



The importance of spatial resolution in IR thermography temperature measurement – three brief case studies

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ABSTRACT

This paper discusses the differences in temperature measurement among three infrared (IR) cameras with different spatial resolutions. The targets used were actual field problems. This was not a laboratory experiment, but a real-world test of these cameras. Images were taken under the same conditions at the same distance with all the IR cameras. The results show there can be dramatic differences in temperature readings illustrating the importance of adequate resolution when making temperature measurements with IR cameras.

INTRODUCTION

Many modern IR cameras have built-in cross-hairs that show the user the size of the spot being measured. One would think this would solve the problem of measurement error due to a target at too great a distance for its size and IR camera resolution. But in our haste as thermographers under pressure to get results, we often don't take the time to ensure sufficient target size, or we use a function such as the maximum temperature in a box that does not show whether the target is adequate for measurement. Or, we don't have adequate optics or IR camera resolution to get a good measurement of a distant target that just isn't quite large enough.

Whether the measurement errors resulting from inadequate spatial resolution really matter depend on the magnitude of the error and the criticality of the target. In our study we found a critical problem on a substation transformer at 40% load that could certainly devolve into a major failure as the load increased to 100% with increasing demand.

The question arises as to how much difference this makes anyway. The answer isn't that simple. The degree of measurement error depends on target temperature, size, distance, IR camera and what is behind the target. The worst case scenario is found in outdoor electrical applications where there are numerous targets a few inches or smaller in size that can be 25 to 80 feet distant with no opportunity for the thermographer to get closer. Frequently, behind these targets is a clear, dry sky whose temperature can approach -50°F or colder. The IR camera averages what it captures for a given measurement spot size. When you average in -50°F you can get significant measurement errors even for hot targets that are just a bit too small for the IR camera and optics in use.

Adequate IR camera resolution is a combination of the IR camera detector and optics. The wise thermographer ensures the right system is available for the job at hand. This paper illustrates with real world measurements on actual thermal anomalies found in the field, the magnitude of error one can expect with 3 different resolution IR cameras using their standard optics. All measurements were made at about the same time from the same distance on the same targets under the same environmental and load conditions using different models (shown in parentheses below) of FLIR Systems cameras. For brevity, we will call them low, medium and high resolution IR cameras. The low resolution camera has 160 horizontal by 120 vertical pixels (E65), the medium resolution camera 320 horizontal by 240 pixels (P65HS) and the high resolution camera 640 by 480 pixels (P640) in their respective detector arrays. Also for brevity, we use "resolution" for "spatial resolution" in this paper.

One quickly recognizes the number of pixels increases by a factor of 2 in each direction resulting in detector arrays for the medium resolution camera having 4 times as many pixels as the low resolution and the high resolution camera having 16 times as many pixels as the low resolution IR camera.

We documented the distance between the IR cameras and the target using a laser range finder accurate to 1.5 feet for targets beyond 11 yards. For closer targets we estimated the distance as running a tape measure to live switchgear was deemed unsafe. In some cases we had to estimate target size for the same reason. Results are presented as brief case studies.

CASE STUDY-1: POLE SWITCH

Figure 1 shows an IR and visual image pair of a problematic mechanical disconnect on a 23kV distribution system. These connections are between an underground feed and the overhead lines. All the IR images for this case were taken with the cameras in their standard configuration with no additional optics at a range of 36 feet.



Figure 1. High resolution IR image and visual counterpart of a set of 23kV distribution switches. The center phase shows a significant temperature rise. Distance to target is 36 feet.

Figure 2 shows the medium (left) and low resolution IR images of the same set of switches.

