applying the same speed and shear rate multiple times

# How to Set up Thermal Stability Test (Time Sweep) in LabKars?

**Setup**

**Data Point Setup # 11**

| Setup # | Program Name          | Start Pos. | Temperature | Melt Time | Sensor1 ID  | Die      |
|---------|-----------------------|------------|-------------|-----------|-------------|----------|
| 2       | 7523 Control Grey PP  | 100        | 230         | 300       | LC-103N     | CY300-33 |
| 3       | Polycarbonate         | 100        | 300         | 300       | LC-103N     | CY300-33 |
| 4       | Position Based Test   | 90         | 190         | 300       | LC-103N     | CX300-33 |
| 5       | Bagley Test           | 100        | 230         | 300       | PT-142BAR-A | CX394-40 |
| 6       | Thermalstability Test | 100        | 285         | 120       | LC-103N     | CZ600-20 |
| 7       | Nylon                 | 90         | 240         | 240       | LC-103N     | CZ394-20 |
| 8       | HDPE                  | 90         | 90          | 360       | LC-103N     | CZ787-15 |
| 9       | PEEK                  | 100        | 400         | 300       | LC-103N     | CY400-15 |
| 10      | PET I.V.              | 100        | 285         | 240       | LC-103N     | CX300-33 |
| 11      | Nylon Stability       | 89         | 240         | 180       | LC-502N     | CZ394-20 |

Control Mode  
☒ Rate ☐ Stress

Test Type  
☐ Steady State  
☒ Position (Acquire At - mm)  
☐ Manual  
☐ Time Delay (Acquire At - sec)  
☐ Elapse Time (Acquire At - sec)

Minimum Speed **0.03**  
Maximum Speed **650**

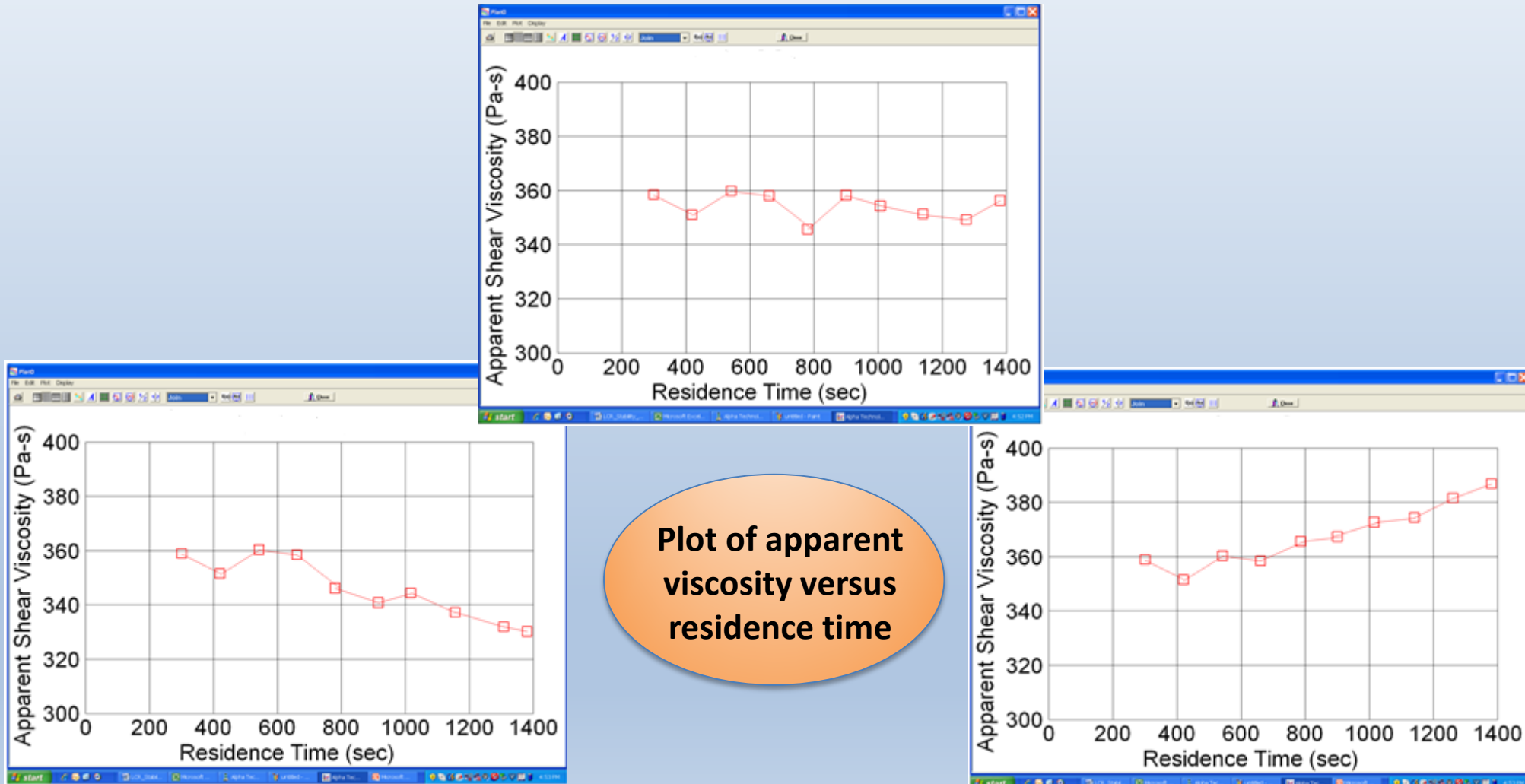
**Point #** **Speed Control** **Shear Rate** **Delay Sec** **Time Min** **Acquire At-mm**

|    |      |       |    |  |       |
|----|------|-------|----|--|-------|
| 1  | 6.50 | 79.05 |    |  | 102.0 |
| 2  | 6.50 | 79.05 | 66 |  | 115.0 |
| 3  | 6.50 | 79.05 | 66 |  | 128.0 |
| 4  | 6.50 | 79.05 | 66 |  | 141.0 |
| 5  | 6.50 | 79.05 | 66 |  | 154.0 |
| 6  | 6.50 | 79.05 | 66 |  | 167.0 |
| 7  | 6.50 | 79.05 | 66 |  | 180.0 |
| 8  | 6.50 | 79.05 | 66 |  | 193.0 |
| 9  | 6.50 | 79.05 | 66 |  | 206.0 |
| 10 | 6.50 | 79.05 | 66 |  | 219.0 |

Add delay time to increase the stability test time while keeping shear rate constant



# Thermal Stability Test Results (Time Sweep) in LabKars





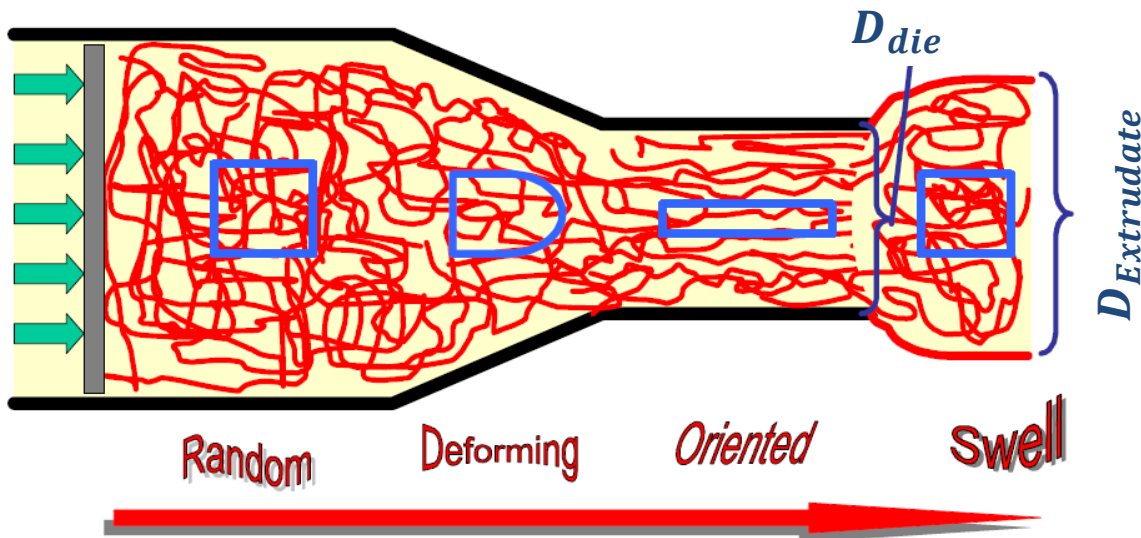
*From lab to production,  
providing a window into the process*



## Die Swell

# Die swell Ratio

## The Source of Extrudate Swell



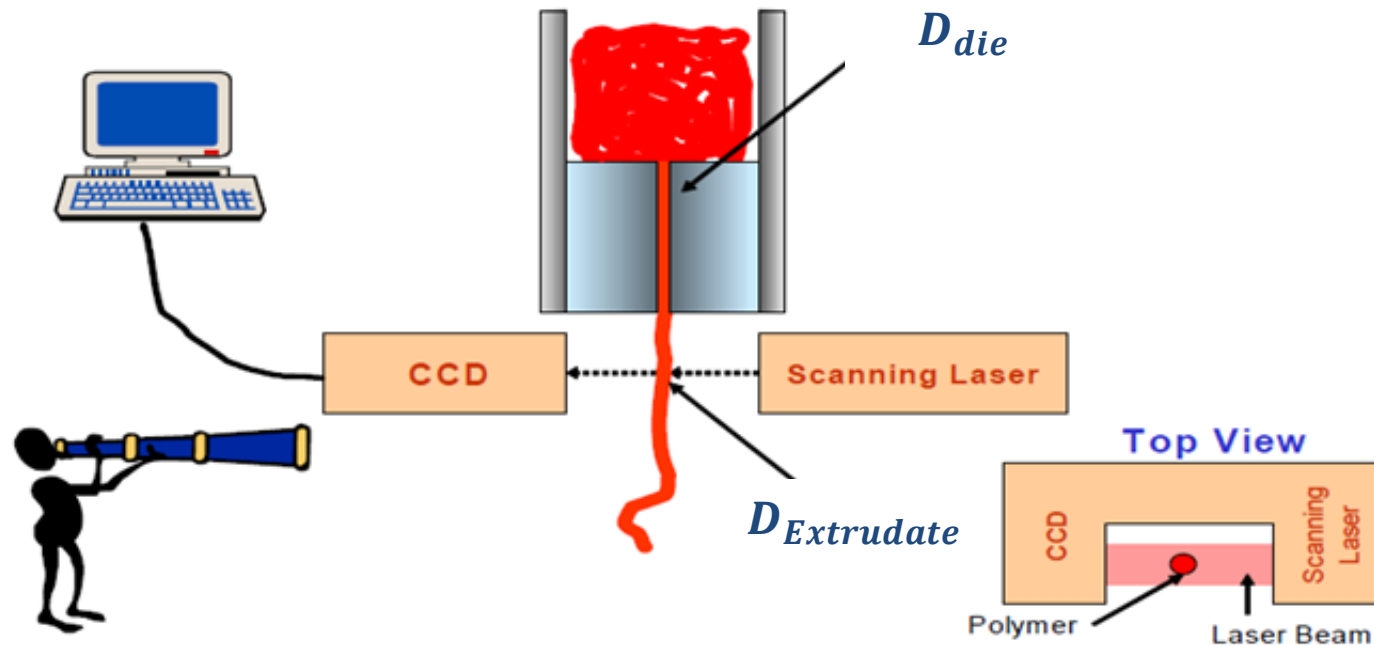
<https://www.azom.com>

$$\text{Percent die swell} = \frac{D_{Extrudate} - D_{die}}{D_{die}} \times 100$$

- ❖ Expansion (re-coiling) of extrudate after exiting die.
- ❖ Qualitative measure of melt elasticity.
- ❖ Relaxed die swell is used to predict part dimension
- ❖ Running die swell is used to predict productivity of extrusion process.
- ❖ Analysis of extrudate smoothness.
- ❖ Trouble shooting by using larger die diameter, longer die, tapering the die, lower shear rate, or higher temperature.

# Die Swell Measurement in LCR

## Measurement of Extrudate Swell

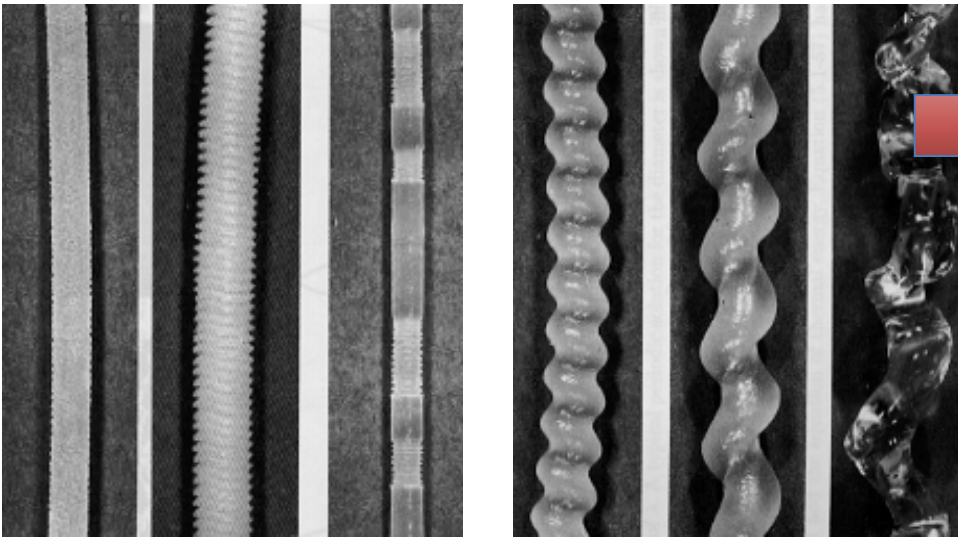


- ❖ Detection: CCD element
- ❖ Light source: 800 nm laser
- ❖ Resolution: 2.75  $\mu\text{m}$
- ❖ Measuring range: 0.13-23 mm
- ❖ Response time: 1.4 ms
- ❖ Accuracy:  $\pm 0.003$  mm