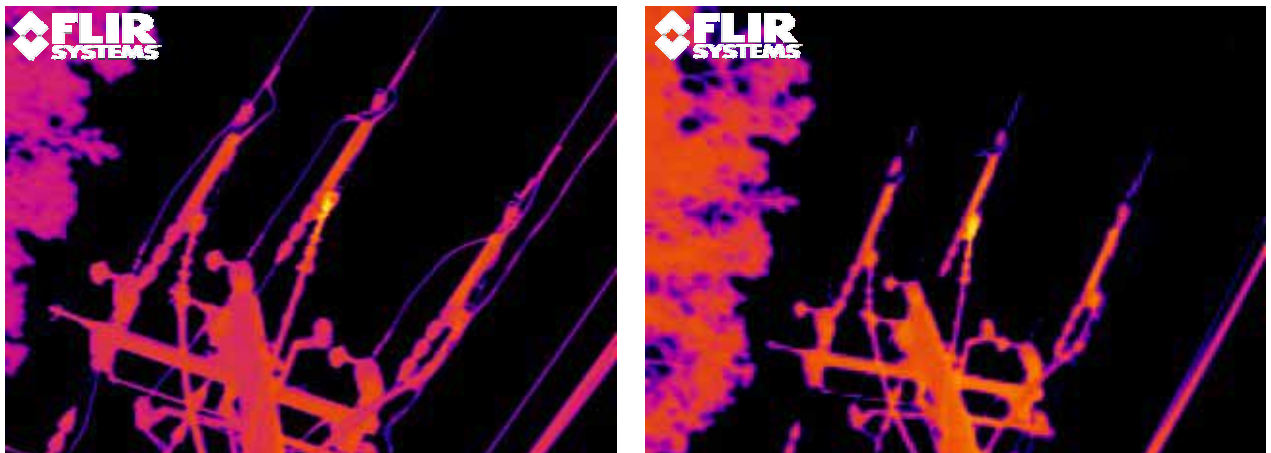


Figure 2. Medium (left) and low resolution images of the same setup as in Figure 1.

We thermally tuned the level and contrast of each image for maximum “viewability” of the problem, so the temperature scales are close, but not exactly the same. In all cases the thermal anomaly can be seen, but it is much clearer in the high resolution image, to the extent one can see the bolt patterns on the connection. But if this were the extent of the difference, one could justifiably argue a lower resolution IR camera, hence lower

cost would suffice. But what do the temperature measurements show? Table 1 gives the measurement summary.

Switch Disconnect at 12 Yards				
IR Camera	Temperatures			% Load (estimated)
	T	ΔT	ΔT Load corr	
Hi Res	173 °F	91°F	271°F	50
	78°C	50°C	150°C	
Med Res	155 °F	72°F	216°F	50
	68°C	40°C	120°C	
Lo Res	125 °F	45°F	133°F	50
	52°C	25°C	75°C	

Table 1. Measured temperature, temperature rise and load corrected temperature rise for three IR cameras of different resolution. Target distance is 36 feet.

It is very interesting to see the high resolution IR camera gives twice the delta-T (ΔT), temperature rise, as the low resolution IR camera and 25% more than the medium resolution camera. For this study, we used an emissivity of 0.95 for all cameras, probably not exact, but this emissivity will give a temperature reading lower than the actual reading. And the differences will only increase as the emissivity is lowered. So, we are considering the best case scenario for measurement comparisons among these cameras.

We estimated the load at 50% based on our utility contact's experience. The temperature rises calculated for 100% load¹ are given in the column labeled " ΔT Load corr". For one set of severity criteria used by the Electric Power Research Institute (EPRI), the load corrected temperature rises are in the critical category (135 °F rise or higher) for the high and medium resolution cameras and almost critical for the low resolution camera.

The bottom line is all the IR cameras would find the problem, but without a telescope lens on the low and medium resolution cameras, incorrect readings would have been obtained and the level of severity would have been significantly underestimated. The disadvantage of telescopes besides expense is they reduce the field of view and enhance the optical leveraging. The latter means it is more difficult to get a good, stable image with a telescope attached as small motion of the IR camera is magnified by the power of the telescope. This is why digital camera companies have patented image stabilizing telescopes for their cameras. The thermographer can still accomplish the task. It just takes longer with a telescope.

CASE STUDY-2: SUBSTATION TRANSFORMER JUMPERS

Figure 3 shows an IR image and visual image pair of a 115kV to 23kV substation transformer low side with definite problems on two of the phases. The jumpers from the bushings to the feed are stranded cables where some of the strands have broken over time or are not well connected electrically. This causes overloading of the remaining good conductors resulting in significant heating. This is often termed "barber poling" for obvious reasons.

Measured load on this transformer was 40% of maximum. Range was 33 feet. Cable diameter is nominal ¾". This was taken in early June when the weather was cool and electrical demand in the area was low. Figure 4 gives the medium (left) and low resolution IR camera images of the same scene.

Again, the thermal anomalies are picked up by all the IR cameras, so these problems would not have been missed.