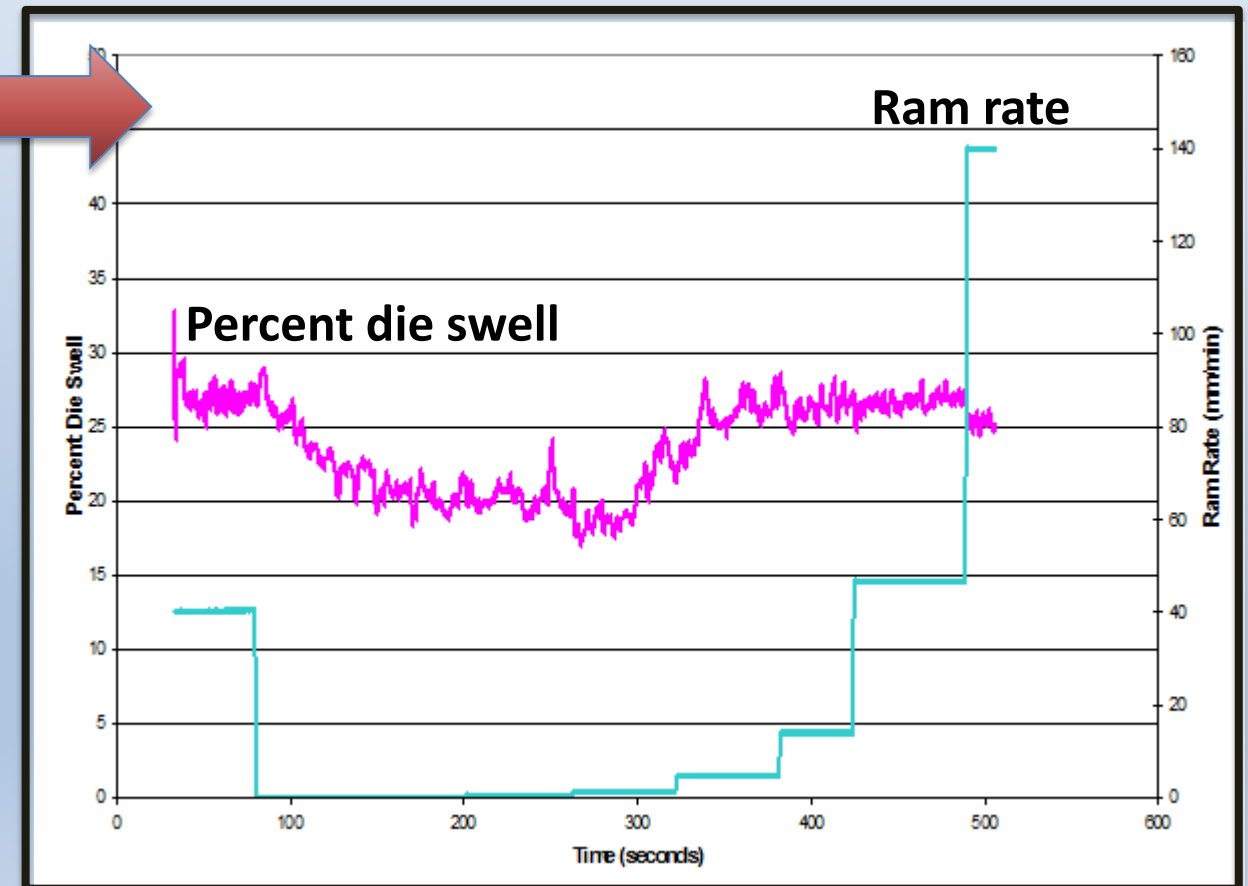
# Die Swell Measurement in LCR

## Melt Fracture

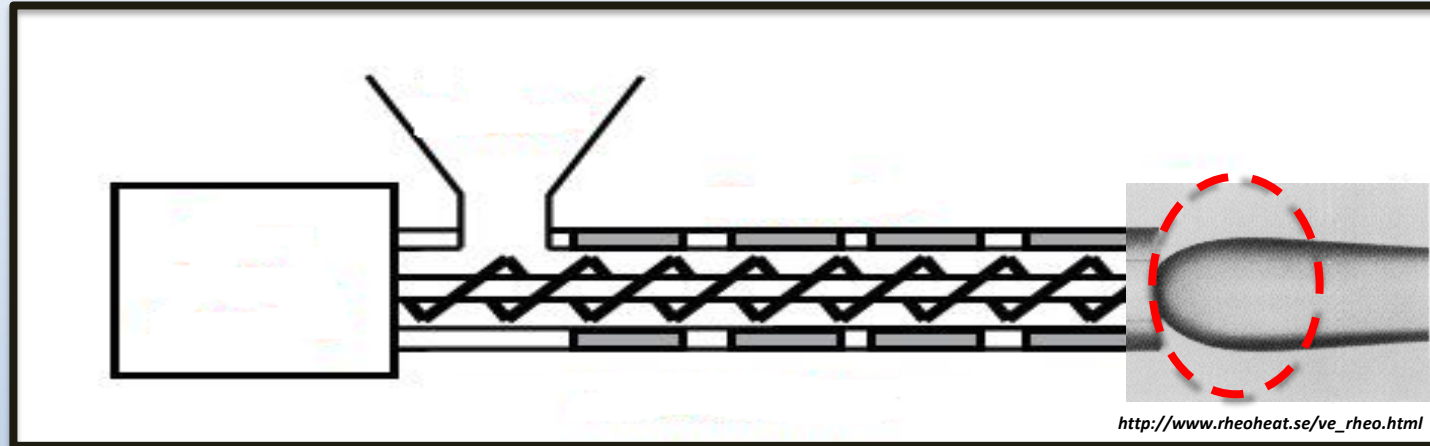


<https://www.azom.com/article.aspx?ArticleID=13578>

Melt fracture produce a noisy die swell measurements.



# Die Swell Trouble Shooting in Extrusion Process



This phenomena happens due to elasticity of polymer melts. **Any procedure that reduces the melt elasticity will help to troubleshoot.** e.g.:

- ✓ Increasing temperature
- ✓ Reducing screw speed (shear rate)
- ✓ Increasing the die length or die diameter
- ✓ Tapering the die



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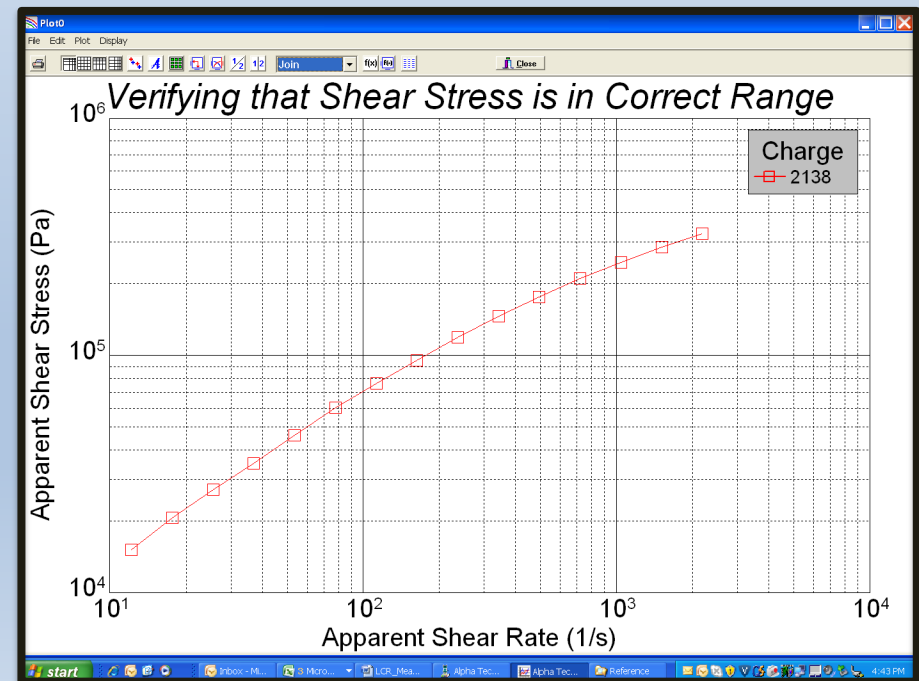
## MFR Correlation

# How to Calculate MFR from Capillary Rheometer?

1. Calculate the shear stress in the melt flow rate tester (using a standard die)

| Weight in MFR test (kg) | Shear stress (Pa) |
|-------------------------|-------------------|
| 2.16                    | 19350             |
| 5.00                    | 44792             |
| 10.00                   | 89584             |
| 21.60                   | 193502            |

2. Determine the shear rate achieved at this shear stress from material flow curve





# How to Calculate MFR from Capillary Rheometer?

3. Calculation of melt volume rate (MVR) as follow:

$$MVR = 600\dot{\gamma} \frac{\pi R^3}{4}$$

where

- $MVR (cm^3/10min)$ : Melt volume rate
- $\dot{\gamma} (\frac{1}{s})$ : Shear rate determined at “step 2”
- $R (cm)$ : Standard melt flow rate tester die radius

4. MFR calculation knowing polymer melt density as follow:

$$MFR = MVR \times \rho_m$$

where

- $\rho_m (\frac{g}{cm^3})$ : Polymer melt density

# How to Measure MFR in LabKars?

The screenshot shows the 'Dynisco Polymer Test - Analyze' window. The 'Interpolate' button in the top toolbar is circled in red. An arrow points from the text 'Select "Interpolate"' to this button. Another arrow points from the text 'Set "Coefficient in Polynomial" as 3' to the 'Coefficients in Polynomial' dropdown menu, which is set to 3. A third arrow points from the text 'Insert "Load" in g and polymer "Melt Density" in  $g/cm^3$  in "Melt Flow" section' to the 'Melt Flow' section, which is highlighted with a red box. This section contains fields for 'Load' (set to 2160) and 'Melt Density' (set to 0.75). The 'Melt Flow' section also displays 'MVR cc/10min' as 0.143 and 'MFR g/10min' as 0.107. The 'Interpolated Data' table is visible, showing a range of shear rates from 100 to 10000. The 'Melt Flow' section is labeled 'Melt Flow Based on Shear Flow Analysis at Same Shear Stress'.

**Select "Interpolate"**

**Set "Coefficient in Polynomial" as 3**

**Insert "Load" in g and polymer "Melt Density" in  $g/cm^3$  in "Melt Flow" section**

| Rate (1/s) | Calc. Visc. (Pa-s) | Calc. Stress (Pa) |
|------------|--------------------|-------------------|
| 100        | 2154.1             | 215411.0          |
| 200        | 1319.3             | 263867.0          |
| 500        | 673.2              | 336578.0          |
| 1000       | 397.1              | 397091.0          |
| 2000       | 230.5              | 460964.0          |
| 5000       | 109.5              | 547667.0          |
| 10000      | 61.2               | 612323.0          |

Melt Flow  
Load: 2160  
Melt Density: 0.75  
MVR cc/10min: 0.143  
MFR g/10min: 0.107  
Melt Flow Based on Shear Flow Analysis at Same Shear Stress

# How to Measure Melt Density in LCR?

Select "Position" Test Type

Manage the positions to have 14 mm of piston travel distance between points

Five measurements of melt density

Whenever the plunger is in its delay time, cut the extrudate and weigh it

**Data Point Setup # 324**

| Setup # | Program Name       | Start Pos. | Temperature | Melt Time | Sensor1 ID | Die      |
|---------|--------------------|------------|-------------|-----------|------------|----------|
| 315     | PE Stability II    | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 316     | PE Short           | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 317     | PE Long            | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 318     | PE Slip Small      | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 319     | PE Slip Large      | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 320     | PP Sweep           | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 321     | PP Stability       | 100        | 190         | 300       | LC-502N    | CX394-30 |
| 322     | PE Stability       | 100        | 190         | 300       | LC-103N    | CZ394-20 |
| 323     | PE Shear Rate Long | 100        | 190         | 300       | LC-103N    | CZ394-20 |
| 324     | Melt Density       | 120        | 190         | 300       | LC-103N    | CZ394-20 |

**Control Mode**  
☒ Rate ☐ Stress

**Test Type**  
☐ Steady State  
☒ Position (Acquire At - mm)  
☐ Manual  
☐ Time Delay (Acquire At - sec)  
☐ Elapse Time (Acquire At - sec)  
☐ Relaxed Die Swell per zone

Minimum Speed   
Maximum Speed

Apply Max Packing Force ☒ Relaxed Die Swell Delay  sec. Average Readings ☐  points, over last  sec.