Figure 3. High resolution thermal image of a 115kV to 23kV substation transformer low side. Significant thermal anomaly on left and center phase jumpers due to some strands broken or poorly connected. IR image effect is often termed "barber poling".

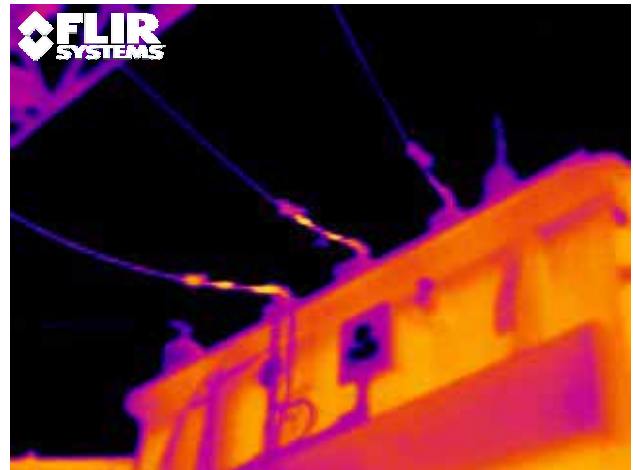


Figure 4. Medium (left) and low resolution images of the same setup as in Figure 3.

But what about the temperature readings? Table 2 gives a comparison of maximum temperature readings for the left-most phase of the barber poling. For this study, the results are even more dramatic than for the pole switch. Here the ΔT measured with the high resolution camera is over 2.3 times that of the low resolution camera. And the problem severity according the EPRI criteria is critical at 40% load for the medium and high resolution measurements!

The load corrected temperature rises are of great concern. We deemed the problem so significant we sent a report immediately to the utility who owns the substation transformer. Because when air conditioning season hits, there is a very high probability of failure of this system with load temperature rises at full load estimated approaching 900 °F.

Substation transformer jumpers at 11 yards				
IR Camera	Temperatures			% Load
	T	ΔT	ΔT Load corr	
Hi Res	280 °F 138 °C	211 °F 117 °C	889 °F 494 °C	40
Med Res	243 °F 117 °C	172 °F 95 °C	724 °F 402 °C	40
Lo Res	127 °F 53 °C	90 °F 50 °C	380 °F 211 °C	40

Table 2. Measured temperature, temperature rise and load corrected temperature rise for three IR cameras of different resolution. Target distance is 33 feet.

CASE STUDY-3: GENERATOR TIE-IN BREAKER

Figure 5 shows the high resolution IR and visual pair for a paper mill 480 v generator tie-in breaker. This breaker had a 3,000 amp load at the time of measurement, estimated at 75% of full load.



Figure 5. High resolution IR image and visual photo of 480 volt generator tie-in breaker.

We estimated the distance at 4 feet, though the problem was somewhat in the rear of the switchgear and could not readily be identified. But it was definitely a problem with temperature rises somewhat lower than the above examples, but still significant. If the tie-in breaker fails the paper mill production shuts down until it is repaired.