Melt Pause  sec. Backup Distance  mm

Barrel Diameter  inch MACRO

Estimate TestTime 300 sec.

| Point # | Speed Control | Shear Rate | Delay Sec | Time Min | Acquire At-mm |
|---------|---------------|------------|-----------|----------|---------------|
| 1       | 32.89         | 400.00     |           |          | 134.0         |
| 2       | 32.89         | 400.00     | 30        |          | 148.0         |
| 3       | 32.89         | 400.00     | 30        |          | 162.0         |
| 4       | 32.89         | 400.00     | 30        |          | 176.0         |
| 5       | 32.89         | 400.00     | 30        |          | 190.0         |



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## Intrinsic Viscosity of PET



# What is Intrinsic/Solution Viscosity (IV)?



❖ Creating a dilute solution of the polymer and comparing the flow rate of the solution to the flow rate of the pure solvent

❖ **Advantages**

- Performing at room temperature
- No need to melt the polymer
- No need to dry hygroscopic polymers (e.g. PET, PA)
- Common flowability specification (rather than MFR) among the manufactures of hygroscopic and filled polymers

❖ **Disadvantages**

- Delicate apparatus
- Using of noxious chemicals as solvent
- Not environmental friendly

# Relationship between Melt Viscosity and Intrinsic Viscosity

**Melt viscosity**

$$\eta_{melt} \propto M_w$$

**Fox-Flory  
Equation**

$$\eta_0 = K_1(M_w)^{3.4}$$

$$\ln[\eta_0] = \ln K_1 + 3.4 \ln[M_w]$$

**Intrinsic viscosity**

$$\eta_{Intrinsic} \propto M_w$$

**Mark-Houwink  
Equation**

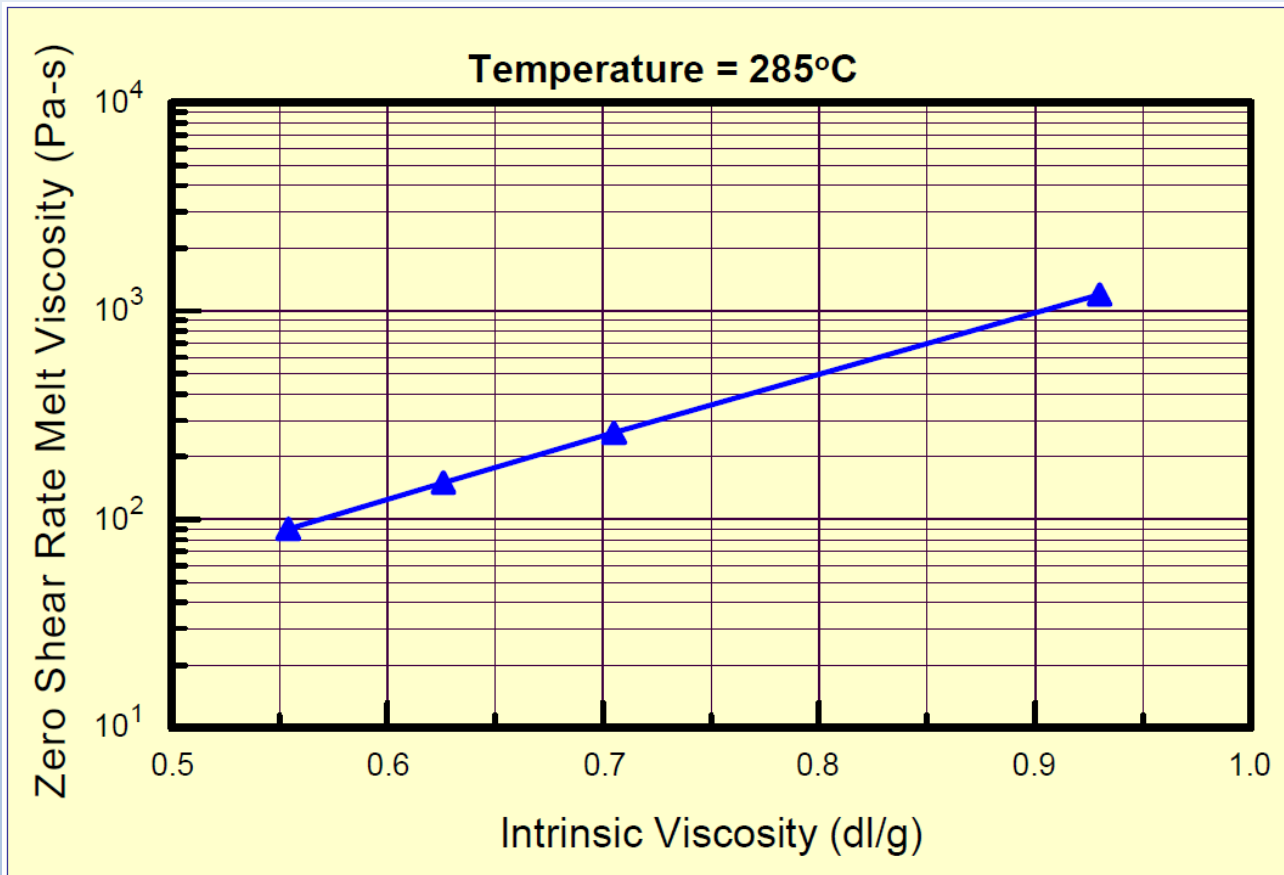
$$\eta_{Intrinsic} = K_2(M_w)^a$$

$$\ln[\eta_{Intrinsic}] = \ln K_2 + a \ln[M_w]$$

L.H. Sperling, *Introduction to Physical Polymer Science*, John Wiley & Sons, 4<sup>th</sup> Edition.

$$\ln[\eta_{Intrinsic}] = \frac{a}{3.4} \ln[\eta_0] + K''$$

# PET Melt Viscosity Versus Intrinsic Viscosity

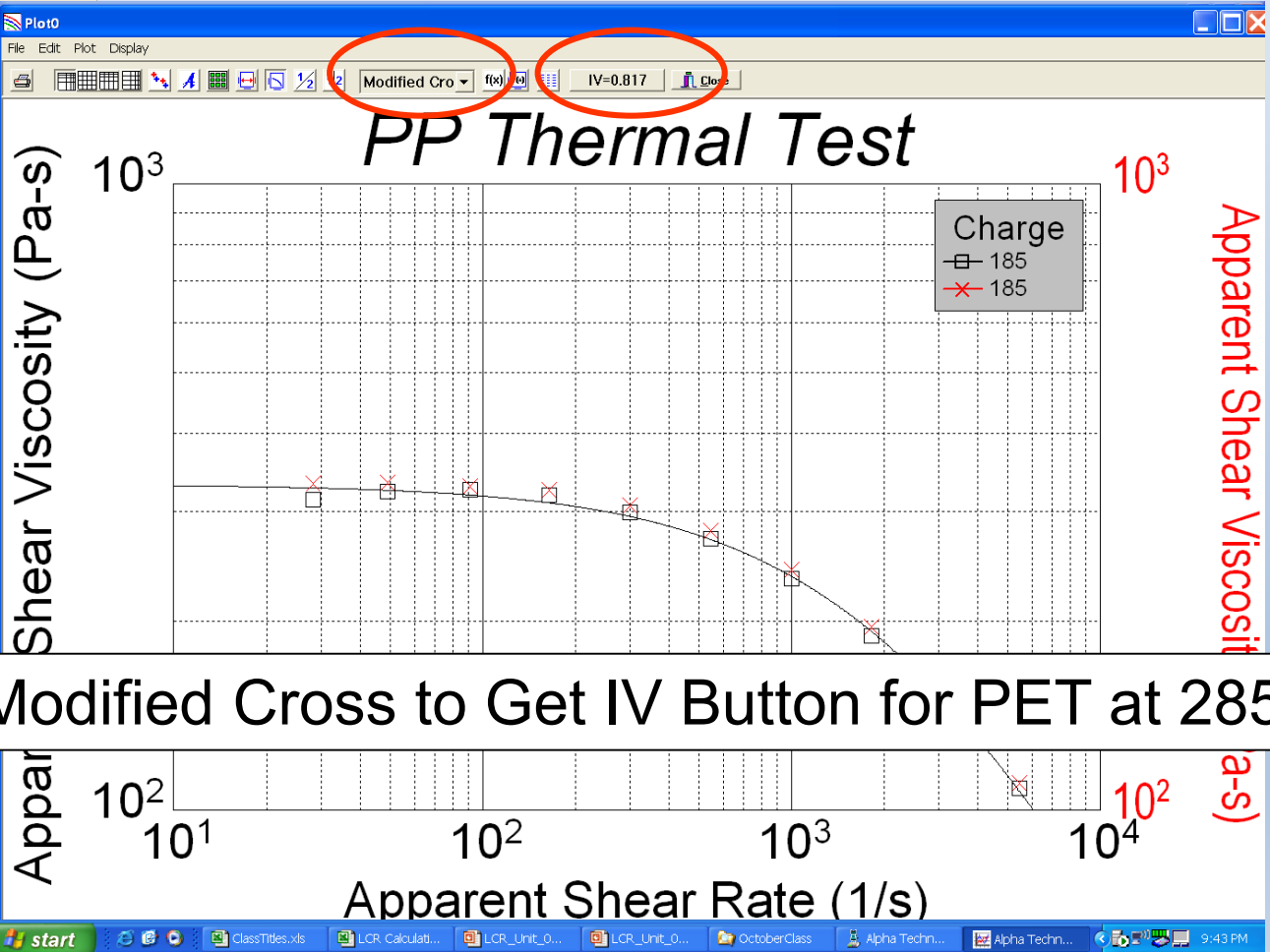
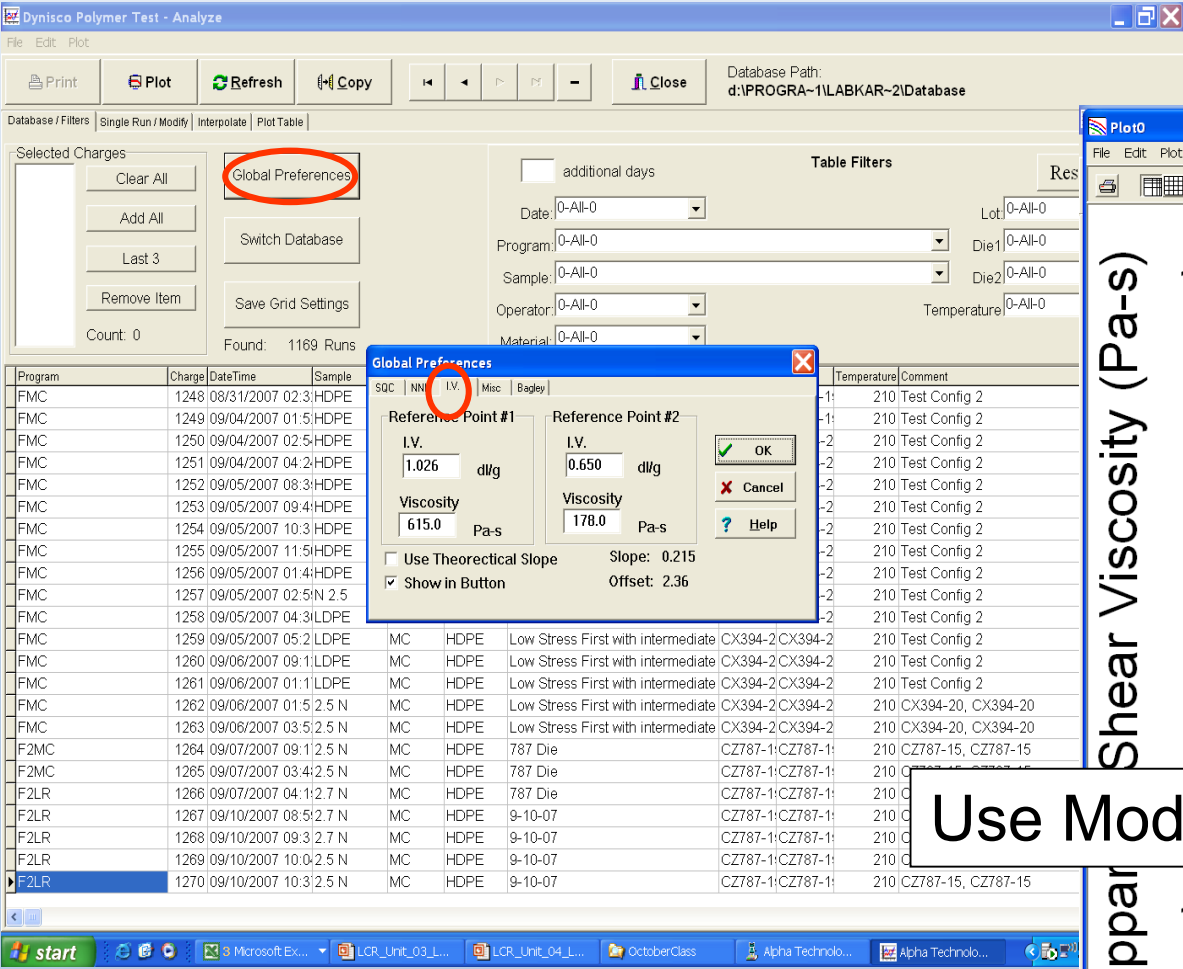