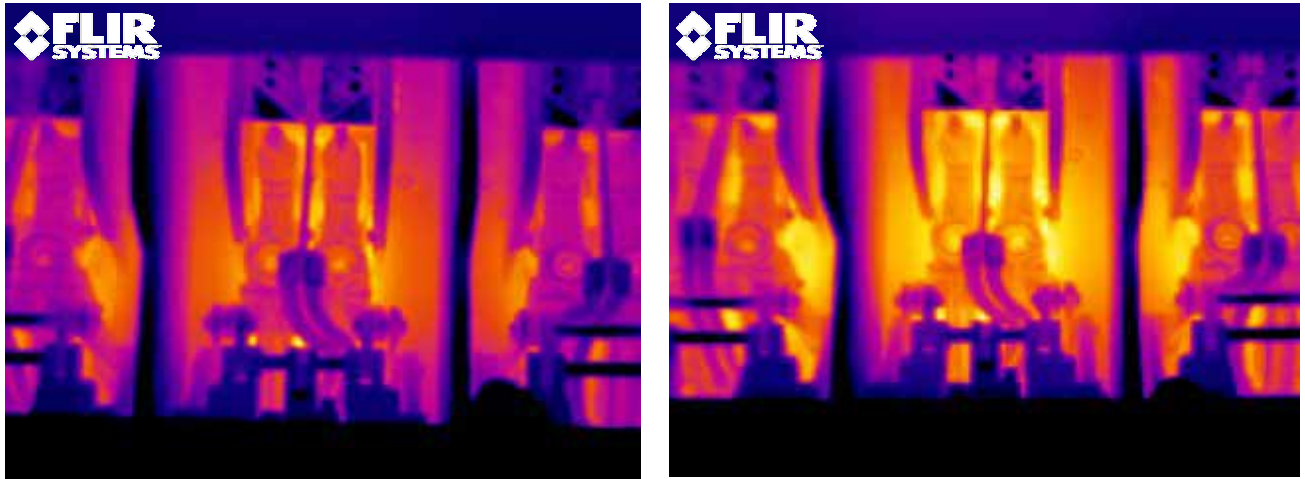


Figure 6. Medium resolution (left) and low resolution IR images of 480 volt generator tie-in breaker.

Table 3 gives the temperature data for this case study. Here the differences among the cameras are less significant than in previous examples due to the closeness of the range and size of the target.

Generator tie-in breaker at 4 feet				
IR Camera	Temperatures			% Load
	T	ΔT	ΔT Load corr	
Hi Res	210 °F 99 °C	85 °F 47 °C	134 °F 74 °C	75
Med Res	198 °F 92 °C	72 °F 40	113 °F 63 °C	75
Lo Res	193 °F 89 °C	68 °F 38 °C	108 °F 60 °C	75

Table 3. Measured temperature, temperature rise and load corrected temperature rise for three IR cameras of different resolution. Target distance is about 4 feet.

There is enough difference so the load corrected high resolution ΔT is right at the EPRI critical level where the Low resolution ΔT is still in the middle of the serious category. Having said that, the EPRI severity criteria are used here just as an example for comparison purposes. The Infrared Training Center does not advocate any specific set of severity criteria as there needs to be a lot more research done. Much of what is published is based on experience and a desire to have something to go on. There are many sets of severity criteria published and they are all different. See the paper by Giesecke in these proceedings for additional comments and insight on severity criteria.

SUMMARY

High resolution IR cameras can get significantly better temperature readings for small targets at some distance. The targets in this study were all on the size of the smallest dimension of about an inch at ranges from 36 feet to 4 feet. The biggest differences were seen understandably at the largest distances. While one could expect results similar to the high resolution camera by applying a 4X telescope to the low resolution camera or a 2X telescope to the medium resolution camera, there are distinct advantages to not having to use a telescope. A telescope reduces the field of view by the power of the optic requiring more care in aiming and target acquisition. It also magnifies movement in the same manner. This adds an additional requirement to the thermographer to somehow achieve stability either through some type of rest, mount or tripod. A telescope is another optic to care for and be careful of as they can break.

For applications beyond electrical anomalies where large surfaces need to be imaged such as building applications, the high resolution IR camera has a distinct advantage in that one must take 16 images with the low resolution camera, either at one-fourth the distance or with a 4X telescope, or 4 images with a medium resolution camera at one-half the distance or with a 2X telescope to cover the same area as the high resolution camera with one image. Think of the time saved in not having to stitch together all these IR images!

Thermographers should be aware of their target sizes and have an appreciation for the demands of measuring small targets at distance. Many of us prefer the "maximum temperature in a box" feature on IR cameras. Use it in conjunction with the spot measurement, as the spot measurement can show you if your target is large enough. You can spot problems and still be fooled in making temperature measurements if you don't have enough resolution in your IR camera.

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REFERENCE

1. Madding, Robert P., Leonard Ken, Orlove Gary L.; "Important measurements that support IR surveys in substations; Proc. InfraMation ; pp19-25; Sep, 2002.

ABOUT THE AUTHOR

Bob is a graduate of the University of Missouri with a BS in Physics, and a Masters and Ph.D. in Physics from the University of Wisconsin-Madison. He began the first infrared thermography seminar at the University of Wisconsin Extension in 1978. He co-founded the Thermosense Conference in 1978 with two other colleagues from the UW. In 2000 he founded the Inframation Conference, the largest annual IR conference for thermographers. Bob holds an ASNT NDT Level III in Thermal Infrared and an EPRI Level III in IR thermography. He has published numerous technical papers on infrared thermography applications, as well as contributing chapters to textbooks such as Applied Thermal Design and the Encyclopedia of Optical Engineering. Bob has over 25 years experience in infrared thermography applications and training.