$$\ln[\eta_{Intrinsic}] = \frac{a}{3.4} \ln[\eta_0] + K''$$

Slope:  $\frac{a}{3.4} \longrightarrow$  For PET:  $a=0.75$

Intercept:  $K''$

# How to Determine IV of PET in LCR Capillary Rheometer?





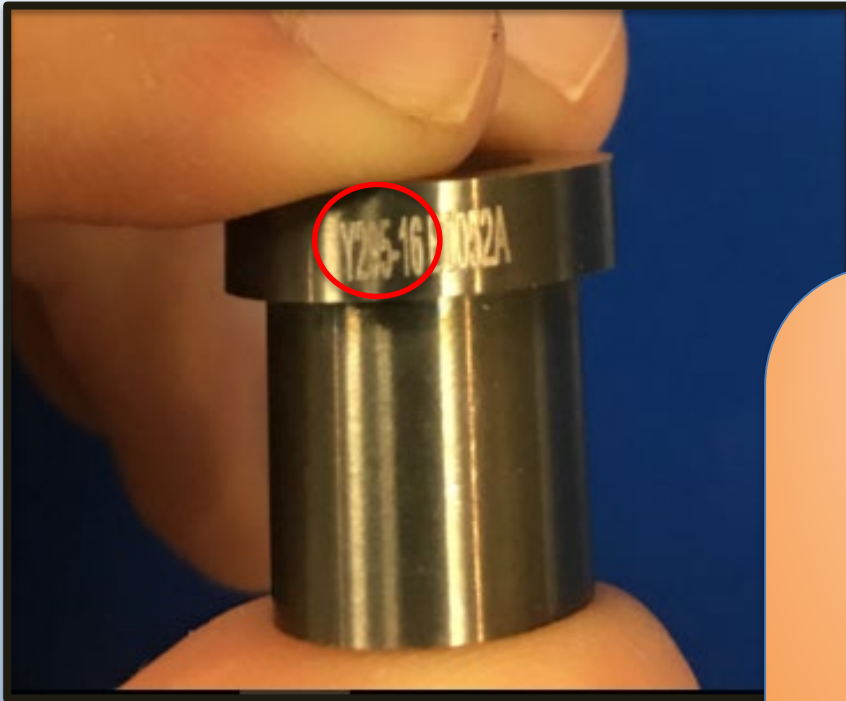


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providing a window into the process*



## LCR Dies Information

# LCR Die Part Number Code



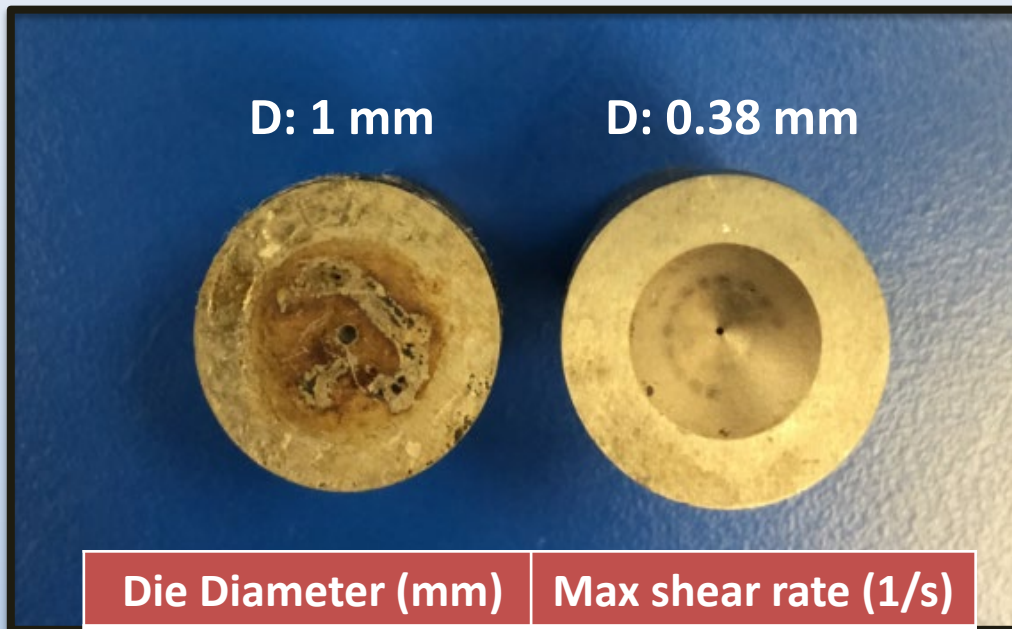
Formula for die part number:

**ADDD-LL**

where

- A: entry angle  
(W=60°, Y=90°, X=120°, Z=180°)
- DDD: diameter in inches×10000
- LL: length to diameter ratio

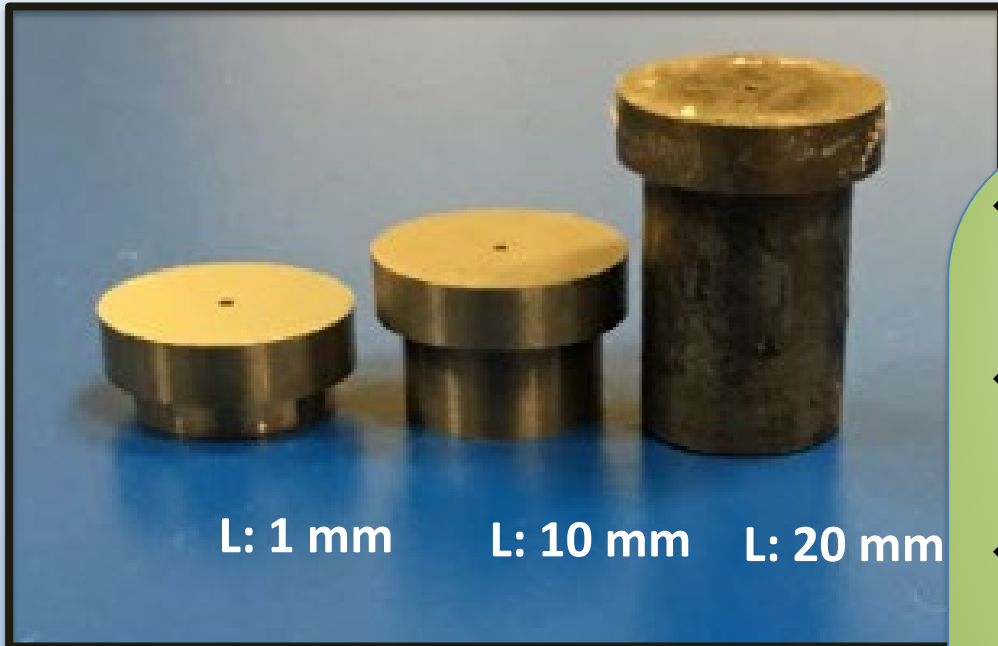
# Die Diameter



| Die Diameter (mm) | Max shear rate (1/s) |
|-------------------|----------------------|
| 0.38              | 142000               |
| 0.75              | 18700                |
| 1.00              | 7900                 |
| 1.50              | 2300                 |
| 2.00              | 980                  |

- ❖ Smaller diameter produces higher shear rates.
- ❖ Larger diameter causes less elastic deformation applied at the entrance of the die.
- ❖ larger diameter cause less entrance pressure drop, less die swell, less extensional deformation, and less slippage.
- ❖ For calculation of wall slip velocity at least 2 dies with different diameters (same L/D) are required.

# Die Length

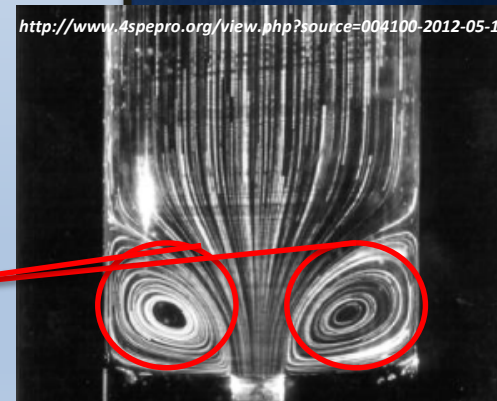
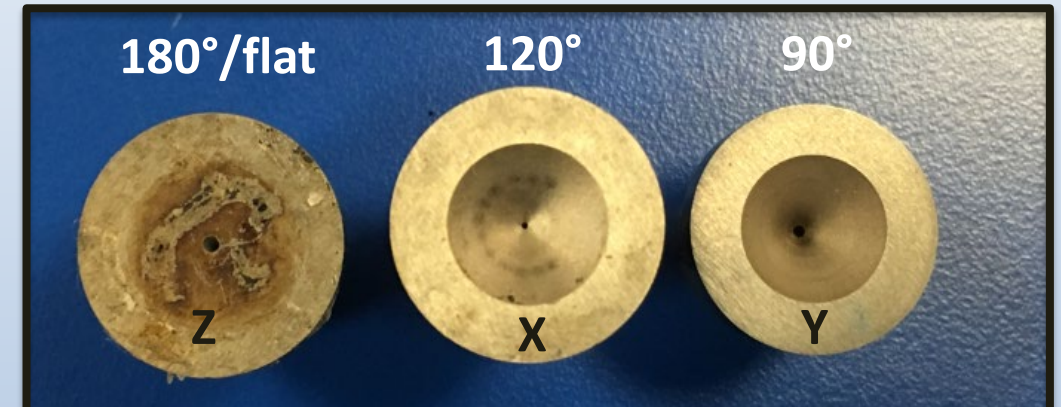


- ❖ The portion of fully developed flow in compare with entrance region increases with increasing the die length
- ❖ The percent error produced by entrance region is less with longer die.
- ❖ Short die for measuring elastic deformation (e.g. die swell, slippage) and long die for measuring shear viscosity.
- ❖ Noisy reading from short die at very low shear rates
- ❖ For calculation of entrance pressure (Bagley correction) and extensional viscosity, at least 2 dies with different L/D ratio (same diameter) are required.



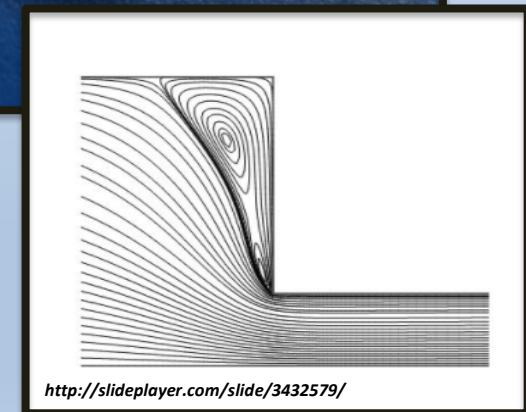
# Die Entrance Angle

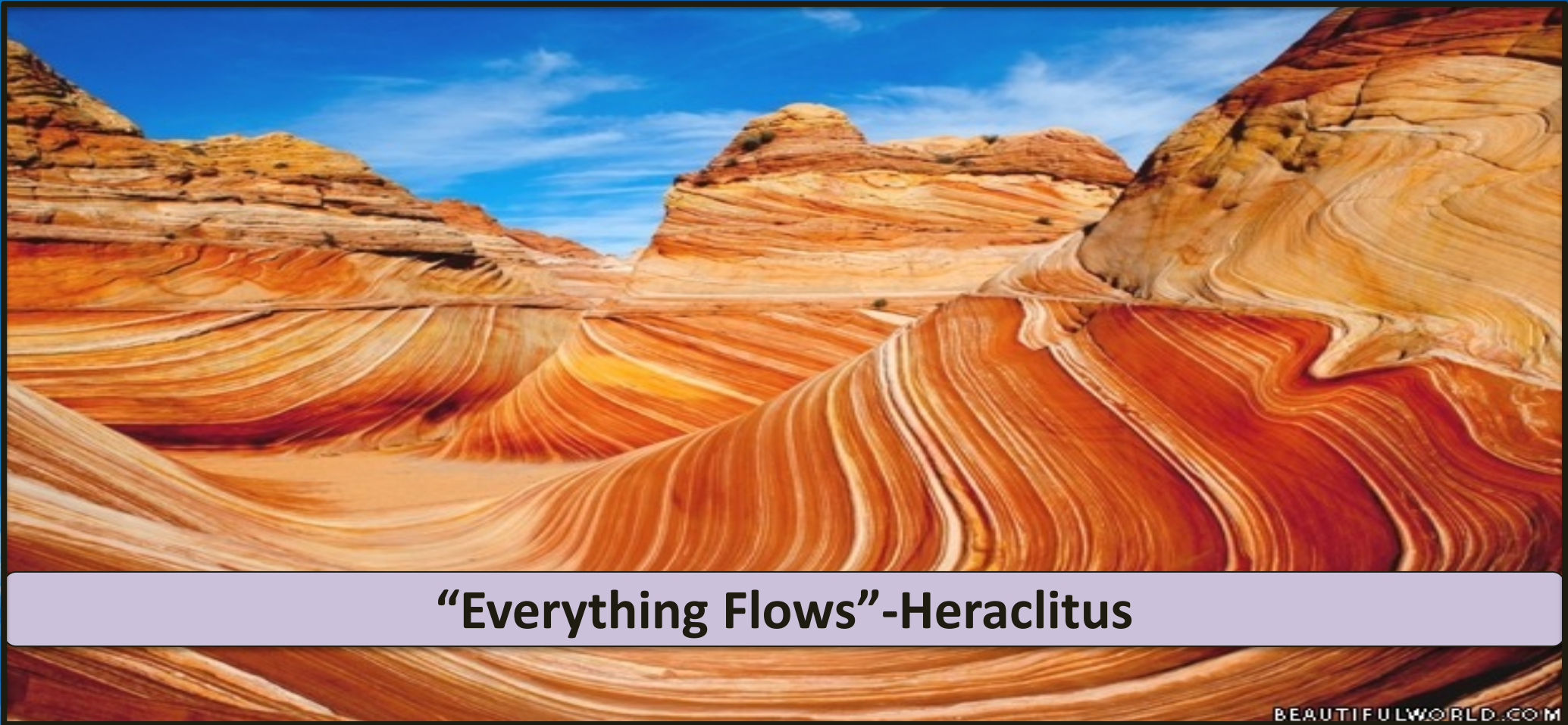
- ❖ Entrance angle has effect on flow patterns at the entrance to the capillary die.
- ❖ Lower angle causes smoother flow, less vortex flow, and less energy consumption at the die entrance.
- ❖ Lower angle reduces the elastic deformations (e.g. less entrance pressure drop, extensional deformation, die swell, melt fracture and wall slippage).
- ❖ Lower angle favors shear flow.



**Stationary vortex flows  
in the corner region**

**Flow pattern at the entrance to  
a die with a flat entrance (180°)**





**“Everything Flows”-Heraclitus**

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**QUESTIONS ?**